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RADIO NEWS

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*Buy Your New Radio
from Your Radio Dealer*

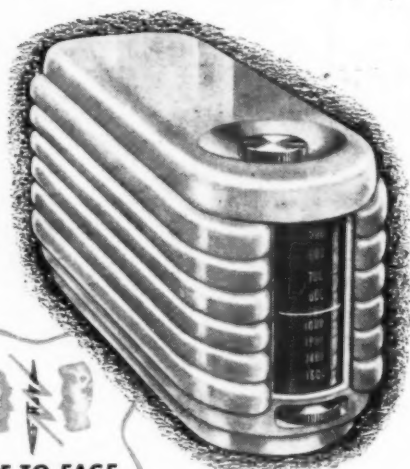


"You will get more satisfaction—better value—from a radio bought through a radio *specialist*—your local radio dealer.

"You will get every worth-while improvement—because my years of experience and technical knowledge enable me to choose the best postwar models.

"Many of us dealers have chosen Meck Radios—because they offer you outstanding engineering advancements as well as a reputation for quality firmly established through years of building world-famed electronic products."

Your Radio Dealer



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MECK RADIOS



MECK RADIOS

JOHN MECK INDUSTRIES • PLYMOUTH, INDIANA, U. S. A.

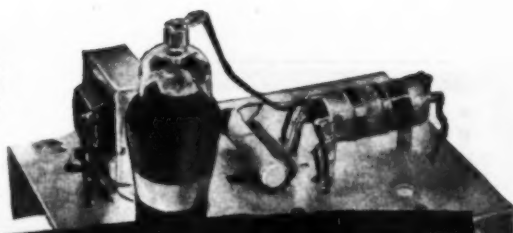
VARIOUS MODELS • PORTABLES • CONSOLES • PHONOGRAPHS



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A. M. SIGNAL GENERATOR
gives you valuable experience. Provides amplitude-modulated signals for test and experiment purposes.

Radio Servicing pays many good money for full time work. Many others make \$5, \$10 a week EXTRA fixing Radios in spare time.



Learn RADIO by PRACTICING in Spare Time

with 6 Big Kits of Radio Parts I Send You

Here's a *practical* way to learn Radio at home in spare time—to train for a good Radio job, or start your own spare time or full time Radio Service Business! You get Radio EXPERIENCE building real Radio Circuits with kits of standard parts I send. You get solid KNOWLEDGE of Radio, Television, Electronic fundamentals from my easy-to-grasp lessons. You follow the same "50-50" method that has helped hundreds of beginners make \$5, \$10 EXTRA a week in spare time while learning—and prepare for good full time jobs at good pay.

Future Looks Bright for Trained Radio Technicians, Operators

The Radio Repair Business is booming. Profits are large and peacetime prospects are bright. Broadcasting Stations, Aviation Radio, Police Radio, Loudspeaker Systems, Radio Manufacturing, all employ trained Radio men at good pay.

Be Ready to Cash in on Jobs Coming With Television, Electronics

Think of the NEW jobs that Television, Frequency Modulation, Electronics, other Radio developments promise for the peacetime future. You have a real opportunity. I will train you to be ready to cash in when amazing wartime Radio developments are released for unlimited peacetime use.

Mail Coupon for Free Copy of Lesson and 64-page Illustrated Book

I will send you FREE, a sample Lesson, "Getting Acquainted with Receiver Servicing," to show you how practical it is to train for Radio in spare time. And with it I'll send FREE, my 64-page, illustrated book, "Win Rich Rewards in Radio." It describes many fascinating jobs in Radio, tells how you can get started. No obligation—no salesman will call. Just mail coupon in an envelope or paste it on a penny postal.—**J. E. SMITH, President, Dept. 5BR, National Radio Institute, Pioneer Home Study Radio School, Washington 9, D.C.**

**My Course includes Training in
TELEVISION • ELECTRONICS •
FREQUENCY MODULATION**



You build this SUPERHETERODYNE

CIRCUIT that brings in local and distant stations. You get practical experience putting this set through fascinating tests.

You build this MEASURING INSTRUMENT

yourself early in the course—use it for practical Radio work on neighborhood Radios to pick up EXTRA spare time money!

BE A SUCCESS in RADIO I Will Train You at Home

Sample Lesson FREE

GETTING ACQUAINTED WITH
RECEIVER SERVICING

Gives hints on Receiver Servicing. Locating Defects, Repair of Loudspeaker, I.F. Transformer, Gang Tuner Condenser, etc., 31 illustrations. Study it—keep it—use it—without obligation! Mail Coupon NOW for your copy!



**GET BOTH 64 PAGE BOOK
SAMPLE LESSON FREE**

**MR. J. E. SMITH, President, Dept. 5BR,
NATIONAL RADIO INSTITUTE, Washington 9, D. C.**

Mail me FREE, without obligation, Sample Lesson and 64-page book, "Win Rich Rewards in Radio." (No Salesman will call. Please write plainly.)

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COVER PHOTO

By Frank Ross
(Staff Photographer)

Production testing of transmitter
r.f. chokes for "Q" at Ohmite
Manufacturing Company plant.

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**"HOGARTH HAS ALREADY OCCUPIED
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ENGLISH IS ECHOPHONE EC-1"**



...of deep sea water and the explosive concussion of depth charges.

Just the same, Jensen Engineers and factory have learned plenty in the process of designing this and many other

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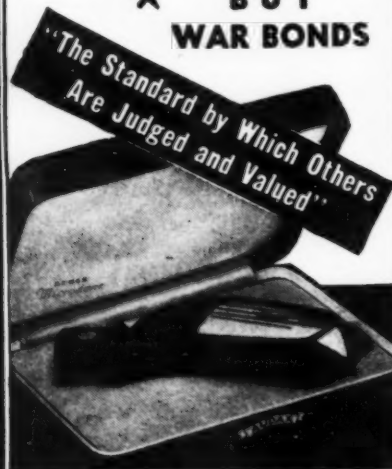
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Creators of High Grade Electrical
and Acoustical Apparatus Since 1915

Send for your copy of our informative
"PICK-UP FACTS"

★ BUY
WAR BONDS



FOR THE RECORD

by the editor

THE acceptance of television by Mr. and Mrs. America will depend a great deal upon the proper use of the lowly antenna. The television user can't toss a wire out of his window—hook to a convenient radiator—or coil a homemade loop under the living room rug and still get satisfactory results. The very heart of a satisfactory television installation is the special antenna required for optimum performance. It is just as vital as any other component and can't be connected by haywire techniques. Good television pictures require that adequate signal strength be supplied to the input terminals of the set. Without a satisfactory signal good pictures will be conspicuous by their absence.

In cities like Chicago, New York, Pittsburgh, etc., where thousands of families live in apartment buildings, the problem of installing adequate television antennas will reach major proportions. The use of high frequencies for television channels means, by their very characteristics, that receiving antennas must, of necessity, be designed to take full advantage of their directional receiving properties. There is, at the present stage of the art, only one antenna system suitable to serve a large number of television sets tuned to different stations. It uses a new type amplifier and is quite costly. There is another problem which must be considered as new television stations come on the air. With widely scattered transmitter locations signals will emanate from various directions and it will be necessary to consider this when installing television antenna systems.

Amateur radio ops realized long ago that if they were to obtain optimum results from their high-frequency equipment that special antennas would have to be designed that would give them the added advantage of a directional system. For example, it was found that best results were obtained when the antenna was located high above the building and well away from trees, metal stacks, towers, etc. It was soon discovered that the most successful antennas were those which could be rotated and, like a "radio searchlight," be directed to the source of the signal. Equally important was the

design of special transmission lines between the antenna elements and the receiver. This, too, must be considered in the design of any television antenna system. It is our guess that the American radio amateur will again solve this problem. He's solved many others which have been directly responsible for the very existence of radio broadcasting (now in its 25th year).

Many of our readers are familiar with the many forms of high-frequency antennas that use directors and reflectors to obtain the desired results. Such antennas are ideally suited for the reception of television signals. However, their general use by the public would meet with many obstacles. Lacking a technical "know how," Mrs. Jones would not be proficient with its use. If she lived in a city having, say, five television stations in five different directions, it is doubtful that she would take the necessary precautions to rotate the receiving antenna to its proper position for each station.

Engineers and amateurs have a golden opportunity at hand for the development of successful and flexible television antenna systems. It is a problem that should be studied now. It should not wait for the end of the war. At this writing, the FCC has not rendered its decision on television frequencies. But, no matter what this decision may be, the fact still remains that television cannot be successful on any frequency until the antenna problem has been solved.

RADIO NEWS joins in extending hearty congratulations to the Radio Broadcasters—who are celebrating their 25th anniversary. Now in our 26th year of publication—we have seen the art of broadcasting develop from a meager beginning to one of the most cherished of man's possessions. From its swaddling clothes has emerged a tremendous public service. To the radio amateur must go much of the credit for its growth. Out of the attic and basement has come developments—directly responsible for its technical achievements. Yes—the ham is indispensable to American radio progress.....O. R.

No Tools Required to Install These ATTACHABLE SWITCHES for Mallory Volume Controls

THEY'RE easier to install than any other "off-on" snap switch—no tools are required to attach them to volume controls! That's why so many service men prefer to use Mallory Attachable Switches.

The Mallory switch designed for controls of $1\frac{1}{2}$ " diameter fits Mallory standard universal controls, carbon and wire-wound types, TRP tapped controls and Universal

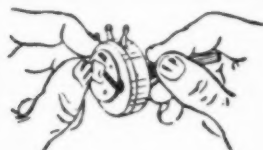
dual controls. The Mallory switch designed for $1\frac{1}{8}$ " diameters fits Mallory MR, MK, UM, TM and DTM controls.

Both may be rigidly mounted without any bending or alteration of the volume controls. Both are available in circuit arrangements to suit any type of application. See your Mallory distributor!

P. R. MALLORY & CO., Inc., INDIANAPOLIS 6, INDIANA



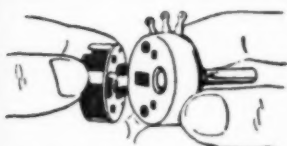
For
 $1\frac{1}{2}$ " Diameter
Controls



To attach switch, remove dust-proof plate from back of control.



Turn shaft as far as it will go in clockwise direction.



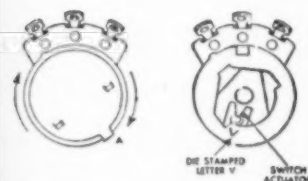
Make sure switch actuating arm is in proper position, as pictured.



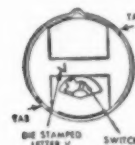
Insert tongue of switch into long slot. Press down, slide up slightly and switch will snap into place. Move back slightly to lock.



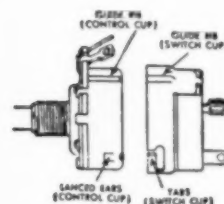
For
 $1\frac{1}{8}$ " Diameter
Controls



Remove cover.
Line up switch actuator of volume control with Letter V.



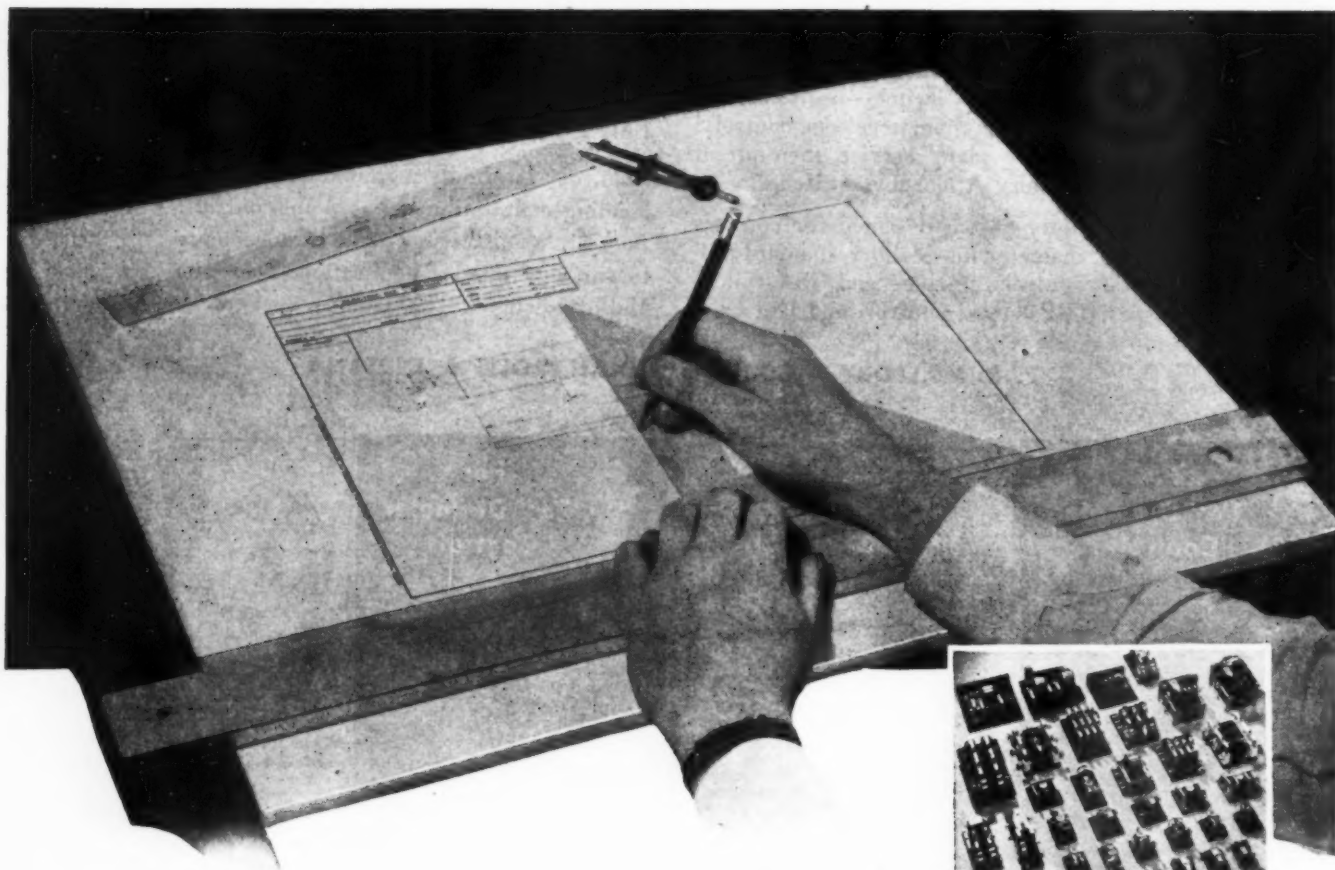
Line up switch cam with Letter V.



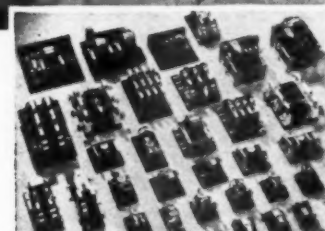
Line up guide rib on switch and on control as shown, press switch down tightly until switch tabs snap over ears on control cup. To remove switch, bend up ears.

P. R. MALLORY & CO. Inc.
MALLORY
APPROVED
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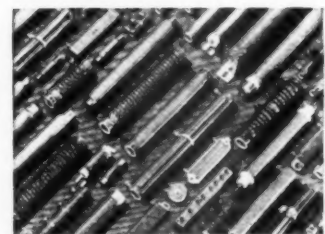
CONTROLS FOR POSTWAR PRODUCTS



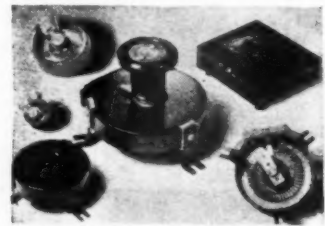
With the rush to catch the earliest possible markets with post-war products, it is important that they be designed with units that can be procured without undue delay. Manufacturers of equipment requiring electric controls will find Ward Leonard Relays, Resistors and Rheostats readily available without "time-out" for redesigning. Facilities at Ward Leonard used to produce products for war purposes required little or no conversion. To serve post-war markets, they will likewise require a minimum of reconversion. Make your selection from the Ward Leonard Line. Let us send you bulletins describing controls of interest to you.



RELAYS for light, intermediate and heavy duty, sensitive, transfer, time delay, antenna changeover, break-in and latch-in operation.



RESISTORS that withstand heat, moisture, vibration and other adverse conditions. Wide range of types, ratings, terminals and enclosures.




RHEOSTATS that include the widest range of sizes, types and current ratings from the tiny ring types for radio to huge industrial assemblies.

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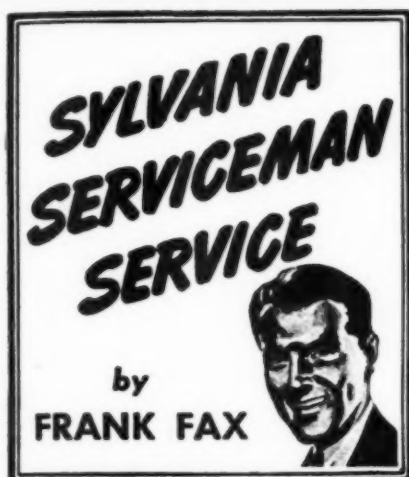
SYLVANIA NEWS

RADIO SERVICE EDITION

FEBRUARY

Published in the Interest of Better Sight and Sound

1945



Neat, attractively styled service garments make a good impression on customers and save wear and tear on ordinary clothes.

For wear in the shop, working on auto radios, or even in customers' homes, Sylvania offers well tailored, practical service coats and jackets. Made of serviceable double-strength herringbone weave dungaree cloth in a green and white mixture, giving a tweed effect, both garments are provided with roomy pockets. Jacket is of single breasted three button style with full sleeves, while coat has a special button arrangement which allows for tails to be buttoned in front, offering added trouser protection when kneeling.



Available in five popular sizes—36, 38, 40, 42 and 44, coats are priced at \$1.95 each, jackets in same sizes at \$1.75.

Order from your local Sylvania distributor, or send your order to Frank Fax, Sylvania, Emporium, Pa.

Servicemen Find Plenty of Ideas in Sylvania's Model Shop Layout

Booklet Packed With Helpful Hints On Low-Cost Steps in Modernization

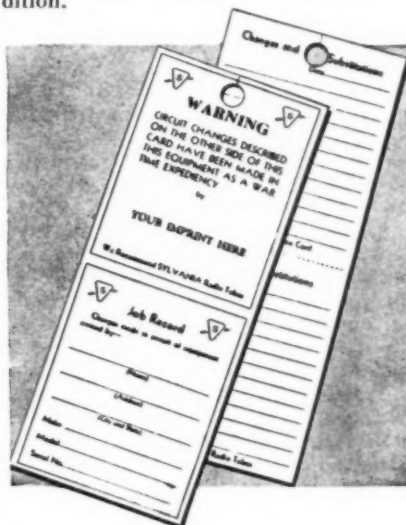
Servicemen can do more than dream about that model service shop. For Sylvania comes through with plenty of practical, down-to-earth suggestions in "The Sylvania Model Service Shop," the book prepared to help radio servicemen modernize their shops at a cost compatible with earnings.

REWIRING SETS AIDS BUSINESS

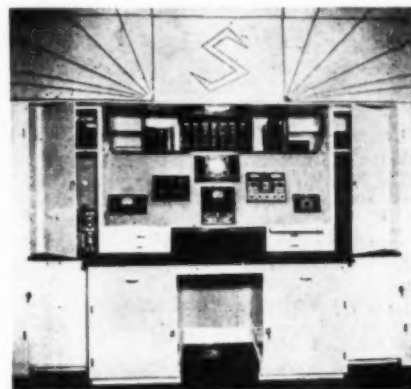
Servicemen who have been revamping sets to meet wartime shortages of tubes have not only been doing a fine job for their customers, but they have also been building up future business for themselves.

When tubes and other replacement parts are freely available, servicemen will have an opportunity to restore sets to their original circuits. Customers whose sets were kept operating by emergency re-wiring will naturally come back to the serviceman who helped them.

Future repair jobs will be simplified by the wide use which servicemen made of the Sylvania Warning Cards. These cards show the changes made in the set, and thus save the serviceman valuable time in restoring the receiver to its original condition.



The book describes an actual shop designed and built by Sylvania with three things in mind: economy, efficiency and attractive layout. Every section of the model shop is described in full detail, from entrance, through office and testing department to repair section. Clearly written descriptions are supplemented by readily



Here is the actual Model Shop built by Sylvania to help servicemen with their modernization plans.

understandable floor plans, and all recommendations are practical ones. A handy list of important instruments, tools and equipment that every shop should have is also included.

Whether he wants to "start from scratch" or merely make a few minor changes, every serviceman will find the "Sylvania Model Service Shop" a valuable guide in improving the appearance and efficiency of his shop. Nor will he have to wait until after the war, because many of the ideas can be put into effect right now by resourceful servicemen.

Price of the book is ten cents, and it may be obtained from Sylvania Electric Products Inc. Emporium, Pennsylvania.

SYLVANIA ELECTRIC

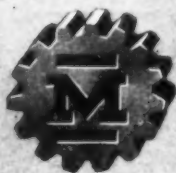
PRODUCTS INC.

Radio Division • Emporium, Pa.

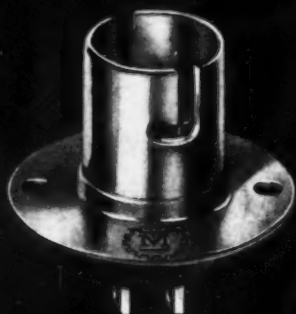
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February, 1945

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Spot Radio News

By RADIO NEWS Washington Correspondent

Presenting latest information on the Radio Industry.

THE FCC FRONT saw another delay, that of the confirmation of Paul A. Porter as Commissioner to succeed James Lawrence Fly. Although Mr. Porter's name had been submitted weeks ago, the heavy calendar of the Senate Committee charged with approving such nominations, precluded such action. The *sine die* adjournment of Congress then ended all hopes of confirmation during the 78th Congress session. The President therefore has been required to resubmit the nomination to the next session of Congress which convened January 3. The Senate Committee of this session began new studies of the nomination. It is expected that confirmation will come soon after the Committee meets and by the time this column appears, Mr. Porter should be FCC Commissioner and probably chairman of the FCC, too.

The Commission probably will have still another new Commissioner in its ranks shortly after the beginning of the new year, a Commissioner who will fill the post left vacant by Commander T. A. Craven. It appears as if the FCC assistant general counsel in charge of broadcasting, Rosel H. Hyde may be that new Commissioner. Mr. Hyde was in the running last year, when E. K. Jett was nominated and named FCC Commissioner.

Accelerated action on the allocation program also is expected when the FCC panel is completed with its new Commissioners.

POSSIBILITIES OF RESUMING civilian receiver production before the defeat of Japan do not seem to be too bright, according to L. J. Chatten, the new director of the radio and radar division of the WPB. Appearing before a meeting in New York and industry committee groups, he said that tubes and other parts still are tight and will continue to be that way for a long time. During the next five months, three times as many tubes will be required by the military for replacement in depots. Over 85% of the current production will be required by the military even after Germany is defeated. This leaves 15% for civilian production, and with the shortages of tubes and components, manufacturers are going to find many production hazards, according to Mr. Chatten.

Discussing the spot authorization plan, which permitted the manufacture of a variety of civilian items, Mr. Chatten said that radios and automobiles were about the only two products that were omitted from the plan. And they will not be placed in that produc-

tion category, unless a miracle occurs, he said. The only nonmilitary radio authorizations that have been extended thus far have been for small quantities of two-way apparatus for police, forestry, and emergency work.

To accelerate production, a *Victory First* program has been instituted by the industry. A maximum peak production of \$250,000,000 a month by March 1, has been set as a goal.

The tube front presents the most serious problem, for military requirements are still growing. Approximately 10,000,000 receiving-type tubes are now required every month by the military. The end of the European war will reduce this requirement slightly, and not until at least one year after Germany's defeat is a reduction expected. At present, this appears to be about 45%. In view of these military requirements, but 13% of the total receiver production is available for civilian replacement purposes. WPB estimated that about 19,000,000 tubes were made for replacement purposes, while the demands exceeded 36,000,000. In the first quarter of 1945, about 2,000,000 tubes a month are scheduled. This is about 500,000 more than previously allocated. Within four months after V-E day, a civilian production of 4,000,000 tubes a month is anticipated. Although this production schedule is a substantial one, it still will not meet all demands. For, according to WPB, the combined military and civilian requirements after Germany's defeat, still will be 60% to 70% above present production rates!

RADIO'S ROLE IN THE famous Red Ball Express transport system on the Western front was applauded loudly recently by military executives of the Motor Transport Brigade. Thanks to the communications system initiated by the Signal Corps, a continuous flow of traffic was possible. In addition, it was possible to maintain constant contact with each convoy, follow its travel, and know the exact destination. Thus, upon arrival of the convoy, radio could direct the vehicles to other destinations, without loss of time.

A six-station radio network provided the communications link. The control station was located at brigade headquarters. And one of the stations was located at a terminal of the highway. Here the convoys were formed and sent out to their respective destinations. When a convoy started out from the regulating point, a message was forwarded to all the stations along the route, describing the contents and destination, and providing

RADIO NEWS

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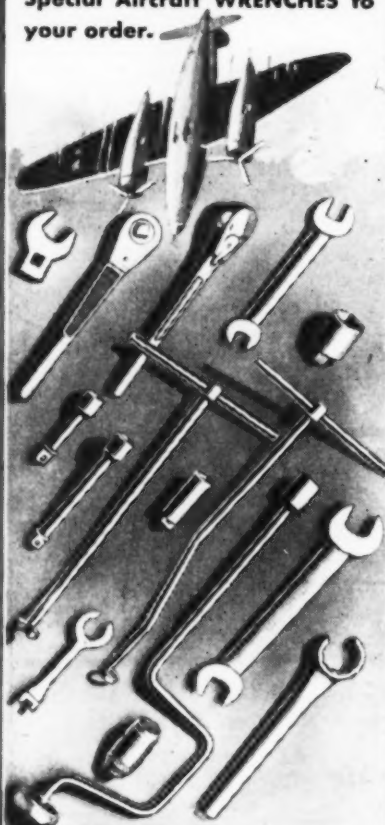


"For the want of a shoe" . . .

For the want of a WRENCH a nut was loose

A handy WALDEN WORCESTER WRENCH would have tightened that nut . . .

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468 SHREWSBURY STREET
WORCESTER, MASSACHUSETTS

full instructions as to how it was to be handled. The net control station handled as many as 93 messages a day, each message approximating 60 words. These messages were cataloged into groups, with five letters to a group. In one day, over 5000 groups were transmitted.

The network also was linked to a telephone circuit feeding into general headquarters, permitting the use of the entire communications network at any time.

RADIO BROADCASTING'S TWENTY-FIFTH year will be celebrated in 1945 by the entire manufacturing and broadcasting industry. The silver anniversary will be exploited in magazines, newspapers and radio programs. Broadcasts will even feature a special 25th-year musical score. And *Pledged to Victory* will be the keynote of the broadcasts throughout the year.

DISC RECORDING WAS QUITE POPULAR with the USO in 1944. The 3000 units in this country and off-shore bases used 170,000 discs for *live letters*. The servicemen visiting the USO club houses found record playing to their liking too. They used 60,000 playing needles, 8,000 cutting needles and 20,000 new records.

The postwar era probably will see a boom in disc-record buying, according to several disc manufacturers, recently interviewed. The present average of around 130,000 records a year is expected to increase to 250,000 or more. This increase is based upon the general trend toward the manufacture of more combination phonoreceivers. The 6,000,000 record players individually and in receivers, now in use, will probably be more than tripled, according to the recording specialists.

AN INCREASE OF OVER 3,000,000 radio families in 1944 was revealed by the research department of the Columbia Broadcasting System, who recently completed a survey of radio ownership in this country. There are now, according to this study, over 32,000,000 radio families. In 1940, there were only about 28,000,000 radio families. Substantial gains appear in the East North Central, South Atlantic, Mountain, and Pacific areas. In the South Atlantic area, for instance, an increase of nearly a million was noted. The Mountain zone family ownership increased from 901,546 to 1,011,700. A radio ownership percentage of 88.9 throughout the entire country was also revealed. In the New England, Middle Atlantic, Pacific, and East North Central States, averages above 95% were noted.

AROUND 100 MANUFACTURERS ARE expected to make home receivers in the postwar era. Of this group, 40 are newcomers. None but licensed manufacturers (licensed under RCA, Hazeltine, Latour, or Armstrong patents), are included in this estimate.

For there will probably be countless others who will make receivers in one form or another.

Several distributors, instrument companies, and motion picture equipment manufacturers will be found among the new receiver manufacturers. Receivers will be sold through distributors to dealers, dealers direct, and from the factory in some instances.

THAT VITAL DECISION on frequency allocations, probed during the recent five-week FCC hearings, was not made on December 1 of last year, as originally planned. The avalanche of testimony and bids for frequencies buried the experts studying the details and months, instead of weeks, were required to solve all the problems akin to the organization of the spectrum. At the present writing it appears as if a decision might be made during the early part of February.

The State Department, who originally set the decision deadline of December 1, sent their experts over to confer with the FCC to align differences. These experts are members of the Interdepartment Radio Advisory Committee, more popularly known as IRAC. Authoritative sources state that many of the frequency allocations proposed by IRAC during the State Department hearings in August will be included in the new frequency program, a program that will not only establish our domestic wavelength schedule, but our international requirements, too.

A MOVE TO ORGANIZE AN FM station on a cooperative basis was initiated recently in New York City. A group known as the Peoples Radio Foundation, Inc., has been formed to build such a station. Thus far there are 28 sponsors in the foundation. They include such personalities as Rockwell Kent, Corliss Lamont, Samuel Novick, Earl Robinson, Charles Chaplin, and Dr. Robert L. Leslie. Recently the group advertised their activities in the local New York City newspapers, declaring that the establishment of a cooperative FM station will provide 12,000,000 people in the New York area with a powerful voice to serve the community and present the advanced thinking of the times.

TRAIN RADIO is playing an important role in the Ordnance Department of the Army Service Forces. Two-way communication systems between locomotives and a central train dispatching point have been operated with considerable success. Experimenting with the system began a year and a half ago at the Savanna Ordnance depot, between the engineer of a locomotive and the train dispatcher at the depot. Today a number of the depots have this method of communication. A distance of 30 miles is usually covered from the dispatcher's office in the depot to the train.

Colonel L. J. Meyns, chief of the Ordnance Field Service Storage Di-

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FASTER—EASIER AT HOME

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See how DeForest's Training has helped many to good pay jobs in Radio-Electronics—others to preferred military classifications—still others to interesting, profitable businesses of their own. See how you can prepare for a bright future now—in your spare time at home—then get started in Radio-Electronics with the help of DeForest's effective EMPLOYMENT SERVICE.

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**R. F. CONTACTORS
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Johnson R. F. Contactors were designed for switching high voltage antenna circuits in Phasing Equipment and for similar applications. Made in two sizes, these Contactors provide long creepage paths, high current carrying capacity, high voltage rating and no holding current is required. They can be operated on either 110 or 220 volt power circuits. Either size is available with a variety of contact arrangements including auxiliary contacts for signal or pilot light indicators. Contacts are sectionalized to provide large contact area and their wiping action makes them self-cleaning. Write today for more information and quotation giving contact arrangement desired.

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a famous name in Radio

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vision, is so enthusiastic about the effectiveness of the system, that plans are being made to equip most of the 193 locomotives in the field service with radio systems. These locomotives operate over 1137 miles of track. Although most of the locomotives are of the Diesel type, no interference troubles are encountered from the large generating units. The Army engineers report that the eddy currents of the generators do not promote interference.

Engineers of the FCC are studying the progress of these systems, believing that the data collected will serve as a guide toward the appropriation of suitable frequencies for train service in the new allocation program.

TWO-WAY COMMUNICATIONS FOR TAXICABS have now become quite practical. In Cleveland, the Yellow Cab Company recently conducted experiments with a fixed transmitter and mobile transmitters in two cabs. Officials reported that dispatching by radio improved travel efficiency and eliminated *dead miles*. All three transmitters were of the FM type, with 15 watts of power. The fixed transmitter was mounted in the top floor of an office building, about 530 feet above the city.

In view of the success of the experiments, the cab officials have requested permanent licenses. About 400 cabs may be equipped with the two-way systems, if the licenses are granted.

BROADCASTING VIA THE POWER LINES is a feature of an unusual collegiate network, the Intercollegiate Broadcasting System, that may soon offer radio networks lively competition. Established some years ago, the system has many colleges in the New England sector and one in Alabama. The system has proved so popular that many major colleges are planning campus stations. Advertisers have also become aware of the interest in this unique network and have begun to sign options for time allotments.

In most instances, installations consist of a master amplifier in a main studio. This is coupled to an automatic turntable, a microphone and a pair of headphones used for monitoring purposes. Microphone and turntable are arranged so that fades between selections, programs or announcements can be made. The output of the amplifier is coupled by a leased line to a master oscillator amplifier, with an output of from 15 to 20 watts. The output of this transmitter is then fed into the wiring circuit of the campus. To receive it is only necessary to tune in a receiver, either standard broadcast or special type, to a prearranged frequency. The frequency may be low, such as 30 kc, or anywhere in the broadcast spectrum.

The USO featured a similar system for camps. And in some of the military camps overseas, similar systems have been installed.

In the collegiate system, both alter-

nating-current and direct-current lines have been used. In one installation, twelve dormitories are linked together via the direct-current lines. In most cases, however, the secondaries of the a.c. transformers fed by a master transmitter are used. Where the power problems are too complex, radiation methods are used. These include a network of fine wires spread over a college campus to form a low power radio field to within a short distance of all student quarters; similar antennas connected by a transmission line with a master transmitter; transmission lines from a master transmitter feeding power into building radiator pipes and lighting circuits; and audio transmission lines to remote transmitters covering one or more buildings.

Some of the colleges included in the network are: Harvard, Yale, Cornell, Columbia, Brown, Wesleyan, Haverford, Bryn Mawr, Union, and Radcliffe.

THE ENTRANCE OF DISTRIBUTORS into the manufacturing business as an additional enterprise was severely criticized recently by members of the electronic distributors industry advisory committee. Members of the committee pointed out that it was not wise to set up new manufacturing facilities, simply because surplus components were on hand. Such parts should be released by manufacturers or distributors who can put them to excellent use.

To provide wide distribution, WPB is sanctioning the approval of many new distributors. Where the request comes from an area well served, the manufacturers have been asked to make sure that the new distributing outlet will materially aid distribution. In screening the applications, WPB is giving particular attention to locations of the new distributors, and the populations they would serve.

THE PRODUCTS OF TOMORROW exposition, in which radio may play an important part appears to be well on its way. The approximate date of March 1 has been set for the opening. And the Chicago Coliseum has been chosen as the exhibition hall. Those who have postwar products that are reasonably new are being solicited. The show is expected to run for two weeks.

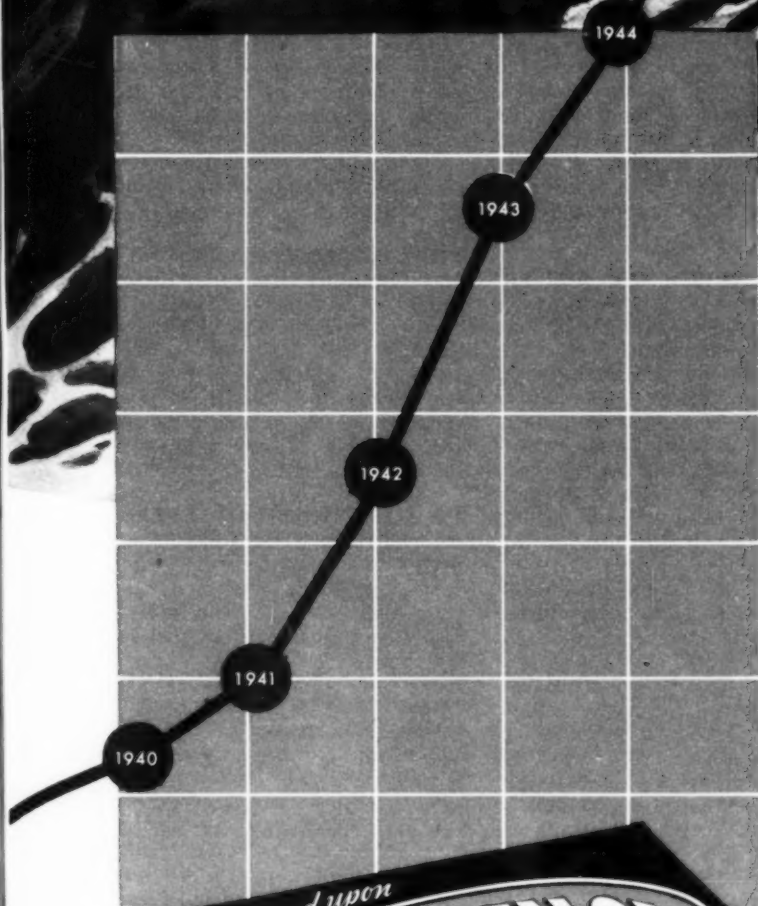
Just how many new types of equipment radio manufacturers will be able to exhibit, will depend on war conditions. Some are planning on special experimental models, only. Others believe that new models will be available for such a showing. The success of the radio part of the exhibit will also depend on whether or not the radio trade show, also planned for the Spring, is held. While some manufacturers would probably hold dual showings, many would probably save all their attractions for their own trade show.

The postwar show topic is also being discussed in England. Some experts

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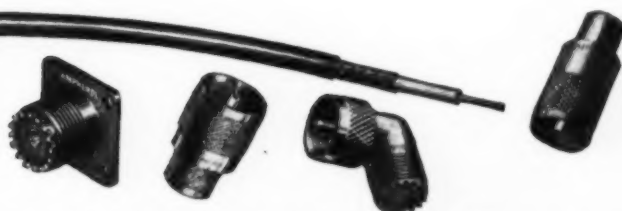
AMPHENOL



● Up to 1940 when war construction began, Amphenol had a long, proud record of achievement in the production of electrical transmission equipment of the better—more critical—kind. Among other "firsts" Amphenol had developed, and built, the first ultra-high frequency cable.

When production for the Air Corps, Army and Navy demanded precision far beyond that of civilian manufacture, Amphenol went to work exclusively for the Armed Forces... will continue working for Uncle Sam until the last bomb burst. When that time comes, the years of experience "under fire", the broadened perspective and knowledge will mean new and improved products, a source of supply of unlimited capacity. This is a rich background of experience in the production of parts for the users of electrical transmission equipment in the electronic, radio and electrical fields.

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SUPREME MODEL 571

- Simple Operation — all ranges read on two basic scales.
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- Electron coupled circuit giving greatest stability. Iron core coils.
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R.F. RANGES:
 65-205 KC; 205-650 KC;
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AUDIO FREQUENCY:
 400 cycles available for external testing.

INTERNAL MODULATION:
 R.F. Carrier modulated at approximately 30% and 70% at 400 cycles. Modulation level selected by toggle switch.

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ACCURACY:
 1/2 of 1% on first three bands. 1% on last two bands.

SIZE:
 9-1/2"x8-11/16"x7-3/8"

POWER SUPPLY:
 115 volts 60 cycles—Special voltage and frequency on request.

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there believe that only when receivers and parts are ready for delivery should any show be held. One well-known distributor said that exposing plans and creating demand is dangerous unless the merchandise is available. Such disclosure and unavailability would permit competition to take advantage. Others say that a general show indicating trend of design and engineering will prove stimulating and helpful. Such a show, they say, would spur interest and create sales when all the models are available. It might even be wise to run a second *ready-for-delivery* show, they say.

Since the original announcement by RMA that a Spring radio show may be held, no further information has been released. However the general feeling appears to favor the trend show, if war conditions will permit.

THE RECENT PROPOSALS for subscription-type receivers, which would permit only those with special receivers or receiver adaptors to listen in, has been frowned upon by officials of the National Association of Broadcasters. Objections to such systems were voiced in a letter filed with the FCC. The NAB experts stated that too few frequencies are available for all the services required and in addition, such a system would prompt interference troubles. Programs of widespread appeal over as many stations as technically possible will provide the public with the variety they require, stated NAB.

INTRIGUING DATA ON SOUND was presented at a recent meeting of an RTPB panel. Discussing the acoustical noise level, members were told that the average acoustical noise level in residences not having receivers operating was 43 decibels (43 db. above accepted threshold of audibility standard which is .0002 dynes per square centimeter). The average difference between summer and winter values was 3 db., according to this report. Measurements made by W. B. Snow of Bell Labs indicated that the maximum sound level required to be reproduced in the home is 80 decibels. Such a level is so great that it is irritating to listeners with average hearing. Most people will readjust the level so that it falls between 66 and 72 decibels. In view of these requirements, reported the sound specialists, the maximum usable dynamic range for reproduction in over 95% of the homes is 80 minus 30 or 50 decibels. This represents the signal-to-noise ratio that a system should provide.

Charts showing the recommended audio-frequency range for high fidelity broadcasting revealed that above 12,000 cycles, noise predominates over musical tones by a wide margin. Above 10,000 cycles, noise still predominates over musical tones. At 9,000 cycles, those instruments which produce noise and those which produce musical tones are equal in number. And at 8,000 cycles, instruments producing musical tones are predominant. At

12,000 cycles, the violin was classified as providing both noise and music; above 9,000 cycles, the violin, bass clarinet, clarinet, soprano saxophone and piccolo were included as those instruments which produce both noise and music. The cello, bass saxophone, bassoon, bass clarinet, clarinet, soprano saxophone, flute and piccolo offered noise only above 12,000 cycles, while above 8,000 cycles, only two instruments, the French horn and bassoon provided noise. At these frequencies, the snare drum, 14" cymbals, trumpet, oboe, and male and female speech provide a predominance of music, while the violin, bass clarinet, cello, bass saxophone, clarinet, soprano saxophone, flute and piccolo offered both noise and music.

Bell Laboratories experts disclosed that observers at the labs listening to speech in special tests could not detect any change until the full audible range was reduced, in gradual steps from 15,000 to 7,600 cycles. No change was observed for musical reproduction until this full range was reduced to 11,000 cycles. Accordingly, the experts agreed that if at above some critical frequency an equal number of *noise producers* and *musical tone producers* may be considered to offset each other, there is little to be gained by using audio frequencies above 10,000 cycles. As a result they therefore recommended 10,000 cycles as the upper limit for high-fidelity audio transmission for FM broadcasting.

THE RECENT NATIONAL bond drive brought one of industry's old-timers . . . Atwater Kent . . . back to the limelight. Mr. Kent, who was quite a radio magnate back in 1925, purchased \$300,000 worth of bonds to engage Arthur Treacher, the screen actor-butler, as a butler for him at a special party. Many radio and screen celebrities attended the party.

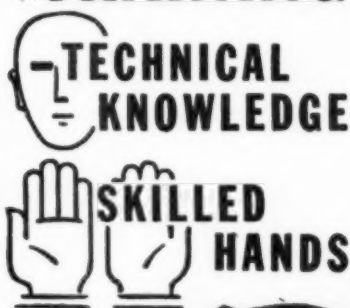
TO GAIN METROPOLITAN RECOGNITION, a station in Brooklyn recently requested that it be permitted to identify itself as of New York. FCC approved the move, wondering though how Brooklyn would feel about it.

THE FACSIMILE SCENE HAS BECOME QUITE ACTIVE these past weeks. Testimony offered by former FCC Commissioner Payne, John V. L. Hogan and other experts at the recent FCC hearings and subsequent engineering meetings seem to have spurred interest. It will be recalled that Mr. Payne, who is now with Finch, advocated the use of multiplexing. He said that entirely automatic record communication for use in the home is available through multiplexing on the band of frequencies assigned to FM broadcasting. Multiplexing operation may also be used on police frequencies, he said, thus meeting the four cardinal requirements, namely, secrecy, orders, finger prints, and identification.

Weather services also could use the
 (Continued on page 136)

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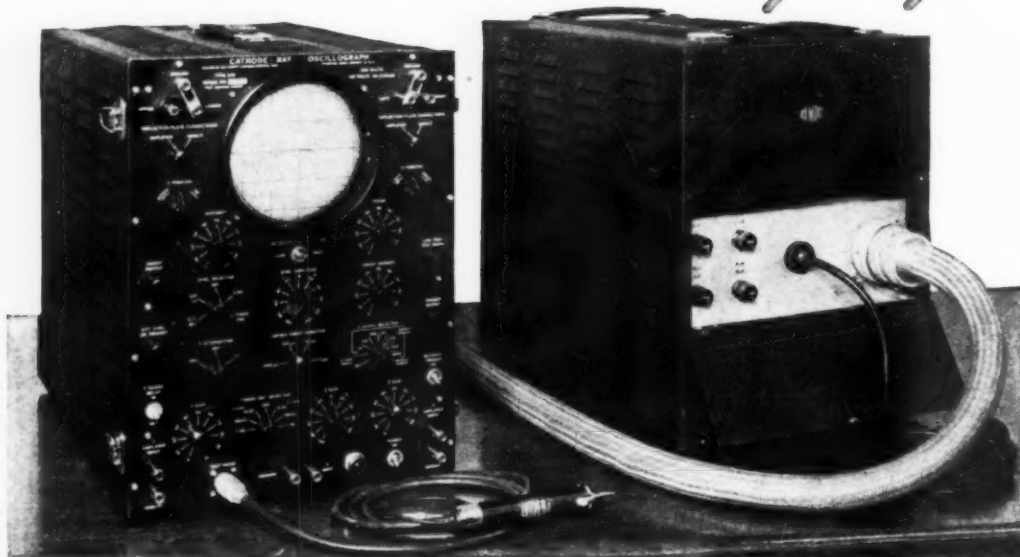
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Wide band vertical axis amplifier usable to 10 MC.

4000 volts accelerating potential applied to cathode-ray tube, allowing observation of fast-writing-rate phenomena.

Extremely flexible time-base generator to display signals which heretofore required special sweep circuits.

Delay network in vertical channel, permitting observation of entire wave shape of short duration phenomena.

Useful timing oscillator for quantitative analysis.

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Optional low capacitance probe input to vertical amplifier.

Convenient mechanical design which permits placing separate power supply on floor or shelf beneath lab bench.

Storage space for all cables provided in

power unit.

Design is such that modifications to standard specs. can be accommodated to special order in the following respects: (1) Driven sweep durations; (2) Marker oscillator frequencies; (3) Trigger pulse rates.

Both metal cabinets, with carrying handles, measure 14"x18"x21" deep. Power supply weighs 80 lbs. Oscilloscope, 30 lbs. Units connected by 6-foot shielded cable. Standard A-N connectors used.

◆ Still another DuMont "first". Incorporating the most advanced features, this latest oscilloscope is now available at moderate cost as a standard commercial instrument. It will be especially welcomed by the investigator heretofore restricted in his work by the inadequate performance or the prohibitive cost of existing equipment.

Type 248 is a portable instrument. Two units facilitate handling and installation. Either transient or recurrent phenomena can be displayed. Also accommodates phenomena of inconstant repetition rate. The leading edge of short pulses is not

obliterated. The accelerating potential applied to the cathode-ray tube is great enough to permit study of extremely short pulses with low repetition rates, usually observed only with specialized and costly oscillographic equipment. Timing markers are available for quantitative or calibration purposes.

In short, this instrument removes the very noticeable deficiencies in commercial test equipment performance brought to light by recent advances in electronic technique. And it is equally useful as a general-purpose or as a production-test instrument.

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from this point on, it's craftsmanship!

In one important respect there is a striking similarity between the millions of Bliley crystals which we now produce and the mere handful of custom made units that constituted our annual production when radio was still young.

In those early days of radio, when each quartz crystal was painstakingly cut and ground by hand, a tradition was born. It was a tradition of craftsmanship that has grown with the years—a tradition that Bliley engineers have successfully translated into the more intricate techniques of volume production.

Etched crystals are an outstanding discovery and development of Bliley research engineers. This technique, by means of which crystals are finished to frequency by acid action rather than abrasive action, was an established part of Bliley production long before Pearl Harbor. It has since proven to be an essential element in the manufacture of crystals that have the dependable characteristics necessary for military communication in global warfare.

We have been called upon to solve

some knotty problems. But that is nothing new at Bliley. It has been our habit to parallel new developments in radio with the right crystal for each application.

Things will be different soon. Peacetime projects will again come first. But our engineers and craftsmen will be ready, as always, with the right answer to your requirements. Don't fail to include Bliley crystals in the component specifications for your peacetime equipment.

Do more than before...

buy extra War Bonds

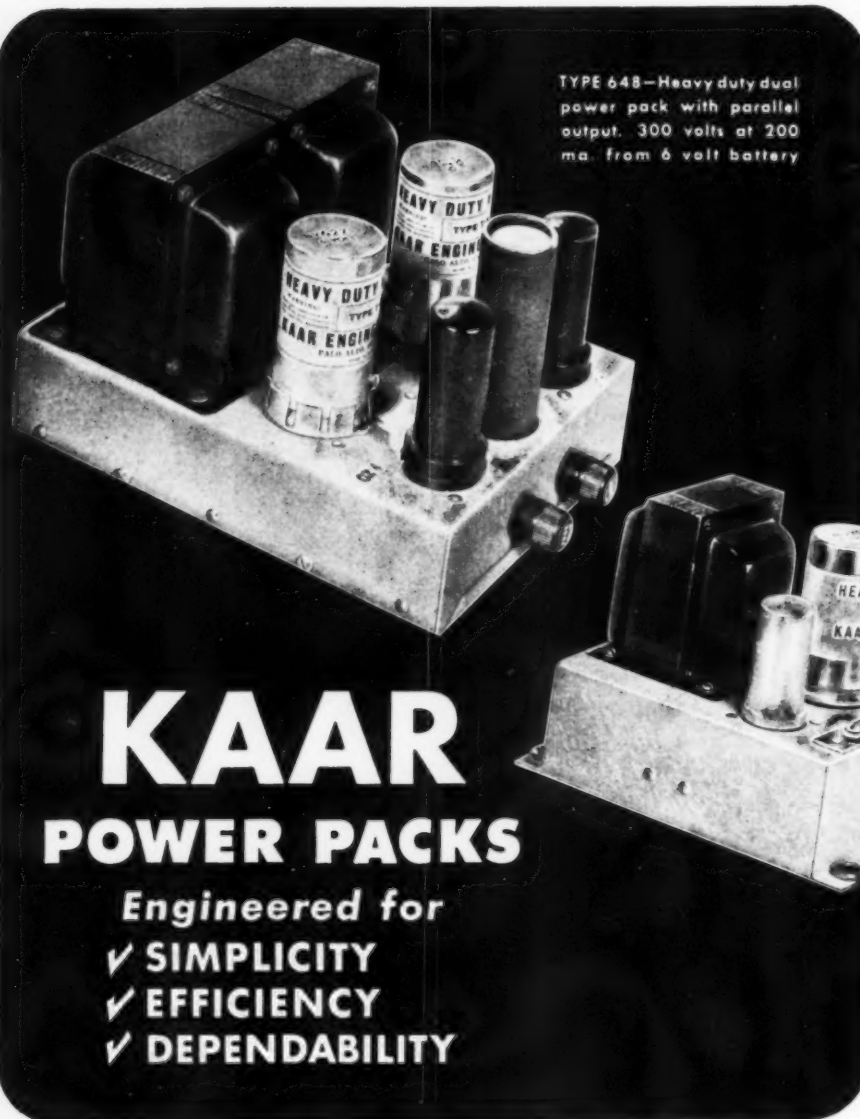


A new star has been added

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BLILEY ELECTRIC COMPANY UNION STATION BUILDING • ERIE, PENN.

February, 1945



TYPE 648—Heavy duty dual power pack with parallel output. 300 volts at 200 ma. from 6 volt battery

TYPE 650—Standard: 200 volts at 50 ma. Optional: 200 volts at 75 ma. This type available for 6, 12, or 32 volt operation. Has built-in filter. Notice simplicity of construction.



TYPE 649—Provides 240 volts at 50 ma. Available at other standard ratings, and for operation from 6 or 12 volt batteries. Type 647, not illustrated, provides 240 volts at 75 ma.

Use this West Coast source for vibrator power packs

Kaar Engineering Company offers prompt delivery of standard and special types of vibrator power packs for operation from 6, 12, or 32 volt sources. In addition, laboratory facilities are available for a variety of power

packs designed to your own specifications.

Take advantage of this convenient West Coast source of exceptionally efficient low-drain packs, designed for simplicity and dependability.

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MOBILE RECEIVERS—Crystal controlled superheterodynes for medium and high frequencies. Easy to service.



CRYSTALS—low-drift quartz plates. Fundamental and harmonic types available in various holders.



TRANSMITTERS—Mobile, marine, and central station transmitters for medium and high frequencies. Instant heating, quickly serviced.

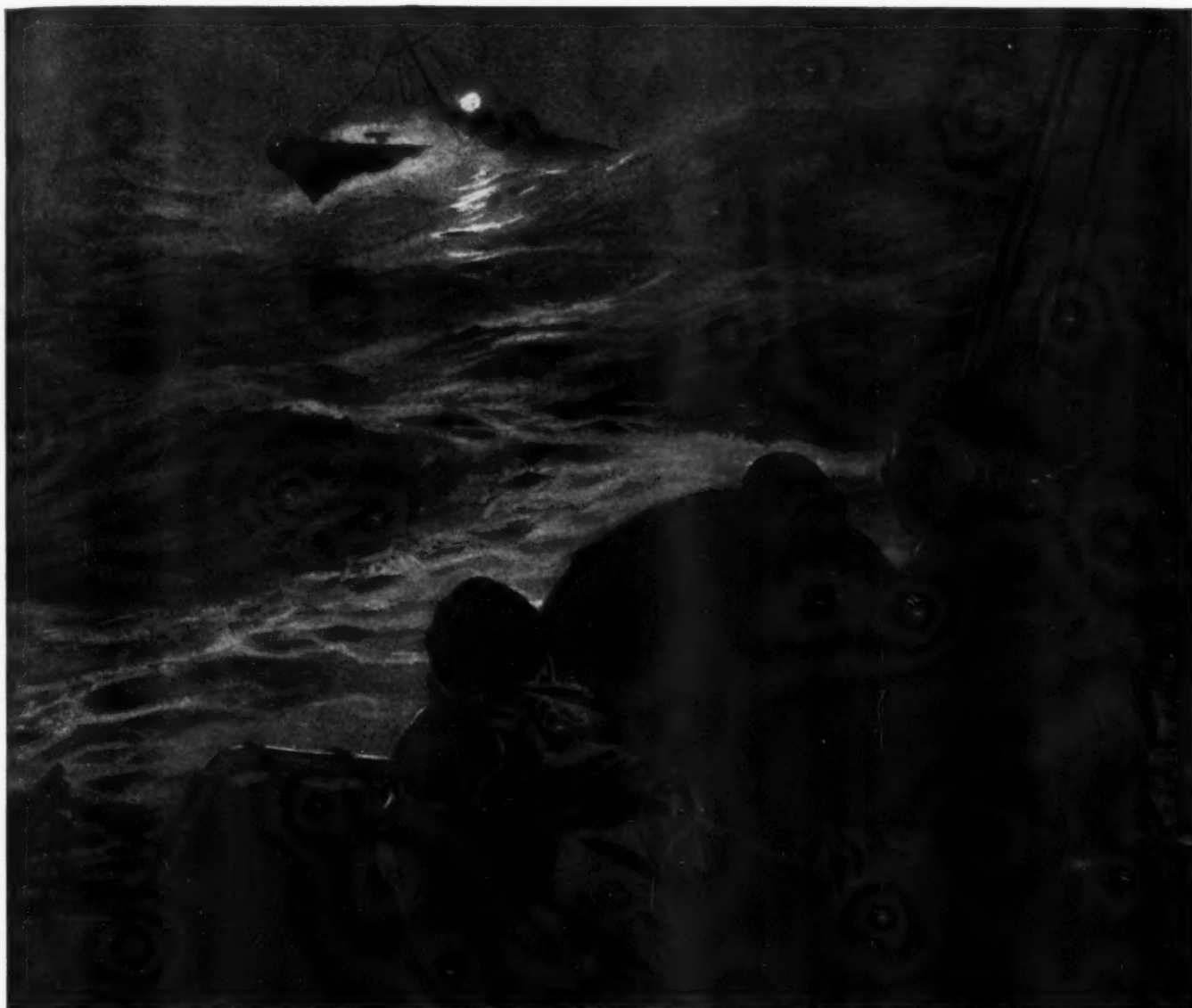


MICROPHONES—Type 4-C single button carbon. Superb voice quality, high output, moisture proof.



CONDENSERS—Many types of small variable air condensers available for tank circuit and antenna tuning.





History of Communications. Number Twelve of a Series

COMMUNICATION BY THE BLINKER



The Blinker, an adaptation of the Heliograph with its own source of light, has been found invaluable for night and day Naval Communications. While limited by "line-of-sight" transmission and the elements of weather, it has been an aid to our cautious convoys during "radio silence."

When Victory is ours and the days of "radio silences" are gone forever, private citizens again will have electronic voice communication equipment for their yachts and other pleasure craft. With the release of civilian radio bands Universal will again offer the many electronic voice components for use in marine craft.

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February, 1945



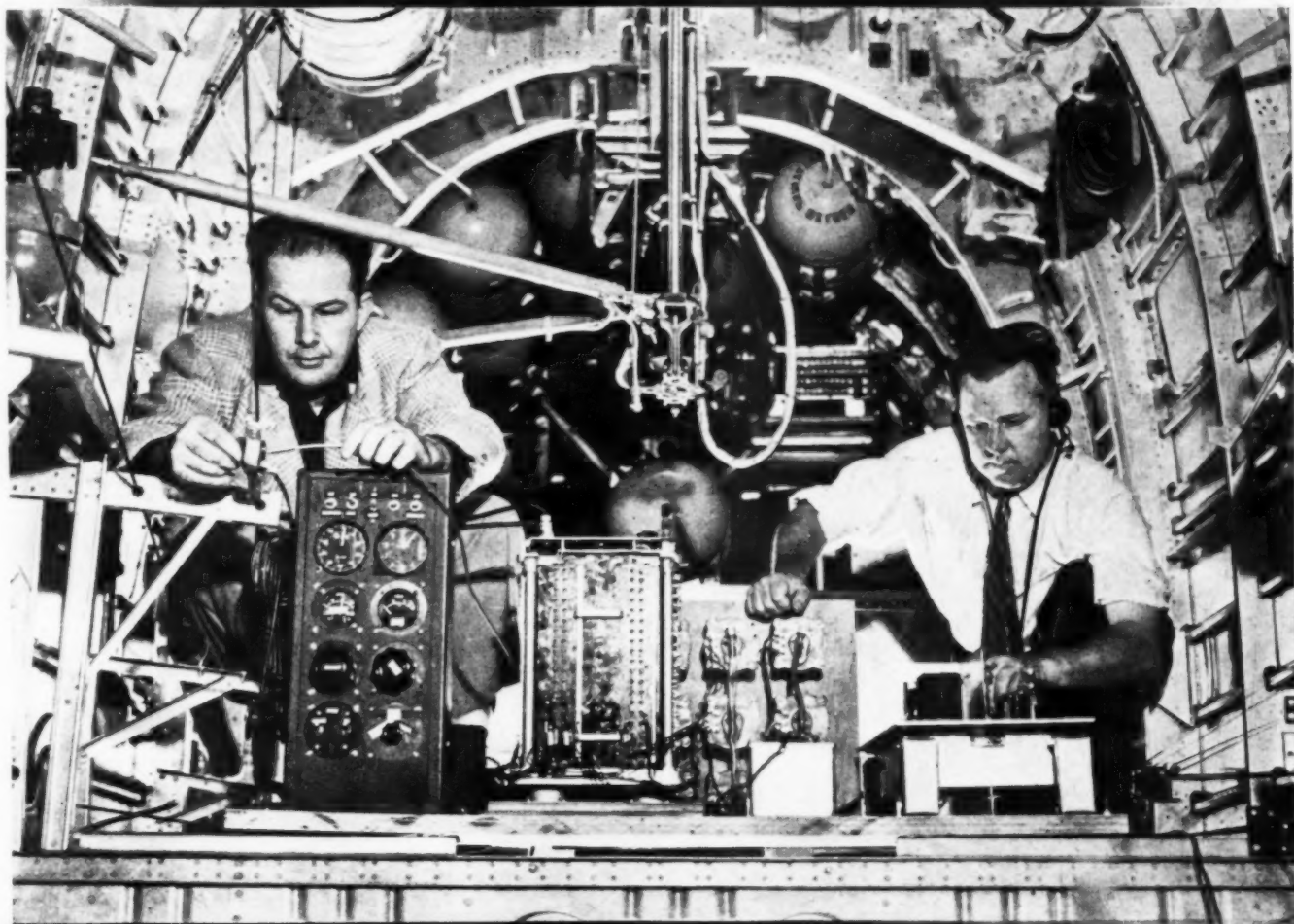
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"Super-Pro" receivers are assisting
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Electronic FLIGHT RECORDER



Engineers of Consolidated Vultee Aircraft Corporation install their new device in the aft end of a Liberator Bomber.

FLIGHT personnel no longer fiddle with pencils, paper whipping in gusty drafts, and temperamental camera equipment when recording the detailed story of an airplane undergoing tests.

In large airplanes, as the Liberator and new Dominator (B-32), it is possible for extra engineering observers to read the dials, gauges and other instruments, and note the results. Pilots flying in the single-seat fighters simply could not fly their airplanes through the many maneuvers and jot down their observations of instruments at the same time. For aircraft, both large and small, means for noting flight test data are essential in order that accurate records not only might be obtained under normal conditions, but which will be available for study should disaster strike suddenly.

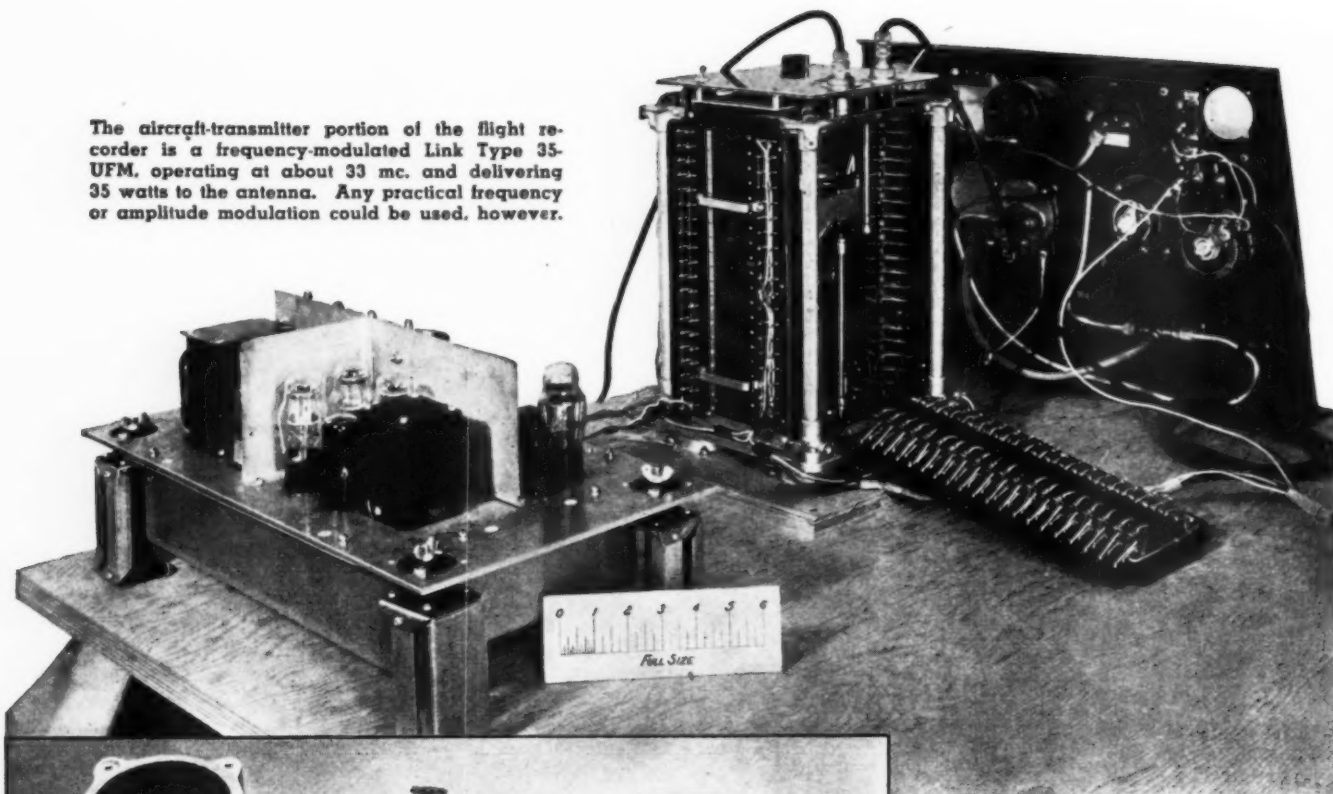
The answer to this need for all types of airplanes is the electronic flight recorder. The flying part of this recorder, developed over a period

of three years, occupies only four cubic feet of space in the airplane, and weighs only 55 pounds; its ground elements, aside from the pickup, occupy a small room. Together, they contrive to give us accurate, instantaneous data. This is an important feature, for it means, should an accident occur, ground engineers probably can determine why.

Were you to inspect the transmission unit in a Liberator, you would note the equipment includes several pickup or gauge devices, so arranged that airspeed and altitude indications, control surface movements, engine revolutions, etc., produce signals which can be transmitted to a conveniently located mechanism through electrical circuits. Each signal has a predetermined travel or range, and varies with the position of the gauge device. As they pass through a high-speed scanning switch mechanism in predetermined sequence, rate of some 80 readings a second, the varying signals

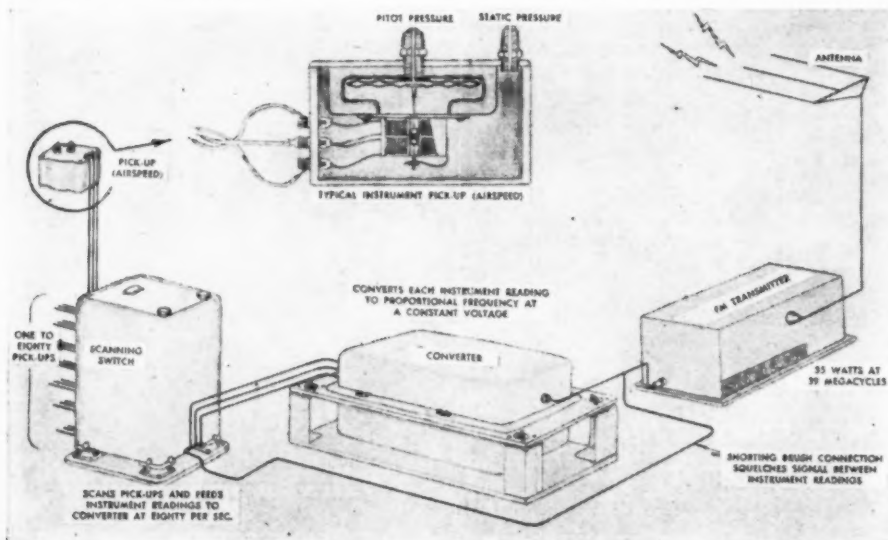
Flight test data for all types of aircraft now is transmitted to receiving stations for observation.

The aircraft-transmitter portion of the flight recorder is a frequency-modulated Link Type 35-UFM, operating at about 33 mc. and delivering 35 watts to the antenna. Any practical frequency or amplitude modulation could be used, however.



Some of the instruments used in connection with the aircraft portion of the recorder.

Schematic shows how the transmission unit functions in connection with airspeed gauge.

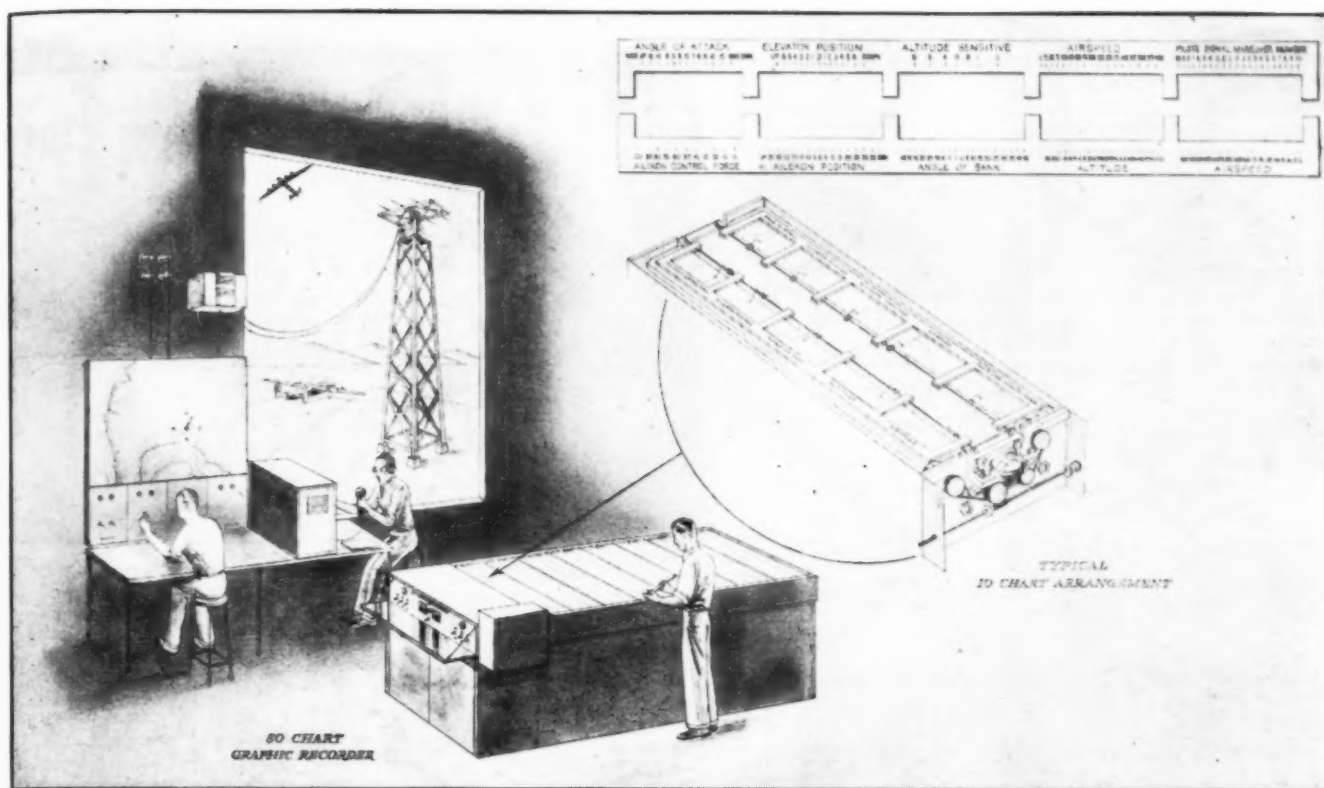


modulate an alternating current in conformity with the gauge indications. Then the modulated alternating current is amplified, rectified, filtered, and used to produce an audio-frequency signal. A small FM transmitter broadcasts the signal.

To record this signal, the ground-based receiver is synchronized with the plane's pickup equipment. On receipt of the signal, the receiver decodes the audio-frequency signal by amplifying and converting it to an amplitude proportional to that of the original gauge reading, then utilizing the proportional amplitudes to record the comparative indications of the gauging devices on individual charts.

This is accomplished by a switch, comprising a rotating arm and a series of contacts, which mechanically interrupts the signal at regular intervals. When the arm engages one of the contacts, a potential, determined by the gauge device in the airplane, is fed into the electronic portion of the recording device. A separate electronic circuit, including condenser and electron tube, is provided for each gauge device.

When the potential is fed into the circuit, the condenser is charged to a negative potential. A potentiometer effects the firing of the electron tubes, and it has a slideable contact arm for each of the separate circuits. Movements of the potentiometer arms are synchronized with the movements of the interrupter switch; and, when the arm for a particular electronic circuit moves around the potentiometer a sufficient distance to pass a voltage to the circuit so as to neutralize the previously-mentioned potential or



Arrangement of ground portion of flight recorder. Charts provide performance data on aircraft during test flights.

charge on the condenser, the electron tube fires. This action energizes an additional portion of the circuit and causes an electric pen or stylus to make a mark on the special recording paper, which reacts to a passage of current.

The pens move continuously along a track with a wire trolley for contact with their respective circuits. Each pen circuit is actuated at a specific time during its movement across the recording paper; therefore, the potential originally applied to the condenser from the impulse source definitely determines the location of the pen at the time it is energized. The marking pen circuit depends on the firing of the electron tube for its operation, and it acts independently of all other circuits, arriving at the zero point of its operation as a contact associated with the circuit commences its travel on the live portion of the potentiometer.

Marking paper in the recording unit is fed between rollers so that marks will be made by the pens at definite intervals, according to the time that elapses between impulses at the transmitter. This makes it possible to place time lines on the paper, and allows the plotting of two-dimensional graphs with time and position or their ordinates; thus, ground engineers can obtain true reproductions of the movements of gauging devices in the airplane. The graphs can be calibrated readily in terms of airspeed, altitude, positions of control surfaces, etc.

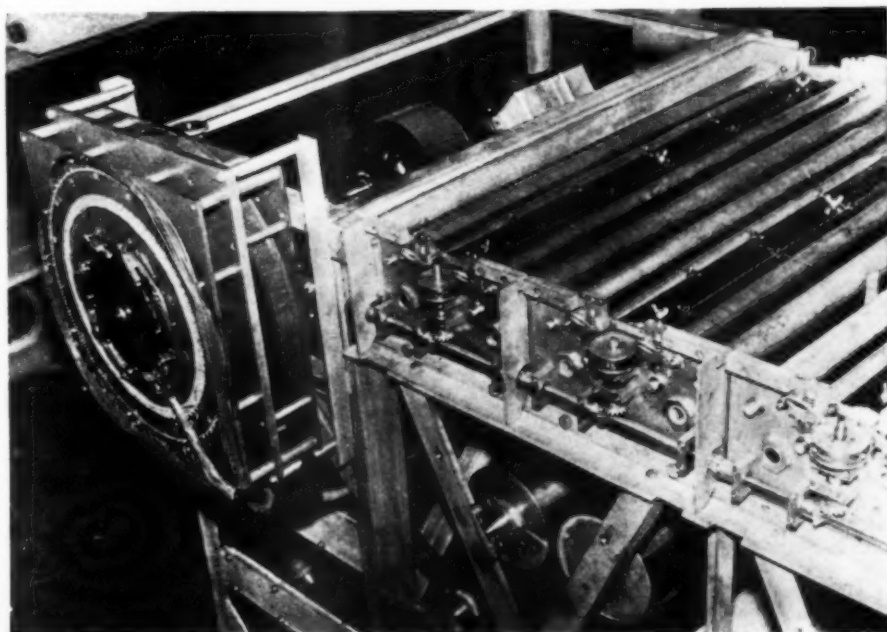
Except for the tachometers, which utilize direct generation, all instruments used in connection with the flight recorder are operated on an

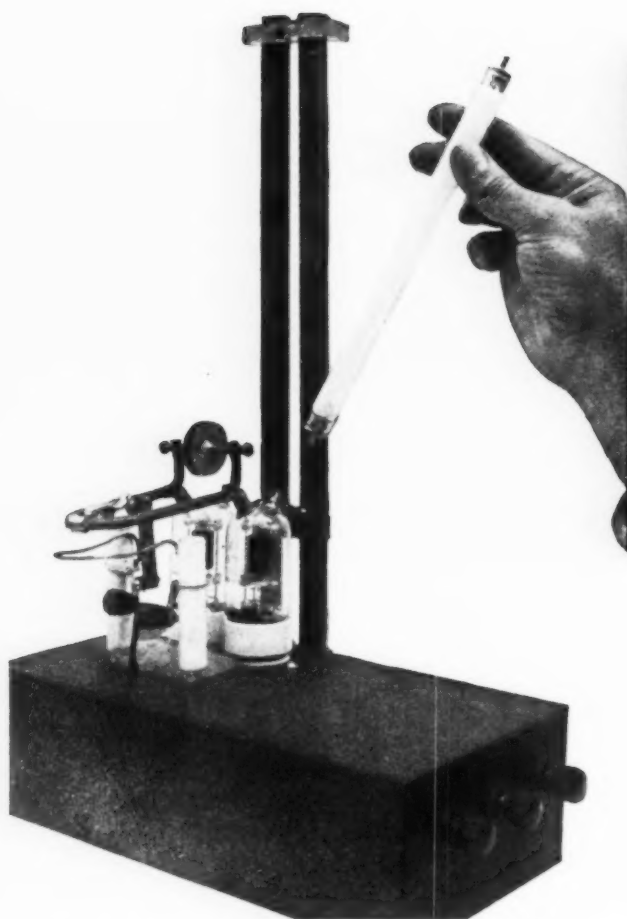
alternating-current bridge principle. The bridge units are divided into three classes: potentiometer, strain gauge, and reluctance bridge. The potentiometers are used primarily for position indicators, as in connection with control surfaces. Normally a 100- or 200-ohm potentiometer is shunted to give the desired range of "off balance." The strain gauges are of the conventional wirewound types,

except that each has a resistance of about 20 ohms. The reluctance bridge is a new-type instrument, specifically developed for use in connection with the flight recorder and may be described as follows:

Two coils are wound, side by side, on a hollow copper or aluminum tube. The coils are about $\frac{1}{8}$ " wide and $\frac{1}{8}$ " deep, and the tube has a
(Continued on page 80)

Ground-based receiver unit is synchronized with the pickup equipment in the plane during flight test, so that it can decode the audio-frequency signal by amplifying and converting the signal to an amplitude proportional to that of the original gauge reading. It then utilizes the proportional amplitude to record the comparative indications of the gauging devices on individual charts.





Showing details of oscillator with a 6-watt fluorescent lamp being used as a radio-frequency indicator.

TRANSMISSION LINES AT 200 mc.

By THOS. A. GARRETSON

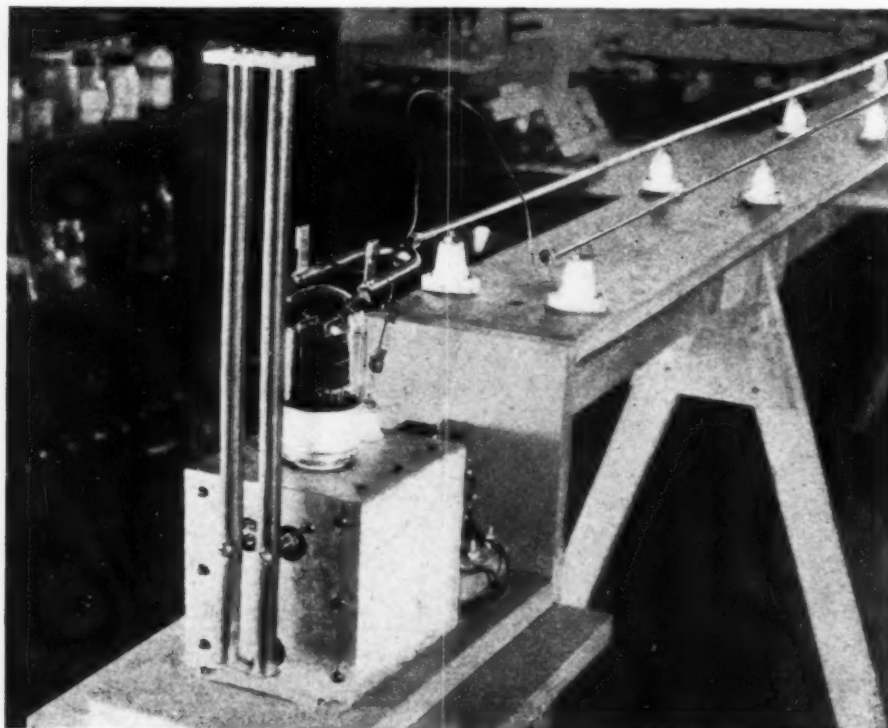
THIS is not really a story about transmission lines at 200 mc. only, but applies as well to lines at any frequency. There are no exceptions to this but there are cases where physical realization is impossible. For instance, at 200 mc. a quarter-wave section of line would be 37.5 cm. in length whereas at 60 cycles the same section would be several hundred miles long. So you see that when we attach such a section to a meter it is quite possible at 200 mc. and utterly impossible at 60 cycles.

The transmission line is generally understood to be the connecting link between a source of power and the load which consumes the power. It has, however, when the physical dimensions allow, several other important uses—it can be used as an impedance transformer or as an impedance matching device; also as a phase shifting element and as a Lecher system for measuring wavelength; it can be made to look like a capacitor or an inductor. It is our purpose to show how some of these applications may be utilized.

In order to investigate these phenomena, we constructed an oscillator which would give us a frequency of about 200 mc. or a wavelength of 150 cm. and having an output of 10 to 15 watts. This frequency was selected because it would allow us to build a transmission line several wavelengths long and still keep it down to a reasonable size. For those who may wish to duplicate this work, Fig. 2 is shown giving details of the oscillator's construction.

The plate supply was a standard full-wave rectifier and filter using a type 80 tube. A variac control was used in the primary of the high-voltage transformer thereby making the output completely variable. For a variable power-supply 0-500 volts makes

A single dual tube was used in this experiment to study the effects of transmission-line operation. This oscillator is not identical to the one described in the article.



A general discussion of the basic characteristics of transmission lines — written in a simple, concise manner for the less-skilled junior engineer.

a nice unit for general use. If it can not be made variable 300-350 volts is about right. The no-load plate current for our oscillator was about 50 ma. and at full load, 100 ma.

For reasons of stability and durability, 3/8-inch brass tubing was used as conductors of the transmission line (Fig. 7). These were spaced 1 1/2 inches apart and mounted on standoff insulators using as little metal as possible. The antenna end of the line was drilled and tapped to receive the dipole while the oscillator end was fitted with binding posts.

It is desirable to know the characteristic impedance of the line for matching purposes. This impedance may be thought of as the impedance of a unit section of line taken at any point and looking in either direction. It is designated as Z_0 . Numerically it may be found from the dimensions of the line and is:

$$Z_0 = 276 \log \frac{b}{a}$$

where b is the center to center spacing and a is the radius of the conductors. Any units may be used for a and b .

Applying this to our line we have

$$Z_0 = 276 \log (1\frac{1}{2} \times 16/3)$$

$$= 276 \log 8$$

$$= 249.2 \text{ ohms}$$

Other means are available for determining the characteristic impedance when the above can not be used. This might apply to telephone and power lines. It may be well to point out again that the same rules apply to all types of balanced two-wire lines regardless of the frequencies they carry. They also apply as well when the line connects a transmitter to an antenna as when it connects a receiver to an antenna.

Measuring Devices

To make measurements on telephone and power lines, we have the usual a.c. instruments and no difficulty is experienced but when we try to make those same measurements at ultra-high frequencies the problem is different. The region of 200 mc. and beyond approaches what might be known as electrical fantasia. For instance, a wirewound calibrating resistor takes on the appearance of a radio-frequency choke and the familiar resistors used in radio sets may behave like inductors or capacitors. Under certain conditions copper wire will act like an insulator and with microwaves in wave guides the dielectric may take on the dimensions of a conductor.

If we put a series meter in a u.h.f. circuit, we may be adding an inductance or a capacitance and we have no easy way of finding out what or how much we have added. All we know is that our readings are worthless because the added impedance changes the values on the line. Our only hope at present with ordinary equipment lies in using shunt measuring devices of maximum impedance to the frequency being considered. This means that our indicating devices will be in the nature of voltmeters.

Fortunately, we have such a device. A little later you will see that a quarter-wave section of a transmission line, which is shorted on one end and open on the other, offers a very-high impedance looking into the open end.

Strange as it may seem, the shorted bar used to short circuit one end of

the line is not really a short at 200 mc. In other words, a voltage may be developed across it. This voltage may be rectified as shown in Fig. 3, by using one of the crystals of "crystal set" days, and the resulting current may be read on a sensitive d.c. ammeter. A 200 microammeter is a convenient size but a 1 ma. meter will meet most of the requirements. A very desirable feature of this device lies in the fact that these crystals are sensitive to frequencies far beyond 200 mc.

Figs. 3A and 3B show the similarity of the low-frequency a.c. voltmeter and the u.h.f. voltmeter. The low-frequency type cannot be used at high frequencies because of the characteristics of the rectifier. Ordinary crystals such as galena and silicon do not rectify linearly so a calibration curve

Fig. 1. A Weston thermocouple ammeter (meter B) being used in exploring the transmission line between stub and antenna.



Testing to see whether matching stub has been placed properly to eliminate standing waves, using meter B mentioned in text.



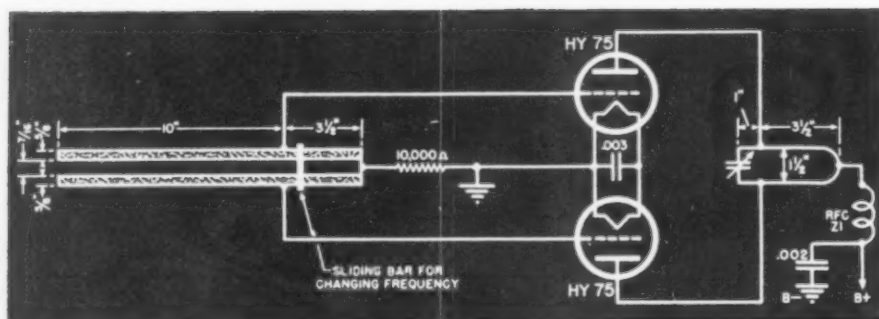


Fig. 2. Diagram of 200-mc., 10-15-watt oscillator. The plate tank coil consists of a quarter-inch copper tubing bent into a U-shape, as shown in the diagram. The plate tank condenser, known as a neutralizing condenser, is 1 1/2 inches in diameter.

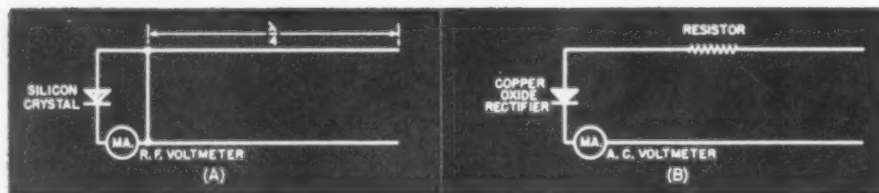


Fig. 3. Method of measuring voltages in u.h.f. circuits (A), and low-frequency circuits (B). It is impossible to use the low-frequency-type meter at u.h.f.

must be made for the crystal used. The method of doing this will be given later. In order to refer later to a meter of this type (shown in Fig. 3A), we will call it meter A.

Another type of meter useful in this work is the thermocouple ammeter. We used in this investigation a 425 Weston, 115 ma. full scale, having a linear scale reading 0-100. This usually is known as a current-squared galvanometer since its readings depend on I^2R . These meters require a correction for high frequencies. We also will use this meter with the quarter-wave section to measure relative voltages. This meter is shown in Fig. 1 and will be referred to later in the article as meter B.

The final type of meter used is a voltage device which is placed near the line, but not in contact with it. It consists of a series circuit containing a 0-1 ma. milliammeter and crystal attached to a probe of variable length. The probe is made variable so that the sensitivity of the device may be changed and also so that it may be used at other frequencies. Used as a

detector it will give some idea as to the amount of radiation from an antenna. This meter shown in Fig. 4 will be referred to later as meter C.

Neon and fluorescent lamps may also be used with good results if sufficient power is available. The fluorescent lamp is especially good for demonstrating voltage conditions on an antenna or transmission line before a large group of people because it can be seen at a greater distance than a small meter.

Open Ended Line

The beginner, trying for the first time to get an understanding of transmission line theory, is very likely to get confused with what appears to be contradictions to all he has learned before. If he will but use what he already knows plus a little logic as he reads the next few paragraphs, he should come up with clear-cut notions of transmission line phenomena. Let us begin by considering an open-ended line, several wavelengths long as shown in Fig. 8, and see what we can find out about it when it is connected

to a source generating sine waves

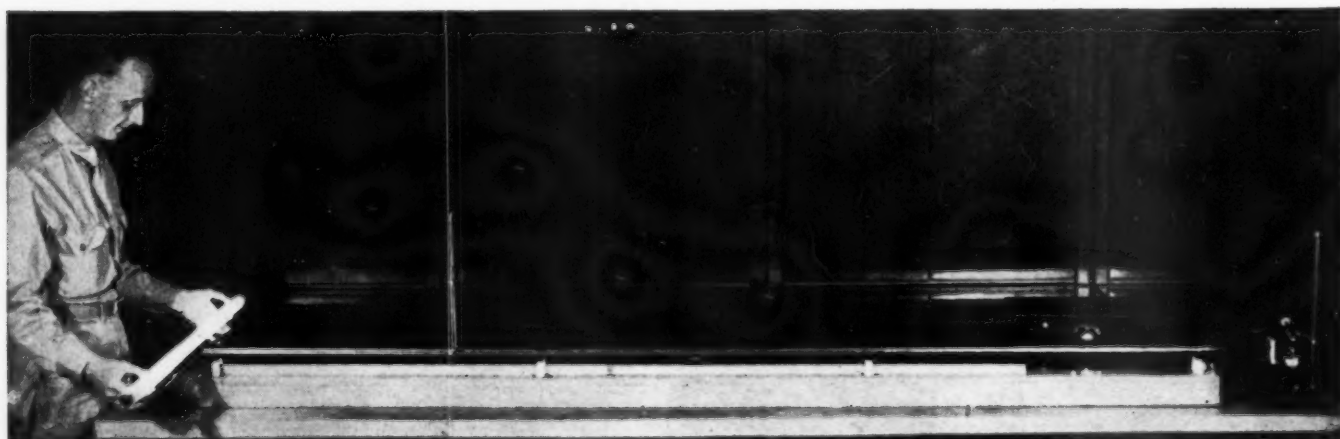
Since the line is open, the impedance at the receiving end must be a maximum and by the same reasoning, the current must be a minimum. Applying Ohm's Law, we find that the voltage must be a maximum. In trying to figure out the nature of the impedance, we find no inductance at the end of the line but we do have the capacity effect of the two conductors. We conclude from this that the impedance is a high value of capacitive reactance. We now know the conditions (neglecting end effects) existing at the end of a two-wire transmission line.

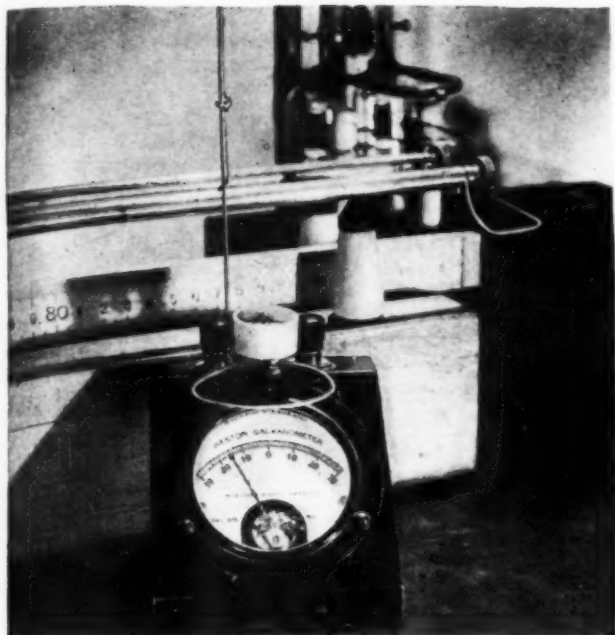
Next we will review the nature of standing waves. A standing wave is produced when the wave from the sending end arrives at a change in character of the conducting medium. This causes all or a part of the energy in the wave to be reflected back toward the source. This gives us two waves on the line and what we read on meters applied to the line will be the resultant of the two waves. If the original wave was sinusoidal, the resultant or standing waves will be sinusoidal but of greater amplitude. This is to be expected since the resultant wave is the sum of two waves and hence must be greater than either one. The condition which might not have been expected but which is nevertheless true, is that the standing waves produce maximum and minimum values at the same place with respect to the end of the line regardless of the length of a finite line. This makes them appear to stand still.

We can now go back to our transmission line and apply this knowledge. We know what the end conditions are and we have found that the standing waves will be sinusoidal. We need know no more in order to determine what is happening on the remainder of the line. We must make one justifiable assumption and that is that the current is 90° out of phase with the voltage, since our line approaches the "lossless" case.

Let us now examine the conditions at a quarter wavelength from the receiving end. We find that the values of voltage, current, and impedance

Using fluorescent lamp to show that proper placing of a matching stub on a transmission line increases power fed to the antenna.





Showing details of generator or sending end of the transmission line. One version of meter A also is shown.

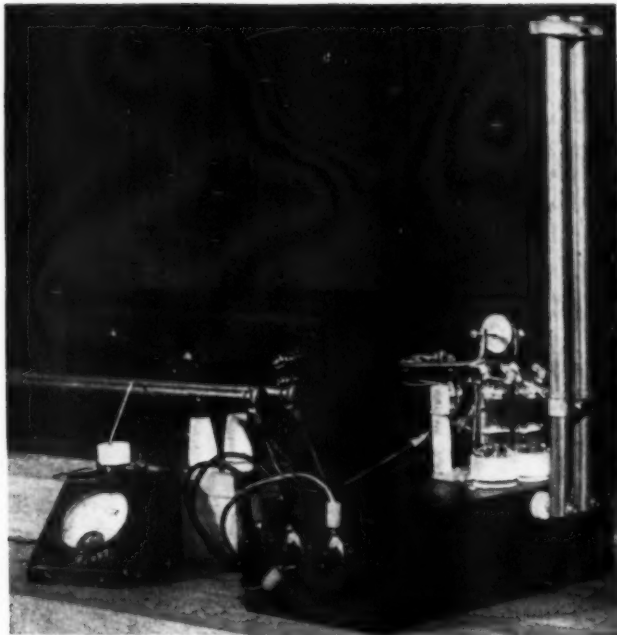


Fig. 4. A 1-ma. ammeter with crystal and variable length probe (meter C) may be used to measure voltages at u.h.f.

have all shifted 90° . This gives us a minimum where we formerly had a maximum and vice versa. We could continue this line of reasoning throughout an entire wavelength but it may be clearer if shown as in Fig. 9A. We know that the current and voltage vary sinusoidally and are 90° out of phase. This could be represented as shown in Fig. 9B.

What about the variation of the impedance? That also can be reasoned out from the knowledge we already

have. We know that $Z = \frac{E}{I}$ and that

E is the sine of some angle. The current being 90° out of phase therefore can be represented by the cosine of the same angle. That gives us a clue to the impedance for by trigonometry $\sin \frac{E}{\cos I} = \tan \frac{E}{I} = Z$. In

other words the impedance variation follows the tangent curve and may be shown as in Fig. 9C.

The impedance at ab, as we see from Fig. 9C, is a low value of pure resistance. But if we look from the open end toward the short circuit it looks like an open circuit or at least an impedance which is a resistance of high value. Here is the case where copper conductors can look like insulators. If we wish to look in the open end and see an open circuit we must use a half-wave section of line. From all this we see that we can get any value of impedance, either inductive or capacitive, by selecting the right length of line. For capacitive values we must use not more than a quarter-wave section while inductive values fall between the quarter and half-wave section, all values repeating themselves every half wave.

To get a picture of the conditions on the line when it is short-circuited at

the receiving end, refer to Figs. 9B and 9C. The end of the line will have shifted 90° to the left and is at the point marked $\lambda/4$. All the wavelength designations shift $\lambda/4$ to the left, all other values remaining the same. The end conditions then become: voltage, a minimum (which is to be expected since the line is shorted); current, a

maximum; and the impedance is a value of pure resistance which approaches 0. All of this is very logical.

Line with Other Terminations

What happens when the line is terminated in some impedance other than those mentioned? Loading the line

(Continued on page 90)

Fig. 5. (A) A method of determining whether the transmission line is properly matched to the load. The line is assumed to be matched when the ammeters read alike. (B) To properly match an antenna to a transmission line, the point of connection can be varied, as shown, until proper match is obtained. The total length of the antenna, including matching section, should be $\frac{1}{2}$ wave or an odd multiple thereof. (C) Another method of matching an antenna to a transmission line is known as delta matching. Total length is $\frac{1}{2}$ wave or an odd multiple and spacing is correct when the ammeter shows no variations along the line.

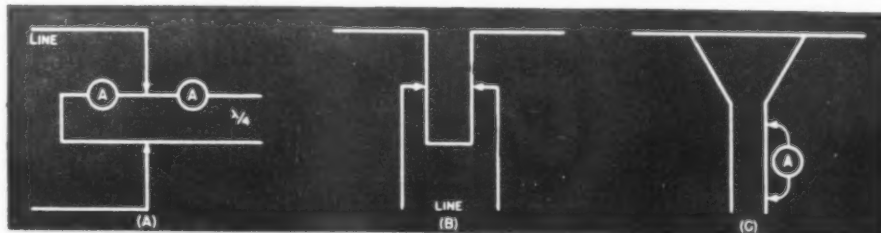
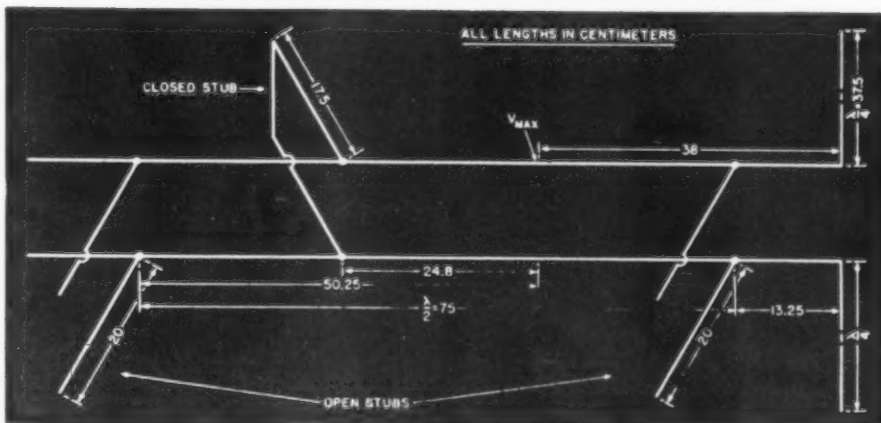


Fig. 6. Results obtained in actually determining the position of the shorted stub when matching a transmission line to an antenna.



Electrical Computing Airborne

Gunsight

By **RUSSELL H. LASCHE**

Director of Engineering and Research
Fairchild Camera & Instrument Corp.

This automatic electrical airborne gunsight takes into account the many variable factors, such as range, altitude, airspeed, angular velocity, etc., which affect the flight of a bullet.

Fig. 1. The computing gunsight with its four components disposed in a revolving upper turret of a bomber. The gunner sits behind the sight component (top), with his foot on the pedal (bottom). Before action he sets three dials on the control panel (just above the foot pedal), recording the altitude and speed of his own ship and the wing span of the target plane (after he recognizes the type). Then he looks through the sight itself—a circle of orange light with a dot in the center. Using the foot pedal to regulate the circle's size, he frames the target from wing tip to wing tip in the circle. The machine then instantaneously makes all the necessary computations; all the gunner has to do is press the trigger. The fourth component of the K-8 is the power unit, nestling out of the way under the gunner's seat (right of the foot pedal).



“YOU may never get the chance again—don't miff it!” The words are underscored in the aerial gunner's handbook. In the case of the man who rides in the important top turret of a bomber this job of perfect marksmanship is no longer a matter of trial and error. Guesswork and the undependable human element now are being taken out of his gunfire by an instrument which has been called the “electrical brain,” the Fairchild K-8 Gunsight. Taking into account the many factors which affect the flight of a bullet: range, altitude, air speed, angular velocity, etc., is no longer his responsibility; the K-8 computes them electrically and instantaneously. All the gunner has to do is keep the target within the gunsight's reticle. The instrument does the rest, turning factors into voltages and voltages into mechanical action which gives the guns the proper aim-

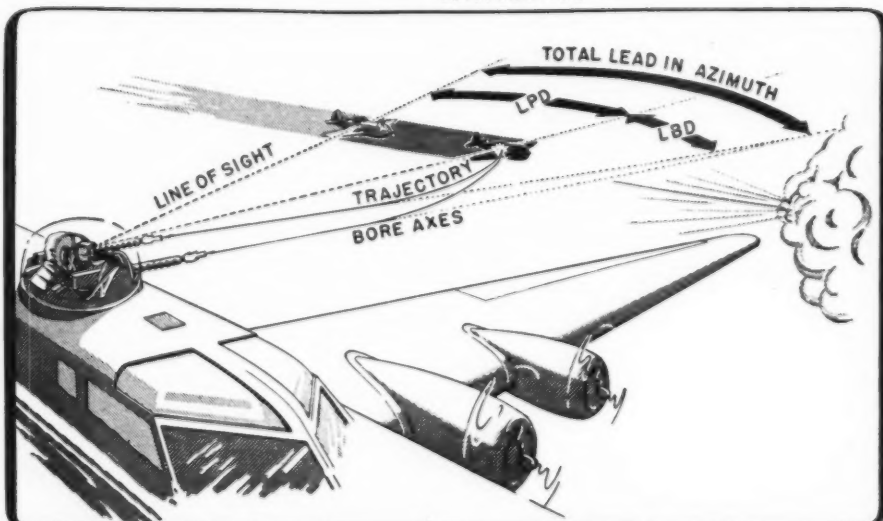


Fig. 2. The Total Lead in Azimuth which is electrically computed by the gunsight.

ing point. Result: rapid and difficult aims now end up in bull's eyes and more enemy planes are getting shot out of the sky.

What the Sight Must Do

Accuracy and effectiveness of a gun-sight depend on the accuracy of the compensation it imparts to the flight of the bullet. To determine this compensation a large number of quantities have to be added, subtracted, and multiplied, and the more factors involved in the instrument's calculations the more accurate are the results.

The final correction given by the sight to the angle of aim of the guns is called Total Lead. This is broken down into two component parts or compensations: Ballistic Deflection and Prediction Deflection, each of which works both laterally and vertically. Fig. 2 shows Lateral Prediction Deflection (LPD) and Lateral Ballistic Deflection (LBD), which add up to Total Lead in Azimuth; Fig. 3 shows the same in the vertical plane. LPD and VPD compensate for the relative velocity between the target and the bomber and are determined from the product of angular velocity and time of flight of the projectile. Time of flight in turn depends upon the following five factors: azimuth position of gun, gun elevation, range of the target, indicated air speed of the bomber, and altitude of the bomber. LBD and VBD are the lateral and vertical corrections for the effects of windage, gravity, etc., on the flight of the bullet. They, too, depend on the five factors listed previously, but since there is no exact relationship between ballistic deflection and time of flight, the same factors must be computed separately.

The mechanical computing systems that preceded the electrical were unable to take in all the factors involved. Indicated air speed and altitude, for instance, were left out and only two of the remaining factors could be used at a time in a given computation. With the electrical computer all variables can be included. Another advantage is its instantaneous action, of obvious importance when it comes to dealing with target speeds of 300 or 400 miles an hour and bullets traveling at 2,700 feet per second. Also, it is not affected by wear, as is the mechanical sight. In the latter there are many gear systems whose teeth eventually become eroded through

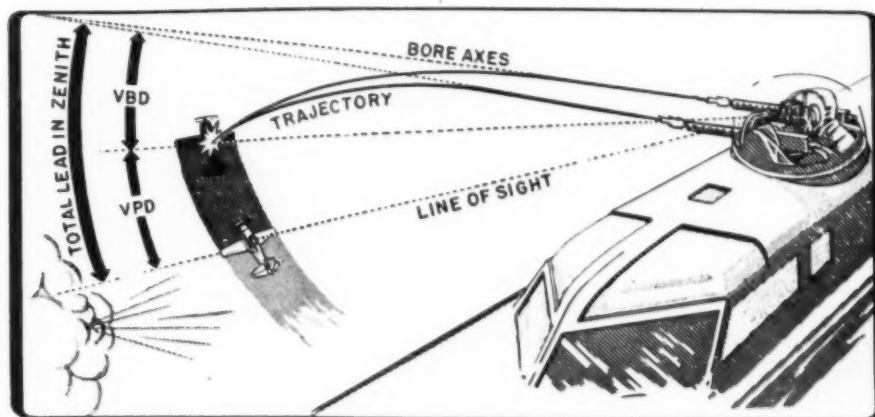


Fig. 3. The Total Lead in Zenith which is electrically computed by the gunsight.

friction and lose their smooth interlocking, with consequent backlash and necessity for adjustment. Lastly, the various component parts of the electrical gunsight, with their connective wiring, can be disposed in the gun turret wherever is the most convenient for the limited space—under the gunner's feet, beneath the seat, or between his knees, leaving only a small piece of equipment in front of his face for greater visibility. Fig. 1 shows the equipment mounted in a gun turret.

The K-8 gunsight, whose development started in 1938 in the laboratories of the Fairchild Camera & Instrument Corporation of New York, and which has been in use by the Army Air Forces for several months, is the only American-born electrical instrument of its kind. Shortly after its appearance the British also put out one, developed apparently inde-

pendently but containing the same principles. Known as the Mark 2, it is being manufactured on contract by three American companies. The Army calls it the K-15 and the Navy the Mark 18. The advantage the Fairchild instrument has over the British is that the latter, for the sake of simplification, gives only the approximate relationship of the variables involved, whereas the K-8 has achieved with success the whole line of calculations down to the most minute.

Construction

The K-8 gunsight is designed to furnish proper aiming point at ranges from 150 to 1350 yards. It weighs 95 pounds and consists of four units with their electrical cable assemblies and flexible drive shafts.

1. *Sight Head.* This contains the optical system, the sight offset motors

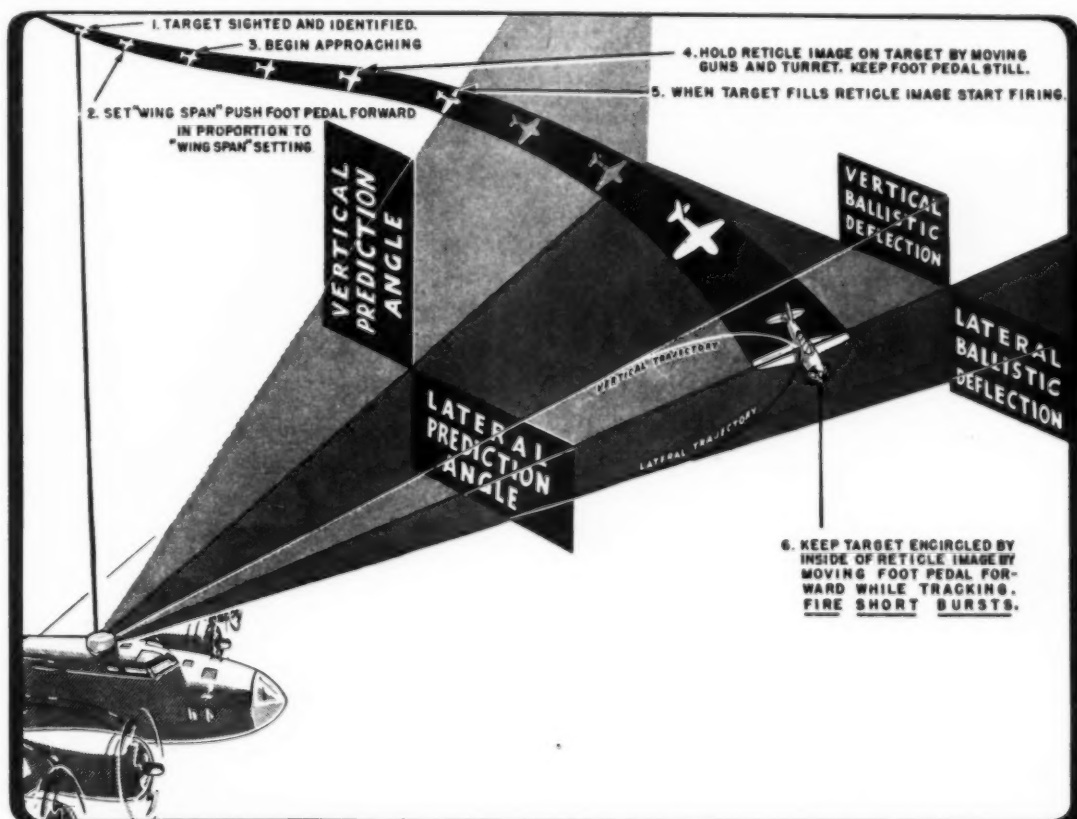


Fig. 4. Illustrating the proper procedure for gunner to follow in firing when employing this gunsight.

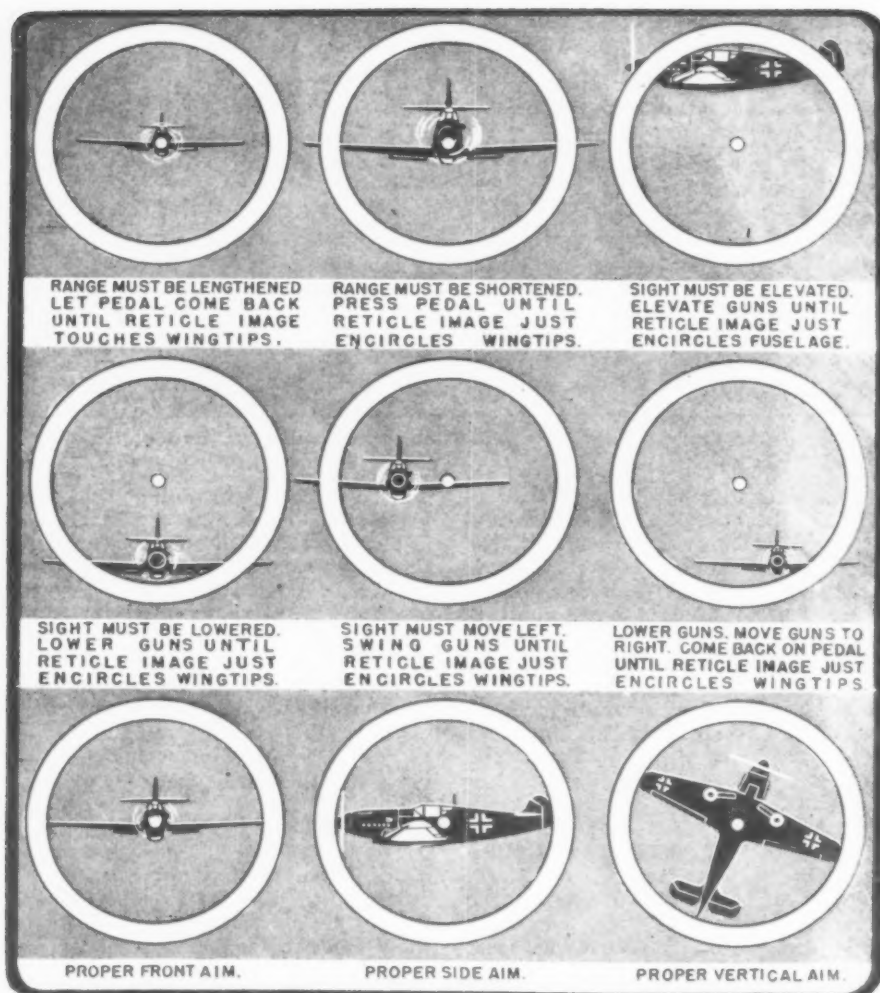


Fig. 5. The optical system of this gunsight employs a solid ring of light in which the gunner keeps the target encircled. Proper aiming procedures are presented.

and the auxiliary generators. It is an electromechanical and optical apparatus for approaching and tracking the target, optically determining range computation and automatically offsetting the line of sight of the guns. It is mounted on a yoke connected by means of a linkage system with the gun elevator sector so that the whole unit can be elevated and depressed

along with the guns. To provide for lateral deflection the sight rotates in its mount which in turn pivots in the yoke for vertical deflection.

Principal part of the optical system is the solid ring of light in which the gunner keeps the target encircled, as shown in Fig. 5. This solid ring is a Fairchild innovation. In some sights the range finder has consisted of two

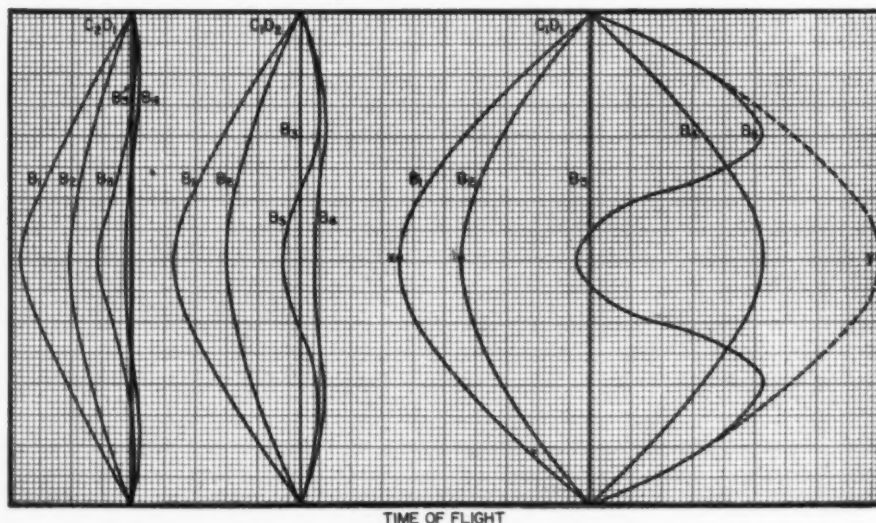


Fig. 6. Three sets of curves that are the result of flight tests and computations, both theoretical and practical. Electrical network is designed from these curves.

vertical lines which could be adjusted in spacing. Here it was difficult to determine the proper range unless the target was horizontal. For other range-finders a ring of dots has been used. This had the disadvantage that, for mechanical reasons, there could be only an odd number of dots (7 or 9) and since there were never, at any time, two dots opposite each other, it was again difficult to estimate the range. The Fairchild solid ring obviated all these difficulties.

There are two motors for offsetting, one for lateral deflection and one for vertical. An auxiliary generator is provided on the same shaft as the lateral deflection motor and is a special feature of the Fairchild K-8. Its function will be described later.

2. *Computer Unit.* The computer unit is mounted between the gunner's knees, unobtrusive and yet with the controls within easy reach. This unit contains the attenuator network whose function is to solve the problem of computation and give the correct electrical answer in the form of the right voltage for each given condition. It also contains reversing switches and velocity generators—the latter connected by flexible shafts with the turret gearing. All controls are indirectly lighted, the brilliance of the illumination controlled by a rheostat. This permits use of the unit under any lighting conditions, which is especially important at night when artificial lighting must be reduced to an absolute minimum so that visibility may be retained.

3. *Power Supply Unit.* The power supply unit, which is under the gunner's seat, contains a balanced d.c. amplifier, a 120-cycle 4-phase alternator, six permanent magnet generators and the motor for driving them and the alternator. The generators are of a special design, with two windings and a commutator on each end of the shaft to provide two d.c. voltage outputs per generator. Four generators supply the computing network, providing the various voltages which are acted upon by the computer unit. A fifth supplies the B and C voltages for the amplifier and the sixth the instrument's bucking potentiometers. They are magnetized to give the exact voltage in a magnetizing jig especially designed by Fairchild for this particular unit. A single casting forms the common endbell for each of the six generators, thus providing automatic alignment for each gear of the gear train that drives them.

4. *Mechanical Foot Pedal Assembly.* With this the gunner can control the size of the ring, so that its edges just touch the wing tips of the enemy plane. It also automatically introduces the factor of range into the computer unit.

All connections between the various units are electrical, with the exception of the connection to the foot control which is a flexible shaft. As previously mentioned, this gives a large

(Continued on page 122)

WACS at WORK

By

EDGAR F. G. SWASEY

Lt. Col., A. C., Chief, WAC Group

War communications must go through at our Army's wire, radio, and cable center in Washington.



Cpl. Colton sorts messages received in perforated-tape form, and decides whether they are to be reprinted for local delivery or transmitted to overseas stations.

MEMBERS of the Women's Army Corps—235 strong—are keeping the messages of war moving at the War Department Signal Center in Washington, hub of the Army's vast wire, radio, and cable communications system.

Working around the clock in eight hour shifts, the Wacs share responsibility for the operation of circuits to all parts of the globe. This station, the world's most important communications center, handles more than 10,000,000 words daily. Through the Wacs' hands pass messages destined to change the course of battles, to bring reinforcements to tired GI's in the front lines, to send supplies to places where they are desperately needed. Every tank, every plane, whether operating in the remote jungles of New Guinea and Burma, on the European battlefields, or in the icy stretches of Alaska, is only a few minutes from the High Command.

The Wacs are a vital part of the communications force which makes this possible. They carry a heavy burden of responsibility, for a message garbled or incorrectly transmitted might cost thousands of lives or affect the progress of a military campaign.

Wacs are carefully selected for this specialized task. They must have a high Army General Classification Test score, and their loyalty records are minutely investigated. Aptitude tests help to show whether or not each individual has the ability to learn the techniques necessary to handle the complex communications assignments.

For those Wacs showing the proper aptitude, the Army offers courses of instruction as typists, or will help them improve their typing speed if they have had prior training and

experience. Two Signal Corps Schools, located at Camp Crowder, Missouri, and at Fort Monmouth, New Jersey, teach the rudimentary phases of communications skills needed for duty in the Signal Center. The Signal Center itself offers a "postgraduate" course as a part of the program of instruction and job-training that fits into regular operations.

This training, while designed to provide skilled operators for the

Army's needs today, will pay off well for the Wacs in postwar jobs. These women are becoming experts in teletype operation, for instance. They operate high-speed perforators, which translate messages into perforated tapes in which each character is represented by a series of five or fewer holes across the tape. The Army has set up an elaborate and highly efficient system for relaying these mes-

(Continued on page 116)

Perforated tapes fed into the transmitters are reproduced by the printers in page form, suitable for delivery to the ultimate addressee. Through operation of this modern equipment, Sgt. McClurg is able to transmit 500 messages per hour.





Many of these Servicemen hope to find a place in electrical and electronic fields.

“ELECTRONICALLY YOURS, —G.I. Joe”

By **WILLIAM E. TAYLOR**

Radio Manufacturers Assn.

***The Radio Industry answers soldiers' inquiries
on how to prepare for postwar electronic careers.***

AMID all the worry and talk—a lot of it pretty loose—about the need for “reorientation” of returning soldiers and their future, Uncle Sam needn’t fret too much about one group at least. Communications veterans know what they want to do when they lay aside their uniforms, and they are already taking steps to do it.

Thousands of letters received by radio manufacturers from soldiers in camps and schools and on the fronts show that many are determined to pursue radio and kindred fields as peacetime careers. Their enthusiasm and interest is at a high pitch as a result of the excellent communications training provided by the Army Signal Corps, the Navy, and Army Air Forces, and the superb performance of communications equipment in the combat zones.

A great number of letters ask for information on how the writers may become electrical or radio engineers, and what opportunities the industry foresees for them in the postwar period. Moved by this interest, we have obtained from some of the leading radio and electronics manufacturers a thorough analysis of the entire electrical engineering field, with suggestions on how to proceed, for soldiers wishing to enter it. But first let’s have a look at a few of the letters,

plus a glimpse of radio engineering in wartime.

A large proportion of the inquiries is devoted to television and its development. One ardent student at a Western AAF school asked about television’s prospects, then showed that he had been giving the subject a lot of thought when he submitted a plan for eliminating the “ghosts,” or repetitions of the transmitted image on the receiving screen, which sometimes haunt television when the video wave is reflected from some object in its path.

“Although I am not familiar with the technical details, not having progressed that far in my training, it seems to me that this simple method of transmission would prevent appearance of television ‘ghosts,’” wrote the private to the chief engineer of a large Midwest firm which makes tele-

vision equipment in peacetime, but like all the electronics and radio manufacturers today, is turning out communications apparatus devoted solely to warfare.

The soldier enclosed a neat diagram of his plan. Although the method was impractical for reasons which a radio engineer knew immediately, the fact that he had arrived at it without benefit of an engineer’s training indicated that he had an exceptionally keen mind which could carry him far in the field if properly developed. The chief engineer promptly marked him down in his book as a promising candidate for the research laboratory.

“Send me everything you have about television. I am going to make it my life work,” wrote a technical sergeant from a Florida school, where he is a radar instructor, to an Eastern manufacturer. He disclosed that he was

saving his money, and intended to complete a full electrical engineering course at Massachusetts Institute of Technology, even though he's 32 now and has no idea how old he will be when he gets out of the army.

Primarily because radio is a young man's game—its development began after World War I, and was aided materially by many veterans of that war who had their first contact with radio equipment as Signal Corps soldiers—the industry has been hard-pressed to maintain engineering staffs adequate to meet the vast demands for communications apparatus of World War II.

Although their work is of utmost importance to the successful prosecution of mechanized warfare, since close control of fast-moving echelons by radio is essential and requirements for apparatus change constantly with the types of war and with lessons learned in the field, numerous radio engineers of combat age refused to endure lifted eyebrows of their neighbors, and got into uniform. The services commissioned many for specialized work in signal fields, of course, and these were able to continue research and development activities in conjunction with industry. The Signal Corps itself has estimated that the manufacturers' laboratories have covered ten years' of development in three years' time.

Those engineers who stayed home haven't all led a quiet life in the laboratory. Apparatus must be tested as it is developed, and some of the testing must be done under actual combat conditions. Danger and thrills aplenty are the lot of other engineers who try out equipment for the Air Forces. Riding in the back of the ships, busy with their instruments, they usually don't know what is going on in flight, and judging from the experience of one radio engineer whom we shall call R. E. Joe, it's a good thing.

This engineer had made innumerable flights, always in the back of the planes, and never had become airsick. At last, on a routine test in Nevada, up came his Waterloo. The air was thin and bumpy, and the B-25 hadn't been aloft more than ten minutes before he stretched out full length on the floor, too ill to move.

"Proceed with test," came the radio command from the base. R. E. Joe didn't dare open his mouth to reply.

"What's the matter?" asked the captain of the ship through the intercom. After repeating his question several times, he went back to investigate.

"Go on up and take my seat," the captain told the engineer when he saw his plight. "The back of the ship is the worst place to be in bumpy weather like this. You'll come around all right."

Groaning, the engineer staggered up front. Sitting in the nose, he stared in fascination at the breathtaking terrain unfolding before him for the first time.

"Prepare for dry run," came the order from the base. "Go ahead."

The co-pilot pointed the ship's nose earthward. Down, down, down it sped. The engineer's eyes bulged as a great clump of trees loomed larger and larger. Perspiration rolled down his face, and he found himself pushing backward with all his might against the floor, as a front seat passenger might do in an automobile when a crash seemed inevitable. His airsickness had evaporated.

At last, when catastrophe appeared certain, the co-pilot leveled off, and the plane cleared the treetops by inches.

"Do you always come that close?" Joe asked when he had recovered his breath.

The co-pilot grinned.

"First time I ever made a dry run with a B-25," he replied. "Didn't know much more about it than you did."

The Radio Manufacturers Association foresees innumerable opportunities for electrical engineers in the postwar period, especially in the communications and electronics fields. Widespread development of frequency modulation and of television in the decade after the war ends is expected to open numerous positions for radio engineers both in broadcasting and manufacturing.

Other opportunities will be open to veterans who do not intend to take the time to obtain the training necessary for an electrical engineer. The War Manpower Commission already has noted that communications veterans will have a better-than-average prospect of obtaining good jobs after

the war, listing among them radio repairman, public address serviceman, aircraft radio inspector, radio installer, electrical tester, instrument maker. In some cases, the training already received by the soldier will be sufficient to permit him to enter his chosen field at once. Additional training of various lengths will be required for others.

For the electrical engineering field, this general list of qualifications and requirements should be of help to soldiers interested in such a career. Electrical engineering is broken down into five general headings:

1. Power engineering, embracing generating stations, substations, transmission line and distribution systems.

2. Transportation engineering, embracing generating stations, substations, rolling stock, right of way and signal systems.

3. Industrial engineering, embracing application of power, communications, electronic and special electrical equipment to industrial purposes having to do with processing, remote control, checking, counting, and a hundred operations.

4. Communications engineering, embracing the telegraph, telephone, facsimile transmission, television, radio broadcasting, radio systems for traffic control safety, etc.

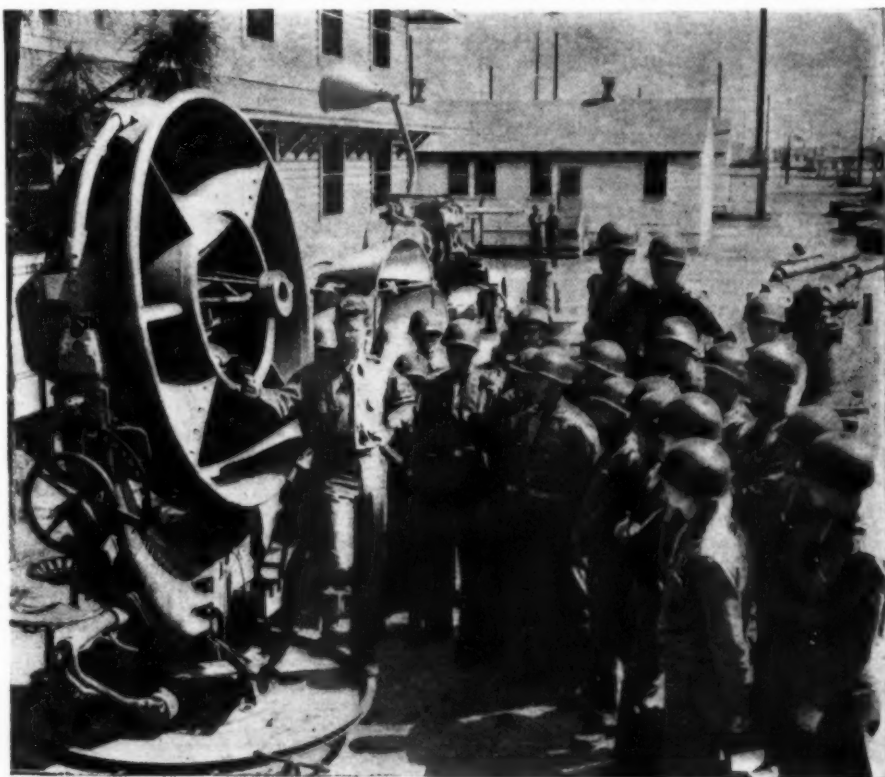
5. Electronic engineering, dealing with tubes, photocells, and application of tubes to special electronic devices and services.

Many kinds of engineering work are performed by specialists in each of the fields listed. Among these are,

1. Service and installation engi-

(Continued on page 128)

Enemy "detective devices" being described to Army Air Forces Officers. These men study the equipment so that they will be able to recognize it during combat.

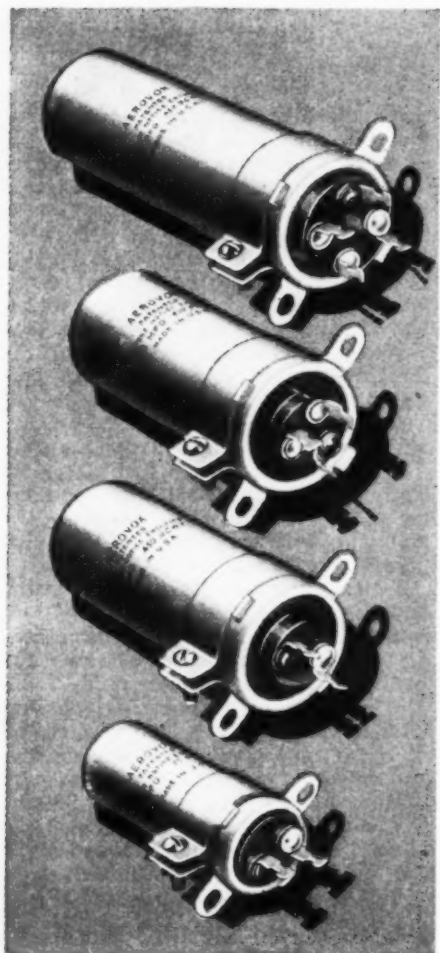


Power Supply Filter Design

By **HAROLD S. RENNE**

Technical Editor, RADIO NEWS

Determining suitable values of inductance and capacitance in power supply filters for reducing the ripple voltage to an acceptable value.



Electrolytic capacitors combine high capacity with small volume.

THE purpose of a power supply filter is to smooth out the ripple in the rectifier output, and so provide a source of essentially pure d.c. Most applications will permit the use of d.c. with a small amount of ripple, the amount of ripple depending on the application.

In order to design a filter intelligently for a particular use, there are several factors which should be known or calculated. Among these are the percent of ripple permissible, the ripple frequency, type of rectifier, i.e., half-wave, full-wave, bridge-type, etc., peak transformer secondary voltage, or the peak supply voltage in the case of a transformerless supply, and the maximum and minimum output currents. These various factors will be discussed as the need arises.

The term "pure d.c." as applied to the output of a power supply is a relative term. The output invariably contains a small amount of ripple, and to describe this ripple properly, a factor called the *percent ripple* is defined. This factor is the ratio of the ripple voltage to the average d.c. voltage

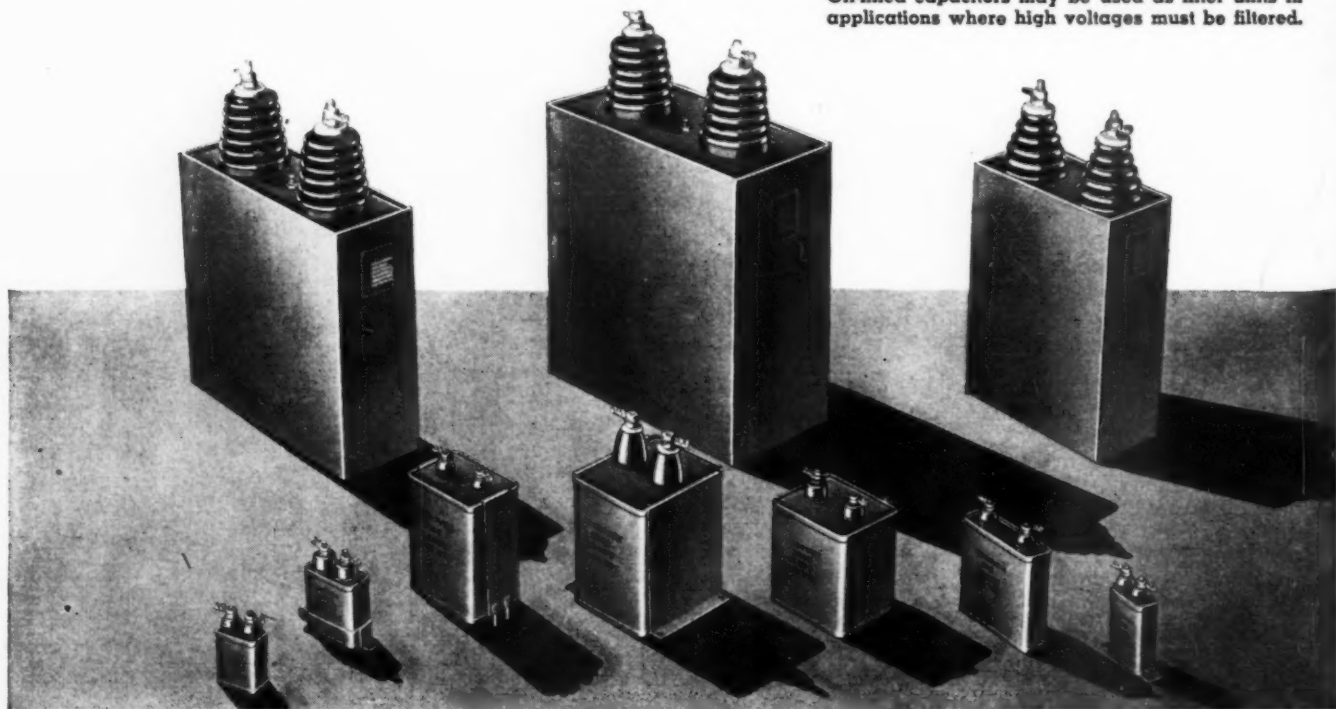
(multiplied by 100 to convert to percent) and is illustrated in Fig. 3. The ripple voltage is the r.m.s. or effective value of the a.c. component in the filter output and may be measured on the a.c. range of a vacuum-tube voltmeter. The average d.c. voltage is the voltage which would be indicated by a d.c. voltmeter. Mathematically, this factor may be expressed thus:

$$\% \text{ Ripple} = \frac{E_R (\text{RMS})}{E_{dc}} \times 100 \dots (1)$$

The percent ripple permissible varies widely for different applications. For a high gain voltage amplifier, the ripple should be less than .001%, while for the final stage of an r.f. amplifier for code transmission, 5% ripple is not excessive. For intermediate amplifier stages, ripple should not exceed .1%, and for power stages, 1%.

Ripple frequency is another factor which must be considered in designing power supply filters. As its name implies, the ripple frequency is the frequency of the a.c. component of the rectifier output. This frequency depends on the frequency of the power

Oil-filled capacitors may be used as filter units in applications where high voltages must be filtered.





Plug-in type electrolytic capacitors simplify servicing problems.

source, the number of phases and the type of rectification, i.e. either half-wave or full-wave.

The power source for the large majority of power supplies is either single-phase or three-phase. Fig. 4A shows the output of a single-phase, half-wave rectifier. The ripple frequency for such a supply is equal to the supply frequency. Fig. 4B shows the output of a single-phase, full-wave rectifier which has a ripple frequency of twice the supply frequency. The output of a three-phase, half-wave rectifier has a ripple frequency of three times the supply frequency, and a three-phase, full-wave rectifier a ripple frequency of six times the supply frequency. Summarizing, if f is the supply frequency, the ripple frequency for single-phase circuits will be f for half-wave rectification and $2f$ for full-wave rectification. For poly-phase circuits, if n is the number of phases, the ripple frequency will be nf for half-wave and $2nf$ for full-wave rectifiers.

It should be understood that this fundamental ripple frequency is not the only frequency present in the rectifier output. Considerable percentages of various harmonics also are present, but any filter designed to reduce the amplitude of the fundamental ripple frequency to an acceptable value will effectively eliminate all harmonic frequencies.

Power supply filters, in general, are made up of units of inductance and capacitance, with a resistance sometimes replacing the inductance. The effect of the capacitance is to smooth out voltage variations, and the effect of the inductance is to smooth out current variations.

There are two main classifications of filters, depending on whether the element immediately following the rectifier is an inductance or a capacitance. If the inductance comes first, the unit is called a choke input filter; if the capacitance comes first, it is called a capacitor input filter. The two types of filters have different characteristics, and will be treated separately.

A typical single section choke input filter, sometimes called an inverted L section, is shown in Fig. 1A. The

output voltage from a filter of this kind is approximately .9 of the r.m.s. voltage of half the transformer secondary for full-wave rectification, or of all the transformer secondary for half-wave rectification, provided that the inductance of the choke is greater than a certain critical value. The true output voltage to the load will be the above value less the voltage drop in the tubes and choke.

The critical value of inductance when the ripple frequency is 120 cycles, is given by the equation:

$$L_{crit.} = \frac{R}{1000} \dots \dots \dots (2)$$

where R is the load resistance in ohms, and $L_{crit.}$ is in henrys. Under no load conditions, it can be seen that the value of the inductance would have to be infinitely large, so a bleeder resistor is usually shunted across the filter output, and the resistance of this bleeder resistor determines the highest value of load resistance and so the maximum value of inductance. For ripple frequencies other than 120 cycles, the above value is multiplied by $120/f_r$, where f_r is the ripple frequency. The complete equation is then:

$$L_{crit.} = \frac{12R}{f_r} \dots \dots \dots (3)$$

With this value of inductance, the

peak rectifier current in a full-wave rectifier will be approximately 10% higher than the d.c. load current taken from the supply.

It can be seen that the value of critical inductance varies widely under varying load conditions, being smaller for larger loads, and *vice versa*. This permits the use of a choke whose inductance decreases as the load current increases. Such a choke is called a *swinging choke*. A choke of this kind is much cheaper than one which keeps its full value of inductance under full load conditions.

Better operation will be obtained under full load conditions if the value of inductance is about twice the critical value. This is called the *optimum value*, and represents the point at which a further increase in inductance does not give a corresponding increase in performance. An ideal choke would be one having critical inductance at no load (bleeder only), and optimum inductance at full load. For example, if the bleeder resistance is 20,000 ohms and the full load resistance 2,500 ohms, a choke which swings from 20 henrys to 5 henrys over the full output current range will be satisfactory. Such a choke would be much cheaper than one designed to have an inductance of 20 henrys over the full current range.

The percent ripple for a single section choke input filter is given by:

Fig. 1. (A) Single section "L" or choke-input filter. (B) Two section choke-input filter. Bleeder resistor R improves regulation.

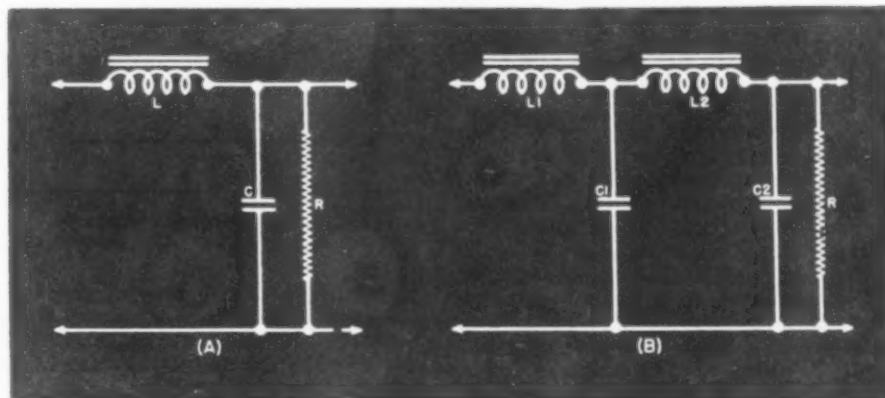
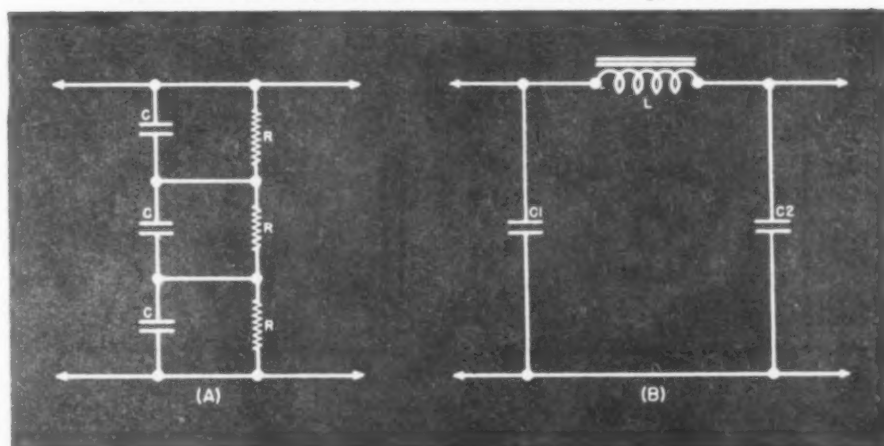
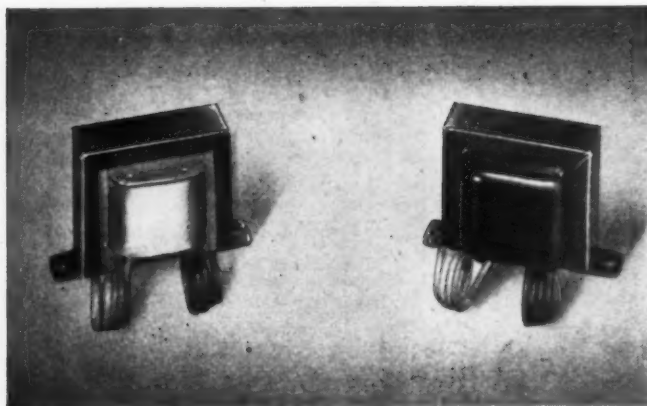
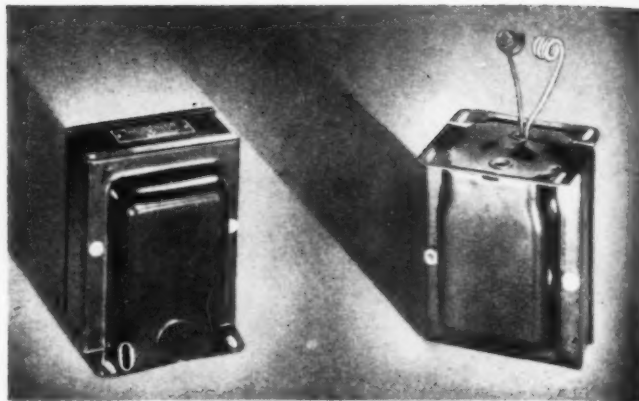


Fig. 2. (A) Filter capacitors in series with voltage-equalizing resistors R . (B) Single section π or condenser-input type of filter.





Filter chokes for top-of-chassis or sub-chassis mounting in low-power applications.



Complete shielding of filter chokes reduces stray a.c. fields and helps reduce hum.

$$\% \text{ Ripple} = \frac{12,000}{LCf_r} \dots\dots\dots (4)$$

where L is in henrys, C in microfarads, and f_r the ripple frequency in cycles per second. If a ripple of less than about 5% is desired, a two section filter may be used (Fig. 1B). The percent ripple is then given by:

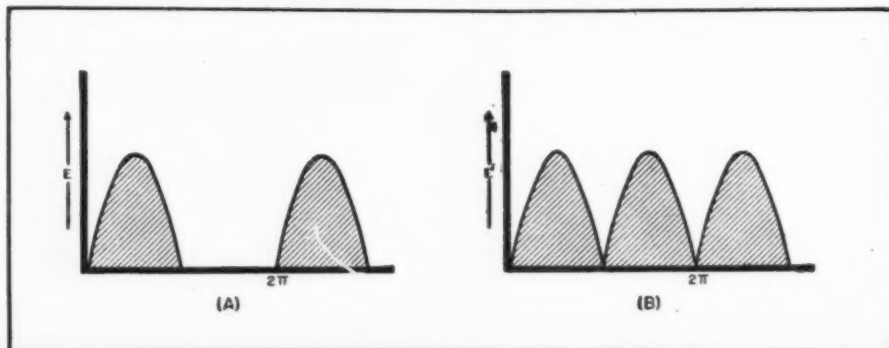
$$\% \text{ Ripple} = \frac{7.8 \times 10^4}{L_1 L_2 f_r (C_1 + C_2)} \dots\dots (5)$$

If the filter feeds an audio-frequency power amplifier, the output current may vary between fairly large limits because of the variation in the current requirements of the power tubes. To avoid excessive distortion, the output voltage should be as nearly constant as possible. To hold this voltage constant, the output condenser of the filter must have sufficient capacity to absorb variations in voltage caused by the varying current. The lower the desired frequency response of the amplifier, the larger will be the necessary capacity.

Another way of stating this would be to say that the reactance of the condenser at the lowest audio frequency being amplified must be small compared with the load resistance. If f_m is considered to be the minimum or lowest frequency being amplified in cycles per second, R_L the load resistance in ohms, and assuming that the capacitive reactance may be one twentieth the load resistance, the value of the output capacitor is:

$$C = \frac{10^6}{\pi f_m R_L} \dots\dots\dots (6)$$

Fig. 4. Waveshape at output of a half-wave rectifier (A) and full-wave rectifier (B).



where C is in microfarads. For example, if the load resistance is 5,000 ohms and f_m is 50 cycles, the output condenser should have a value of at least 12 μ fd.

The d.c. working voltage rating of the condenser or condensers used in a choke input filter should be at least

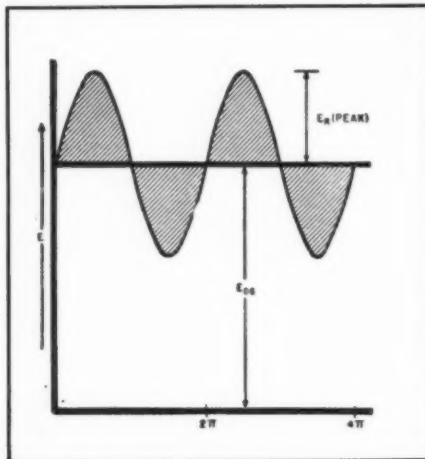


Fig. 3. A.c. ripple superimposed on the steady d.c. voltage.

equal to the r.m.s. value of one half the secondary voltage of a full-wave rectifier. This assumes that the bleeder is connected at all times. If there is a possibility of operation with neither the load or bleeder connected, the r.m.s. voltage should be multiplied by 1.5 to give the required condenser voltage rating. If no condensers of this rating are available, two or more

condensers may be connected in series, in which case the voltage ratings are additive (Fig. 2A). The resistors connected across the condensers tend to equalize the d.c. voltage across each condenser. The values of these resistors must all be the same and should be in the neighborhood of one-half megohm.

Condensers having different capacity or voltage ratings should not be connected in series, as this greatly increases the possibility of breakdown. When two or more condensers are used in series, the total filtering capacity is given by C/n , where C is the capacity of each condenser, and n is the number of condensers in series. The voltage rating of the combination will be nE_{wv} , where E_{wv} is the working voltage rating of each condenser.

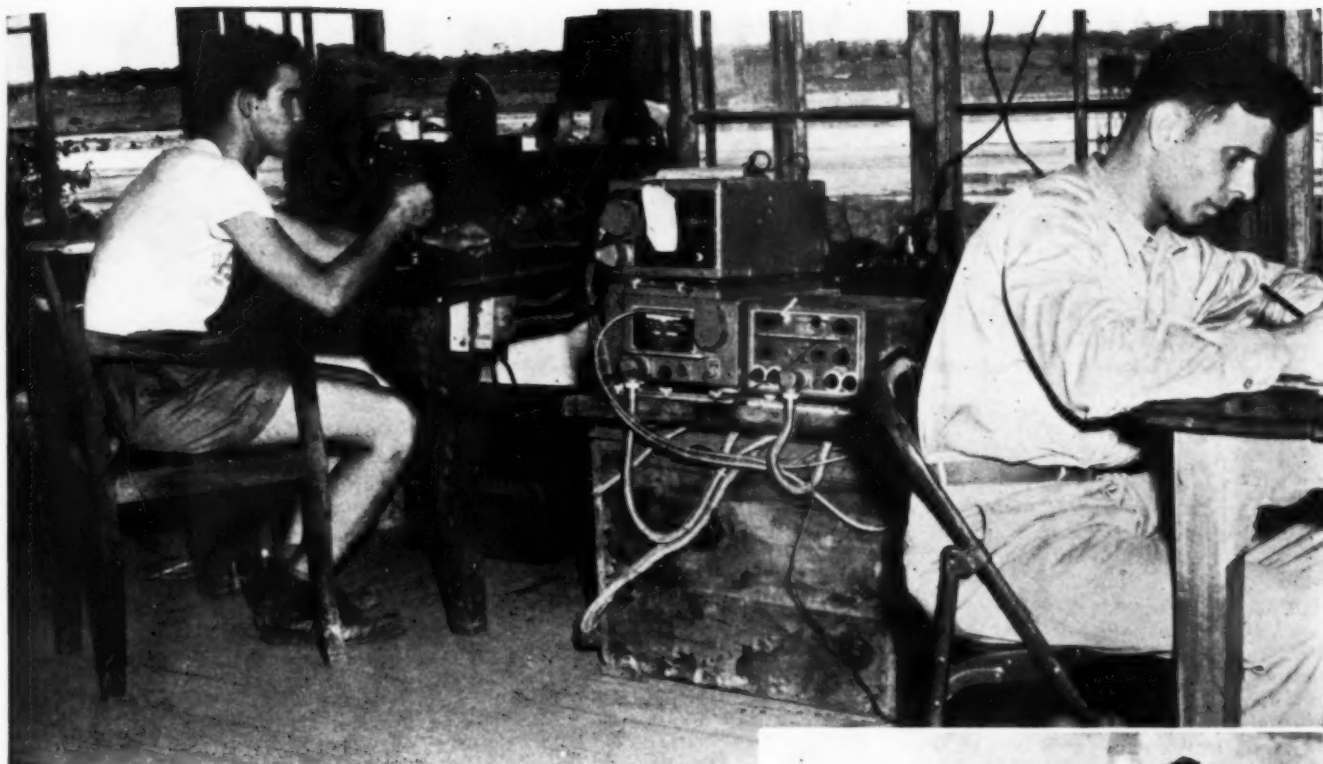
Fig. 2B shows a single section condenser input, or pi section filter. This is a low-pass filter with a cutoff frequency well below the ripple frequency and is sometimes known as a brute force filter, because large values of inductance and capacitance normally are used without much attention being paid to the actual cutoff frequency. The output voltage of this type of filter varies widely under different load conditions. With no load, the output voltage is approximately 1.41 times the r.m.s. value of half the secondary for a full-wave rectifier, and under heavy loads may drop to .9 the r.m.s. value or lower.

The percent ripple for this type of filter is difficult to calculate, but will be lower as L and C are made larger. A filter design which is suitable for a 120 cycle ripple frequency may be converted for use at some other ripple frequency by multiplying the values of L and C by $120/f_r$, where f_r is the new ripple frequency.

The output condenser for this type of filter may be calculated in the same manner as for the choke input filter (Eq. 6).

The peak value of rectifier current in the condenser input filter is much larger than for the choke input filter, and increases as the size of the input condenser is increased. This ordinarily is not detrimental when high vacuum-type rectifiers are used, but with gas-

(Continued on page 94)



A Ferrying Squadron Operations Control Tower located in India.

BOMBER'S EARS

Radiomen aboard our bombers must keep in contact with their base at all times, while winging their way over enemy targets.



The departures of all planes leaving either India or China for a trip over the "Hump" are PX'D from this Control Tower to the field where they are to land.

HIGH above Italy a formation of 15th Army Air Force heavy bombers flies to bomb German troop concentrations in a certain town. It's a clear day, and a large escort of speedy fighters makes a protective umbrella for the big bombers. Until they actually reach the target, or encounter flak or fighters, the crew of a bomber takes it easy; it's a "milk run" to everybody but the radio operator, who monitors one of the several radio sets on the bomber, from the time they take-off till they land.

As the bombers roar through the air, 20,000 feet high, the radio operator suddenly receives a coded message from their base—turn back! The radioman on the lead plane repeats the order to the pilot over the interphone.

The formation banks, and heads for home. Back at base they learn that our troops, in a surprise attack, had taken the town the night before. Radio had prevented a horrible "mis-

(Continued on page 88)

Transmitting and receiving equipment at one of our Army Air Forces' outposts. Operators control not only all departures and arrivals, but keep in contact with planes in flight.



TONE CONTROL CIRCUITS for Phonographs

By F. E. WINTER

A tone control providing a form of equalization may be used to obtain ultimate tonal reproduction from commercial phonograph records.

THE search for better phonograph reproduction leads away from Chippendale cabinet-work to a businesslike assembly of high-fidelity parts. Given a sensitive wide-range pickup, a quiet and smooth-running turntable motor, and a powerful high-fidelity amplifier and speaker team, a phonograph system might be expected to deliver the finest results obtainable from records.

Often, however, such a system sounds quite drowned in a muddy roar of bass. When, in attempting to make the high notes more audible, the operator turns up the volume control, the bass notes break and distort from the resulting amplifier overload and the highs appear intermittently as stabs of ear-splitting resonance. Equalization is lacking, and no setting of tone or volume controls will correct the predominance of bass frequencies.

Due to mechanical limitations of the cutting and reproduction processes, commercial phonograph records are made with their higher frequencies deliberately reduced in scope. Sound waves are recorded by a side-to-side (lateral) undulation, an irregular and often jagged displacement of the groove from its spiral path. To reproduce these waves, the needle point must faithfully trace each minute change of direction in the groove. It is seen easily that groove contortions could be violent enough to throw the

point out of the groove, causing it to rattle or skate loosely along the shoulders of the track. Since the needle point receives thousands of these lat-

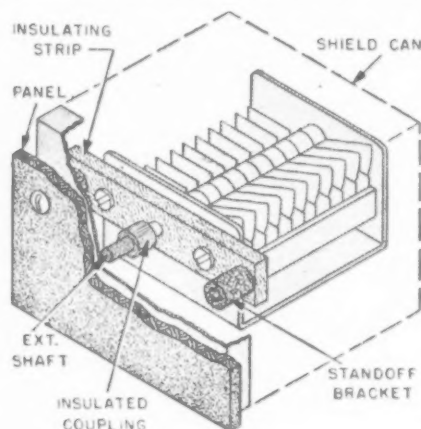


Fig. 2. Showing the method of mounting the variable condenser.

eral impulses each second from the groove track, recording engineers have developed a means for insuring that no movement of the groove will be too quick for the inertia of the needle point to follow. This, the so-called "constant velocity" method, keeps the point in accurate track, except for low frequencies, where constant velocity recording produces so wide a swing in

the groove path that neighboring grooves may intersect one another, and also may be violent enough to toss the point completely out of the groove channel. Here, in the low frequencies, a method of limiting, called "constant amplitude," keeps the groove-swing within safe tracking dimensions.

A commercial recording utilizes both methods to produce a mechanically practical disc, but one result is the great compression or attenuation of higher frequencies and an overabundance of low frequencies, an inaccurate tone picture faithfully and distressingly reproduced by any wide-range phonograph system having an unequalized pickup circuit.

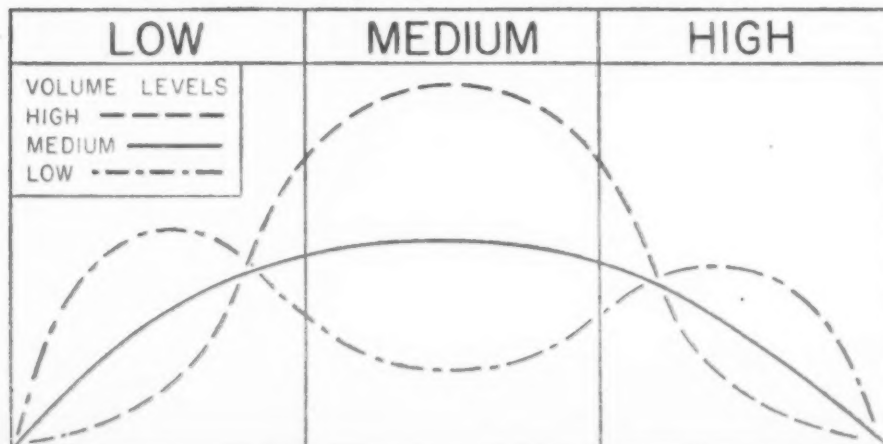
Composed of a few simple parts, the equalizer circuit given here has been installed in phono-systems using amplifiers of various output ratings, designed originally for such purposes as small public-address units, coin phonographs, or wide-range, high-fidelity phono installations. In each case, performance improved remarkably, particularly in the instance of fine, commercially built phonograph amplifiers. Tone of such widely different instruments as the oboe and contra-bass sounded clearly, and at high volume levels the colorful panorama of orchestral voices replaced a previous incoherent roar.

How the Circuit Functions

The bass cutoff is a variable resistance in the familiar volume control form, inserted in parallel with the pickup. The loading applied by this resistance diminishes the low-frequency response of the crystal pickup, to correct the excessive amount of bass present in recordings. Since most amplifiers distort easily on lows, where power output ability can be overdrawn on by too strong an input signal, the cutoff keeps bass tones safely within distortion limits of the amplifier at any volume level and provides compensation for minor variation of bass strength in different recordings.

At low volumes, the control has another application, for, as shown by the frequency graph of Fig. 1, the necessary proportion of bass to middle and high frequencies is much greater at low volume levels. Here, the control

Fig. 1. Curves showing relative proportions of low, medium, and high frequencies for proper reproduction at various volume levels.



permits the full strength of low frequencies present in a recording to boost the audibility of bass tones. A value of 5 megohms should be satisfactory for this control, although some experimentation may be necessary to find a suitable value.

The series resistance and condenser by-pass controls form a filter system for varying the high-frequency response of the pickup. The highs, not appreciably affected by normal settings of the bass cutoff, are damped by the series resistance, around which they are by-passed through a condenser of 25 to 500 μfd . The ratio of resistance to capacity in this filter determines its effect on the high frequencies. The series load is usually set at 2 megohms for older types of 2½ oz. pickups, and at 5 megohms for the newer low-pressure units. With the by-pass inoperative, low notes are very prominent, but as capacity is cut in around the load, the highs increase, to where a 400- or 500- μfd . value transmits so much of them that the damping action of the resistance load is confined largely to the region of 4000-5000 cycles per second, where surface hiss and mechanical resonance peaks of the pickup predominate over recorded sounds.

Thus, by use of stepped or variable condenser by-pass, the filter network accentuates or cuts off the high-frequency bass cutoff control. Both controls operate effectively in the middle-frequency range, yet each retains its characteristic effect here as well as in its own particular zone.

Parts

As low-voltage audio circuits easily pick up a.c. noise from power wiring, the equalizer design includes complete shielding, a necessary practice extended in high-gain systems to include all cable and connections between pickup cartridge and amplifier chassis. Shielded wire is not available for non-war purposes, but excellent substitutes exist in single-conductor armored automotive cable from car-salvage lots, or can be made by winding single-conductor insulated wire with metal foil or with flexible sticky-tape radio aerial. Such improvised cable-shielding is quite satisfactory if there are no breaks along the shielding and care is taken to make good electrical contact at the ends of the shielding.

Elements of the high-frequency filter are more conveniently operated in steps through selector switches, but these may not be readily obtainable, hence Figs. 3 and 4 show alternate sets of parts, using either 6-stepped units or a 5-megohm volume control and a 450- μfd . t.r.f. condenser whose capacity increases with clockwise rotation.

A simple shield for the equalizer is a tin can with a removable lid, on which are mounted panel, input and output terminals and all controls, so that the body of the can is merely a removable cover. If the equalizer is to use stepped condensers, the flat

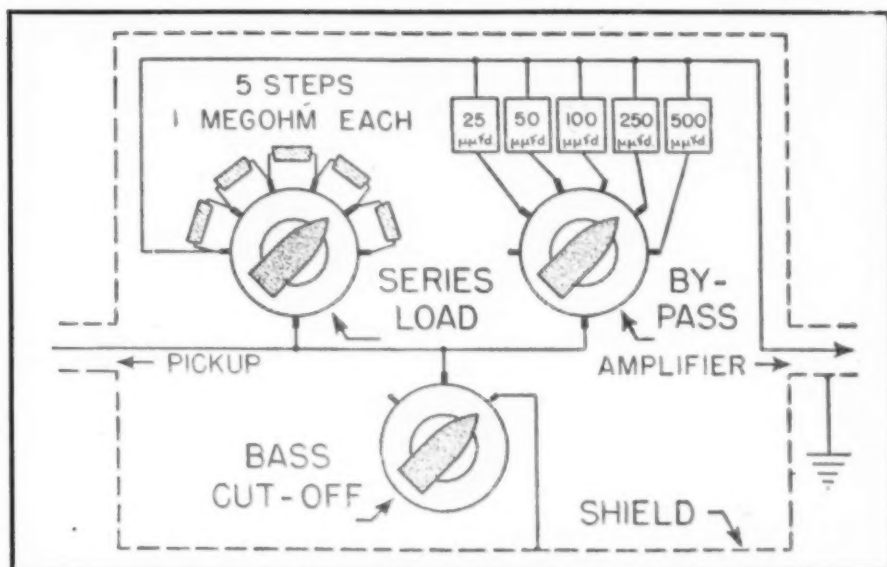


Fig. 3. Wiring diagram of the low- and high-frequency tone control. Six-position rotary switches are used to obtain a variation in the tonal response.

type of can in which 35-mm. motion picture film is shipped in bulk rolls is suitable. With a variable condenser, a larger can is necessary, but the insulated mounting may be bracketed to the can lid assembly also. In locating this mount on the panel and lid, clearance must be allowed for the condenser rotor to open fully without grounding to the shield cover, and the condenser frame must be kept from touching grounded volume control shells, for either contact would result in no signal to the amplifier. Detail of an insulated mounting for a variable condenser is shown in Fig. 2.

Assembly

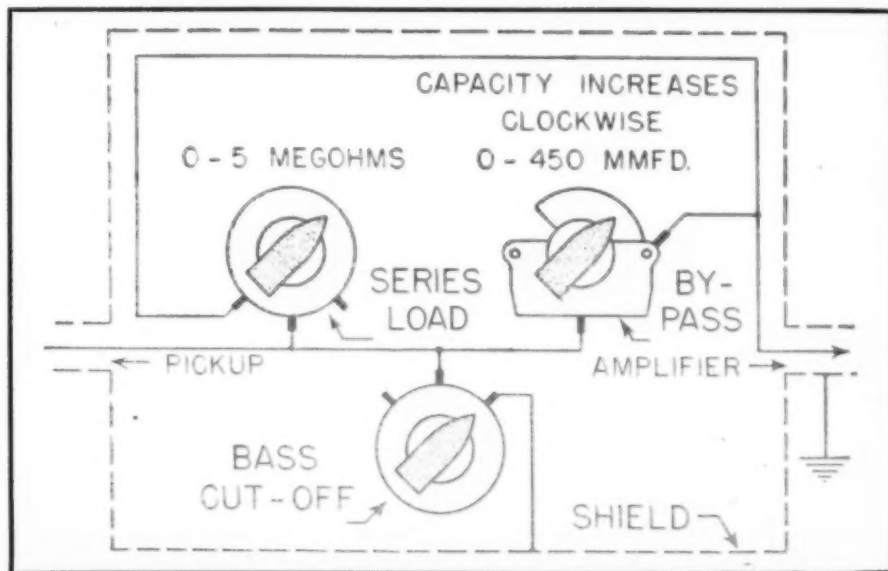
If your plan includes phone-tip, phono or microphone types of connectors, mount these on the panel assembly, rather than on the shield can body, as the unit thus remains accessible for replacing aging volume controls or for checking connections

easily. In hooking up, mark fixed condensers with their values to avoid confusion, and solder all leads quickly to minimize overheating of resistance or capacitance elements via their terminal wires, particularly in assembling the stepped units, where working space between selector taps is cramped. Threaded shanks of volume controls or switches will hold the panel assembly together solidly if shakeproof washers are used beneath the shank nuts.

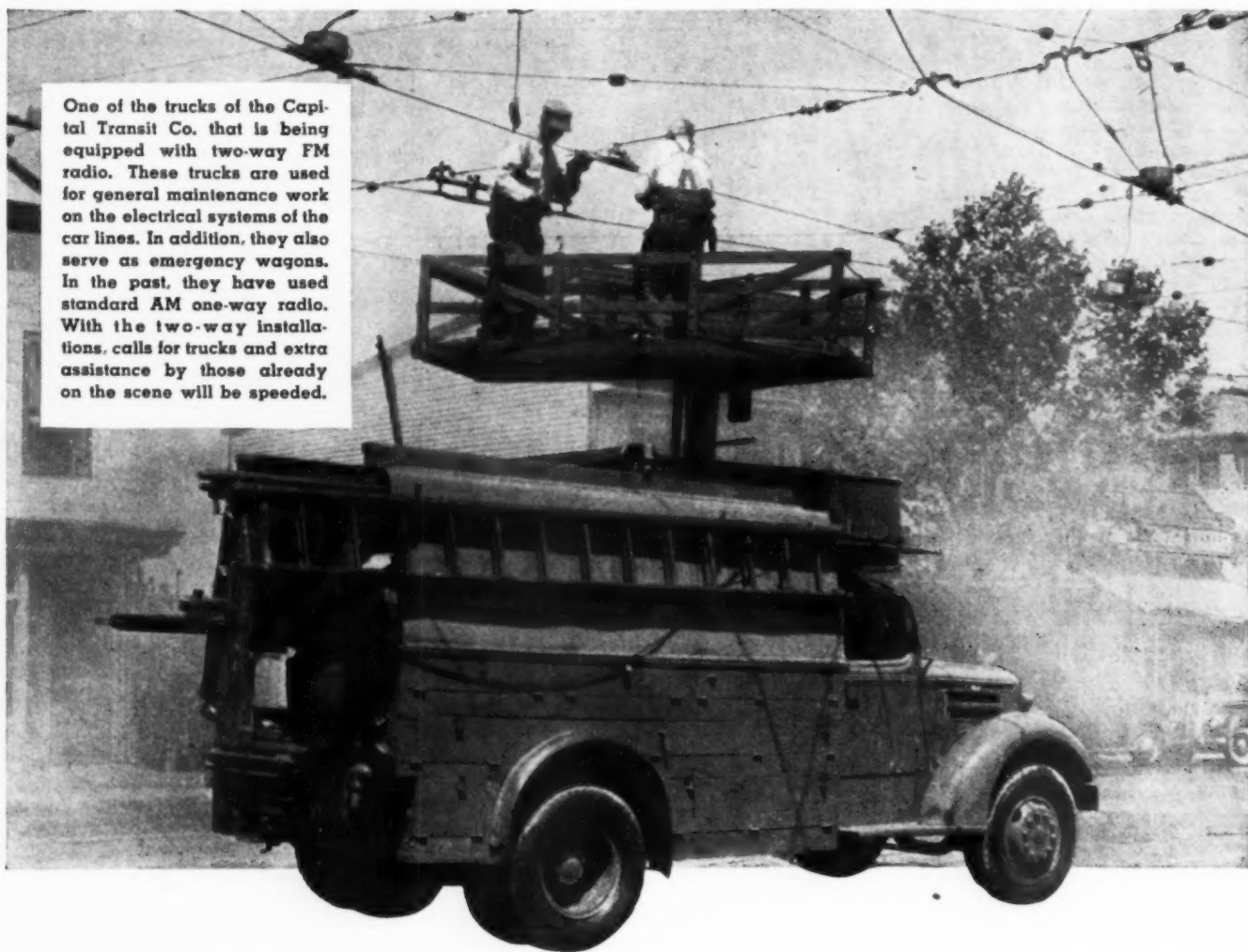
Numbered dial plates may be installed with the controls, but steps or reference points can be shown effectively by drilling shallow holes in the panel at points selected, and by filling each spot with a drop of red or white lacquer. In tightening bushing nuts, the maximum positions of controls (all the way right, clockwise) should fall at three o'clock, and the flat sides of volume-control shafts opposite, at nine

(Continued on page 142)

Fig. 4. Similar tone control to that of Fig. 3, using in this case continuously variable controls. A 5-megohm bass cutoff potentiometer is used.



One of the trucks of the Capital Transit Co. that is being equipped with two-way FM radio. These trucks are used for general maintenance work on the electrical systems of the car lines. In addition, they also serve as emergency wagons. In the past, they have used standard AM one-way radio. With the two-way installations, calls for trucks and extra assistance by those already on the scene will be speeded.



RADIO FOR TRANSIT

By JOAN DAVID

FM two-way radio is fast replacing the obsolescent AM one-way type as an aid in relieving many transportation difficulties.

FIVE thousand people were late to work in Washington last February 12th. A score of skeptical employers called the Capital Transit Company to check up and were reassured. There had been a two-hour delay on one of the busiest downtown-bound streetcar lines. Cabs were scarce and there were few private cars on the road. Sleet mixed with snow had fallen during the night and the ice-covered roads were innocent of sand. Such semi-Arctic municipalities as Boston and Chicago probably would have rendered their main thoroughfares navigable by the time the morning rush hour started. Icy streets in Washington, however, usually are regarded as a freak having no business so far south. Wait a day or two is the theory, and the problem will cease to exist.

And so, despite and because of the 15-degree weather, the crowds at the streetcar stops were bigger than usual. The trouble started at about 8:28 a.m.

Here, in essence, is Capital Transit's record of the event: A telephone call received in our central dispatcher's

office at 8:33 a.m. informed the dispatchers that two cars were standing at 18th and Columbia Road, N.W., without current. By telephone at 8:34 a.m. emergency truck No. 105 was dispatched to the scene of the trouble. At 8:35 a.m., by one-way radio (shared by the local power company which broadcast messages phoned to it by Capital Transit's dispatchers), No. 65 cruiser, a Transportation Department Supervisor, was also dispatched to the scene. By 9:01 a.m. no report had been received in the central dispatcher's office regarding the trouble. At this time, 9:01 a.m., No. 67 cruiser, Transportation Supervisor manned, was dispatched by one-way radio, and at 9:09 a.m., No. 72 emergency truck

was dispatched by telephone. At 9:15 the wagonman in charge of No. 105 truck reported in with details on the cause of the breakdown. Eighteen cars had run through a broken rail and been so damaged that they could not collect current. Thirty-eight more cars which had started down the same route were stalled on the line until it was cleared. Eighteen cars in a row unable to proceed under their own power provided an extremely difficult problem. It was necessary to obtain heavy trucks to push these cars to a location where repairs could be made. Throughout the 115 minutes detention the line was at a standstill. There was no means of turning the cars back.

If the whole incident were transposed ten months to December 12, 1944, this unavoidable accident might have caused a total delay of only 30 minutes. For, toward the end of November, the Capital Transit Company began the operation of its newly licensed frequency-modulation 250-watt transmitter which, together with the two-way General Electric 30-watt mobile units installed on each of their 30 emergency trucks and supervisory cars, has more than halved the time needed to handle emergencies.

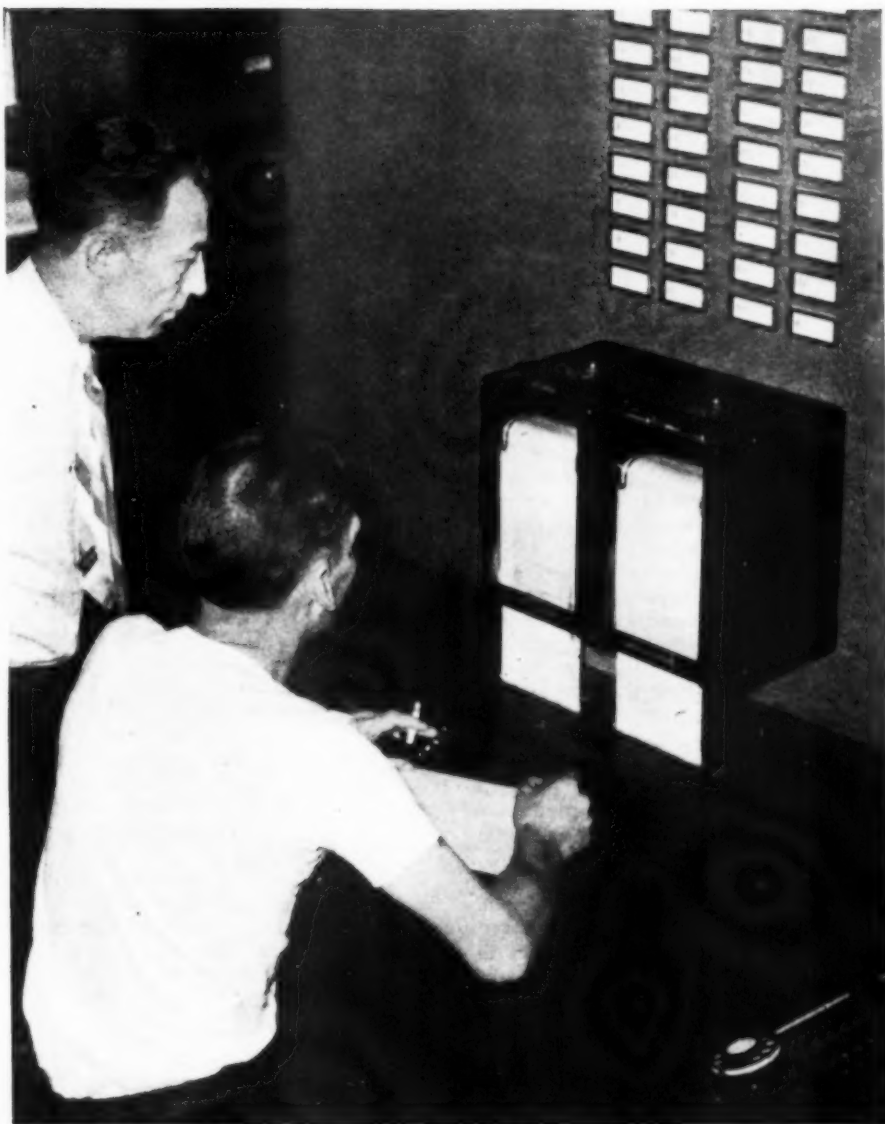
Capital Transit's chief engineer, Ronald Thring, explains that the incident, if duplicated today, might develop in an entirely different manner. "Eighteen cars would not have been placed out of service because No. 105 emergency truck and No. 65 cruiser would have coordinated their activities and held the line at the point of fault. No. 105 emergency truck would, in all probability, have cleared the trouble in about ten minutes. There would have been no more than eight cars crippled. At least sixty cars would have been rerouted if talk-back had been available. Thirty-eight cars which ran in after the fault developed and were tied up throughout the 115 minute delay could have been freed for other service. Other emergency wagons could have been dispatched on arrival of No. 105 truck, instead of 29 minutes later. Inspectors could have been sent to cut-backs or points at which the line could have been rerouted. Regular routing could have been re-established immediately after the line was cleared instead of after

UTILITIES

fifteen minutes of telephoning.

The Capital Transit Company, with its new station WQHA, is the 13th transit company to install its own radio facilities since 1938, when the Federal Communications Commission first decided that transit utilities might be assigned frequencies in the 30-40 megacycle band, which is reserved for emergency use. (Police, forestry, marine, and other government services share this same band.) That decision was an amendment to a general reallocation of frequencies made possible by the widening of the usable spectrum due to developments in short-wave.

Today the FCC is again making a general reallocation of frequencies. Investigations have shown the need for such reallocation, although permanent decisions in most cases are contingent on international agreement and will be put off until the postwar period insofar as possible. The important advances in radio and the tremendously increased demands on
(Continued on page 144)



"Headway recorder" automatically records the passing of streetcars at 40 points scattered over the company's system. Transit failures are indicated by this machine.



"Dispatchers' desk" in the Central Dispatchers' Office of Capital Transit Company, Washington, D. C. Through two-way radio, any assistance that the calls indicate are needed can be sent more quickly than possible ever before.

THE TELEVISION CHANNEL

By **EDWARD M. NOLL**

Part 2. Continuing our study of television, the author discusses the standard television broadcast channel.

THE standard television broadcast channel is six-megacycles wide, as seen in Fig. 1, and contains both the picture and sound carriers plus sidebands, the picture signal occupying the greater portion of the channel. The picture is amplitude modulated and occupies a $5\frac{1}{4}$ -megacycle channel; the sound, frequency modulated with a 150-kilocycle channel. An exceptionally broad picture band is necessary to transmit a sharp well-defined picture; in fact, the wider the channel the better the sharpness and definition becomes. Consequently, while a 10,000-cycle band is adequate to transmit an amplitude-modulated sound signal, a band of at least 4,000,000 cycles is required to transmit a satisfactory picture. With that end in view a portion of the low-frequency picture sideband is attenuated at the transmitter and not radiated from the antenna. Observation of the drawing shows that the low-frequency sideband is only $\frac{1}{4}$ -megacycles broad, while the flat portion of the high-frequency sideband is 4-megacycles broad. Thus, it is possible to obtain a 4-megacycle defini-

tion in a 6-megacycle channel with partial suppression of one sideband—called vestigial-sideband transmission. The most to be expected in a 6-megacycle channel with symmetrical picture sidebands would be a flat sideband of $2\frac{1}{2}$ megacycles.

Two $\frac{1}{2}$ -megacycle guard bands are located at the edges of the picture sideband to allow the signal to fall from maximum amplitude to a very low level, without overextending the low-frequency end of the channel or interfering with the sound signal. The sound carrier is $4\frac{1}{2}$ megacycles above the picture carrier, and is permitted a maximum deviation of ± 75 kilocycles with modulation. In a recent proposal by the television panel of the Radio Technical Planning Board it has been suggested that the deviation be reduced to ± 25 kilocycles. As an aid in obtaining a clear conception of a typical television channel, the layout of the first three channels is given in chart form in Table I.

Scanning

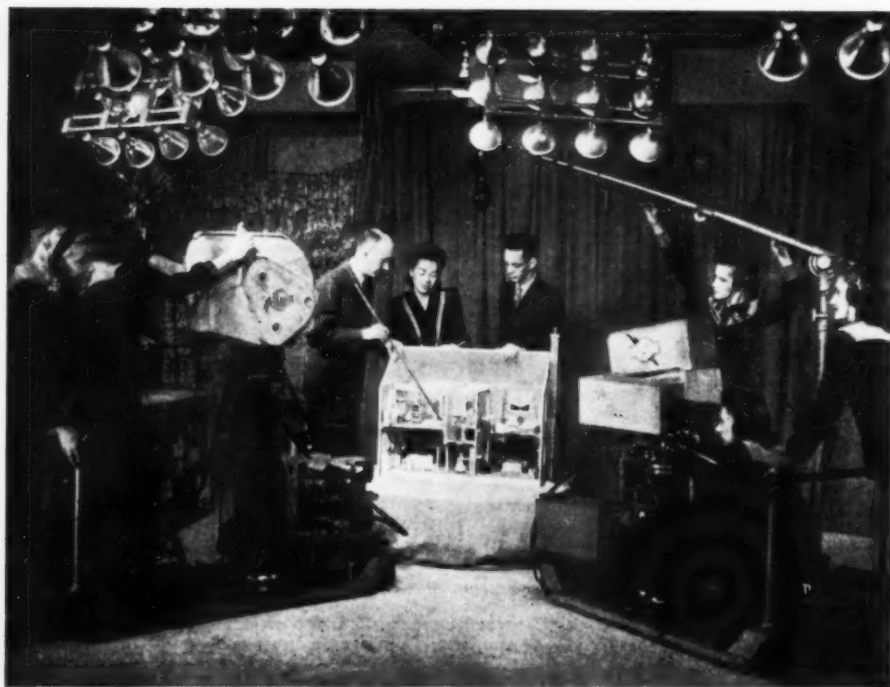
In modern television systems scan-

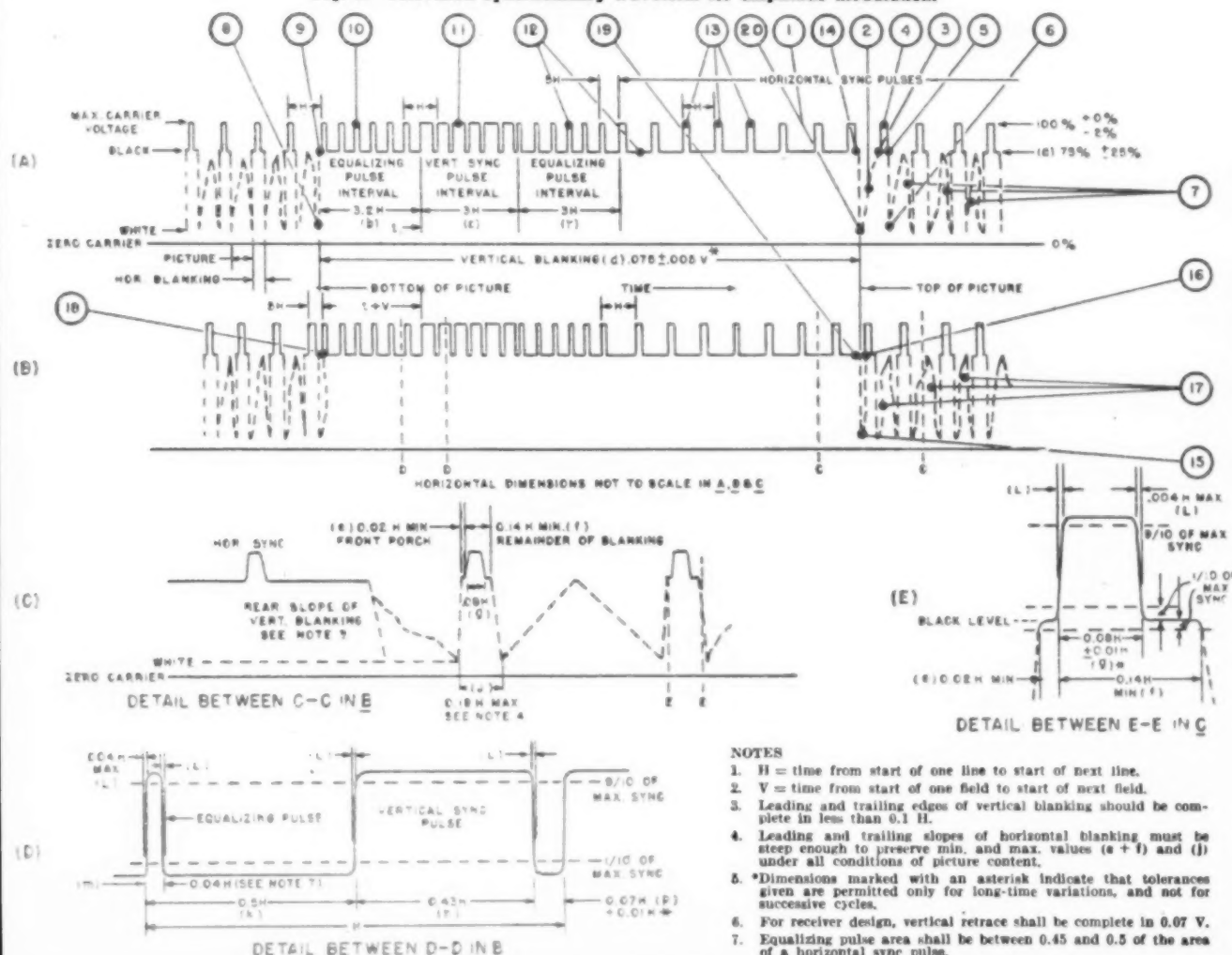
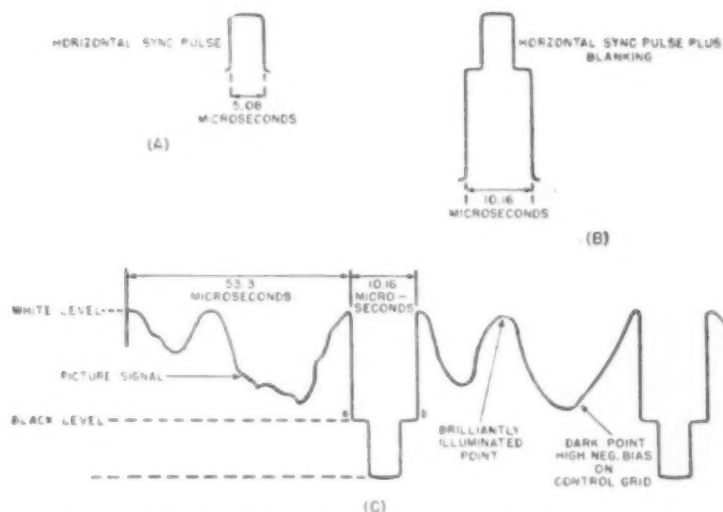
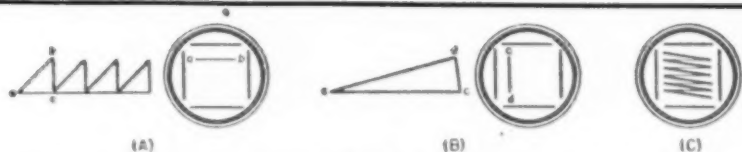
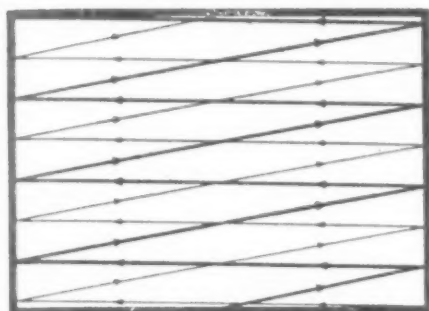
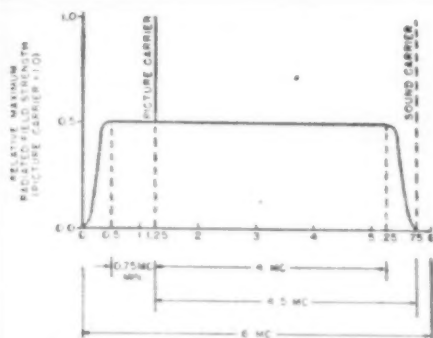
ning is an electronic process; first, the electron beam at the pickup tube, under control of an electron gun, moves across the photosensitive mosaic left-to-right and top-to-bottom progressively gathering the light distribution off the mosaic. And, second, by a similar process the electron beam in the picture tube, also under control of an electron gun, moves across a fluorescent screen and reproduces the original variations in light and dark. To reproduce the picture accurately it is necessary that the electron guns of both tubes direct their beams at the same relative position on both screens for any given instant. Therefore, the transmitted signal not only contains picture information (actual variations in light and dark) but also the necessary signal (synchronization pulses and blanking) which keep the electron beams in step.

The scanning process is performed by sawtooth voltages similar to those used in an ordinary cathode-ray oscillograph. As demonstrated in Fig. 3A, the slow linear rise of the horizontal sawtooth voltage moves the electron beam from left to right (a to b) across the screen in approximately 53 microseconds. When the beam reaches the right side the faster change in voltage of the sawtooth, rapidly returns the beam from right-to-left (b to a) in approximately 10 microseconds. This motion is repeated 15,750 times per second and produces line ab on the face of the scope, just as it would if applied to the horizontal deflection plates of an ordinary oscillograph. However, in the television cathode-ray tube we not only apply a horizontal sawtooth but also a much slower vertical sawtooth. Now with the vertical sawtooth of 60 cycles-per-second applied to the vertical plates as shown in Fig. 3B and with no sawtooth applied to the horizontal plates, the linear rise of voltage would move the beam from top-to-bottom (c to d) in approximately 15,400 microseconds. When the beam reaches the bottom the faster change in voltage of the sawtooth returns or retraces the beam in approximately 1250 microseconds (d to c). If we apply the sawtooth voltages to both sets of plates, Fig. 3C, the beam is moved rapidly across the screen (horizontal sweep) but at the same time the beam is moved slowly down the screen as

(Continued on page 110)

The National Safety Council's miniature "Safe Home" was the subject of what is believed to be the first safety telecast in history. This telecast took place over Television Station WBKB, the Balaban & Katz station located in Chicago.





Multi-Band 30 WATT TRANSMITTER



Fig. 1. The transmitter constructed in two separate units: transmitter proper and power supply.

By McMURDO SILVER

Plainville, Conn.

A masterpiece in miniature with dual-crystal control, and built-in antenna-matching network.

LOOKING forward to the period slightly after V-Day when the amateur radio operator will be permitted to resume practice of his hobby, which has stood his Uncle Sam in such good stead in two successive wars, is responsible for the equipment here described. It is entirely possible that, in the normal bustle of peacetime amateur activity, that the order of contemplation leading up to its creation might never have been indulged.

During enforced quiet evenings thought seemed to turn continually to amateur equipment. Consciousness gradually developed that there was no design, clean-cut and workmanlike, to which the amateur, beginner or experienced "oldtimer," seeking serious portable gear, could turn with the assurance that if he followed straight through on a clearly defined path he would come out with a shipshape rig. True, innumerable amateurs have designed and built such equipment for themselves, but each was an individual job involving a considerable amount of tinkering and puttering about to finally get it to work acceptably. It occurred to the writer, as he contemplated this prob-

lem, that such leisure hours as he had after devoting most of his time to the war effort might be put to good use trying to translate the excellence and dependability, coupled with the desired easy serviceability, of military radio equipment into a solution of this problem.

The result is pictured in Figs. 1, 2 and 3, and diagrammed in Fig. 4. Unfortunately the photograph of Fig. 1 ran so dark as to lose the label-detail of the cigarette package visible between the transmitter proper and its 115/125 volt, 50/60 cycle a.c. power supply.

Nevertheless the white object with the dark center "bulls-eye" is a standard, regular-size package of cigarettes which was placed in the photo just before it was shot to dramatize the compactness of both units. Soon to be produced as factory-built and tested equipment by the Grenby Manufacturing Co., of Plainville, Conn., they also will be available as kits for those desiring to "roll their own," while the always-difficult-to-produce-at-home metal panel, chassis and cabinet similarly will be commercially available to the trade.

This course is pursued with the

thought of giving maximum possible assistance to amateurs desiring to build such units but already having many of the standard commercial parts on hand. To those interested, it is more than probable that their junk-boxes will yield up the small number of needed parts even today, so that they may get their hands back in, and get ready for the opening gun of resumed amateur operation by building replicas at once. Such replicas may be tested upon dummy antennas for which a 115-volt, 15-watt lamp is a good substitute. Despite its nonantenna-like impedance, such a bulb will function very nicely as a dummy antenna for this transmitter, since the built-in antenna-matching network will feed almost any kind of antenna at all—from a couple of feet of wire up to a telephone line!

The 8" long by 5" high by 3½" deep box of 1/16" aluminum, painted with Navy grey enamel at the left of Fig. 1 houses the entire M.O.P.A. transmitter with its rear view in Fig. 2 and its "engine-room," or bottom view, in Fig. 3, left. The circuit, Fig. 4, shows that the basic design uses a 6V6GT beam tube as an oscil-

lator-frequency multiplier, followed by an HY65 30-watt-input beam power amplifier in the final stage. Visible just in front of the 6V6GT oscillator tube in Fig. 2 is the dual crystal socket, a wartime development designed to accept simultaneously two of the small, rectangular Signal Corps type FT243 crystal holders such as will no doubt be standard amateur items after the war.

The installation of two crystals permits operation upon either crystal's fundamental frequency, as well as upon appropriate multiples thereof by multiplying frequency in the Tri-tet oscillator circuit, in the final amplifier, or both. Either crystal is selected from the panel by a conventional type of three-position slide switch which was redesigned especially for this and similar applications by eliminating low-grade insulation and substituting low-loss phenolic, together with large-area silver-plated contacts. Crystals are labeled X1 and X2 in Fig. 4, with their selector switch S1.

Harmonic oscillator operation is insured by inclusion of the tapped cathode coil, L1, in the oscillator cathode circuit. Switch S2, identical to S1, allows selection of the entire coil for 3.5-mc. crystals, a smaller portion thereof for 7-mc. crystals, or the short-circuiting of the entire coil for straight-through operation with any crystal frequency between 1750 and 30,000 kc. L1 is visible just to the upper right of the oscillator tube socket seen at the lower left of Fig. 3.

The oscillator plate circuit is conventional in that it uses a 100- μ fd. "APC" type of ceramic-insulated variable air capacitor to tune coil L2, which is wound upon a commercial Polystyrene form $\frac{3}{4}$ " long having five pins, of which only two are used for winding terminations. Winding data for all coils is shown in the parts list of Fig. 4. The 3.5-mc. coil also will cover 7 mc., while the 14-mc. coil covers right on through to 30 mc. when the oscillator is putting out at a high crystal harmonic—and it is possible to get useful output at 28 mc. from a 3.5-mc. crystal in this little rig.

Mazda #49 dial lamp, B1, indicates crystal r.f. current at the same time it acts as a fuse to prevent crystal fracture in event of overloading or improper adjustment in tuneup. This 60-ma. lamp, together with its counterpart, B2, in the final plate circuit, both are located upon the front panel next to the two switches which control crystal and oscillator cathode circuits. They make unnecessary the use of meters in initial tuneup or operation, since indicating the two vital currents in the circuit, tuneup for maximum power output on crystal fundamental or harmonic frequencies is made easy—two 10-cent lamps replace two seven-dollar meters, protect the crystal, and save large "chunks" of space.

The AMP. knob to the right of the OSC. knob in Fig. 1 controls the 100-

μ fd. "APC" tuning capacitor for the final amplifier plate circuit, seen to the left of Fig. 2 just behind the horizontally-mounted HY65 power amplifier, and to the right of its plate coil, L5. In Fig. 2 it can be seen that the HY65 socket (tube plate in a vertical plane) is mounted to the right of a vertical partition joining panel and chassis into a rugged structure; the tube itself is projecting to the left through a $1\frac{1}{2}$ " hole. This partition provides essential shielding between oscillator and amplifier circuits, so that the whole transmitter runs "cool" without any trace of undesired oscillation or instability, and without need for always-tricky neutralization. The grid lead to the amplifier is carried "upstairs" through the ceramic stand-off insulator seen near the HY65 socket in Fig. 2, while its plate lead is carried "downstairs" to r.f. choke L4 by a second such insulator near the HY65 plate cap. C6, C7a, R7 and R8 are all mounted closely about the HY65 socket for short, direct leads, the common connection of R7, R8 going to a dead lug on the HY65 socket.

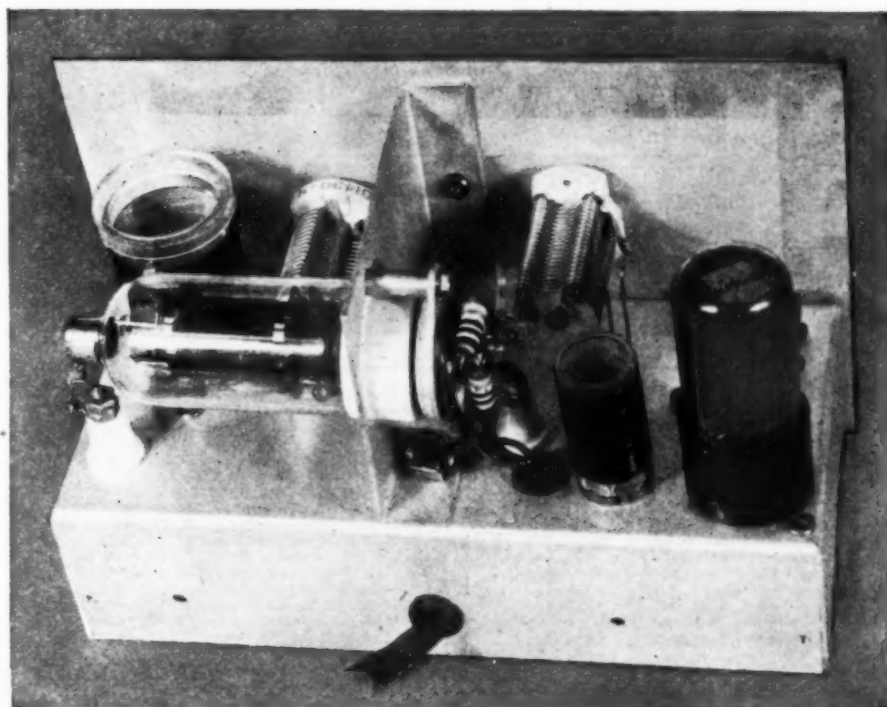
The antenna-matching network is a simplified pi-circuit, involving the addition to the basic circuit of C9a, C9b, C9c, and S3. S1, S2, and S3, each has an open center position, with two separate closed positions, one at each end. Each is thus a single-pole, two-position switch plus a neutral, or open, position. C9a is the fine antenna-matching adjustment, and could do the entire job, in fact, were it available in sufficient capacity. Its procurable 140- μ fd. maximum is not sufficient to take care of all possible antennas to be anticipated in portable operation, so

it is padded up through S3 which adds C9b or C9c in parallel with C9a when required. This type of antenna-coupling circuit is used widely in serious commercial equipment, and its virtues are so great that it is to be strongly recommended to amateurs. It is ideal in choice both as to antennas and frequencies—a great boon indeed to easy tuning and efficient power transfer.

The transmitter construction is so clearly illustrated in Figs. 1, 2 and 3 as to deserve little further comment here—except to say the panel, chassis, and cabinet drawings may be had on application to the writer at no charge other than for postage and blueprinting. Operation is so clean and straightforward as to be a delight. Keying is done in both cathode circuits to minimize drain on the power supply in portable operation, when it presumably would be a vibrator-type unit driven from a 6-volt car storage battery. Chirping is noticeable by its absence, even though in keying, the plate voltage of the a.c. power unit illustrated varies from about 325 volts at full 85-ma. load up to 490 volts at no load!

Tuneup initially involves removal of the HY65, plugging of a key into the KEY jack on the front panel, insertion of appropriate oscillator crystal and coil, and tuning of OSC. dial for minimum crystal current as indicated by XTAL bulb, and as found just on the low-C side of oscillation stoppage. The HY65 is then inserted and its plate circuit tuned for minimum-current resonance-dip. Oscillator and amplifier tuning is trimmed up a bit, and the ANT. capacitor is adjusted for greater AMP. plate current lamp brilliancy at resonant dip—when all

Fig. 2. Rear view of the transmitter proper. The HY65 tube should be mounted horizontally so that all leads to the tube are as short as possible.



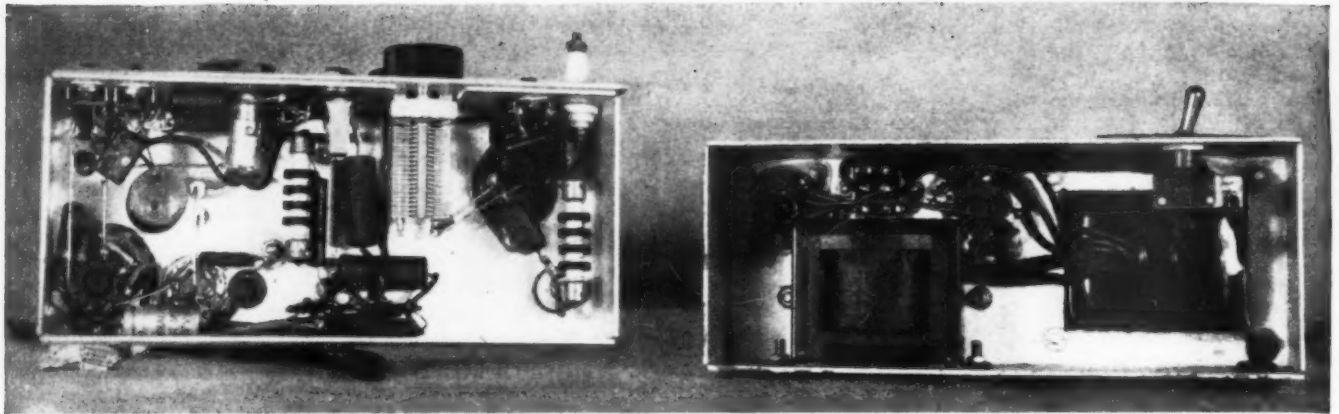


Fig. 3. Under-view of both chassis. All components should be spaced properly and wired so that no interaction will occur.

is done. This latter condition corresponds to maximum brilliancy of the 15-watt lamp used as dummy antenna initially.

The power supply, also of 8" by 5" by 3½" size, is mounted on a conventional chassis, no cabinet being necessary to protect its relatively rugged component parts, nor desirable in terms of heat confinement in a neces-

sarily small cabinet. This power unit is built as diagrammed—with a double-section filter involving three electrolytic filter capacitors contained in a single, instantly replaceable plug-in unit like a vacuum tube, and two filter reactors. This is because the power supply also is intended to power a companion receiver when not used for transmitting, and the receiver benefits

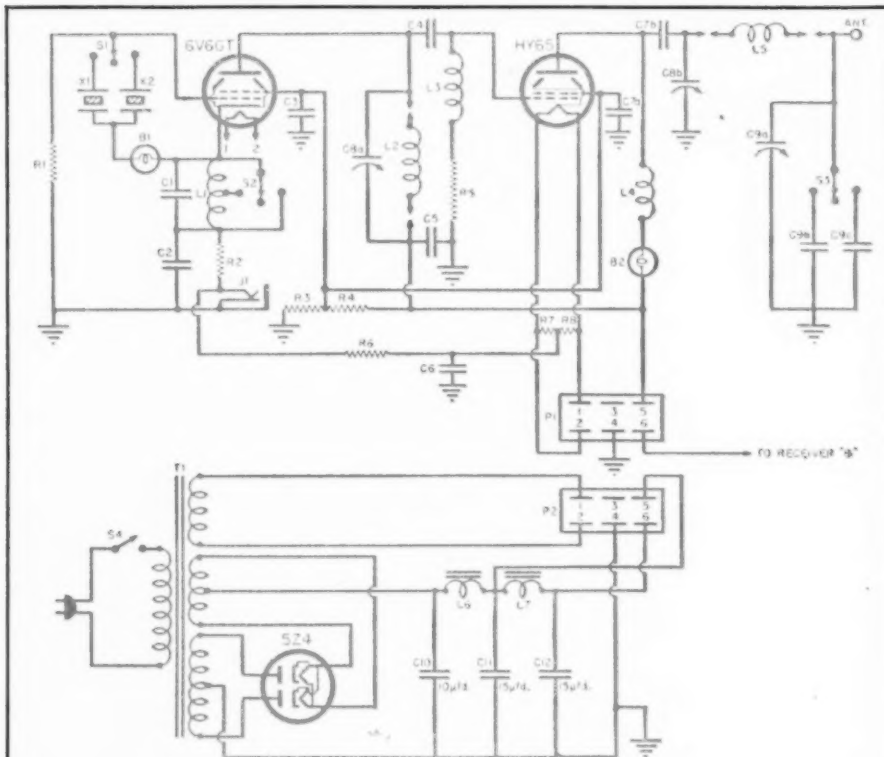
by more filtration than is needed by the transmitter. Thus, for transmitter operation alone, the reactor seen above the chassis might be omitted, as might C12, since both are used only in receiver operation. The circuit diagram appears at the bottom of Fig. 4, as does a listing of essential electrical component parts.

This compact little assembly, each unit of which is almost small enough to slip into an overcoat pocket, is a serious DX-worker, indeed, if power inputs and outputs and antenna characteristics be considered. Power input to the final stage with the supply illustrated will be about 16.25 watts—325 volts at 50 ma.—, with the output at around 60% efficiency, or about 10 to 11 watts. This is on crystal fundamental. On second harmonic operation output falls off a bit to about 8 watts, and drops further to about 6 watts on 3rd and 4th harmonics of crystal frequency. Outputs will go up proportionately if effective plate voltage is raised to 450 volts, the top rating of the HY65, when 20 watts output or a bit better may be expected on crystal fundamental frequency. Such powers are not to be overlooked by the beginner, or by the "oldtimer" either, for the latter knows that they are capable of plenty of DX under halfway decent conditions. And its neither good sense nor good sportsmanship to use a "rock-crusher" to put out a signal louder than needed for essential communication at the price of excessive nearby interference. Nor should it be forgotten that doubling power will only give a 3-db. increase in audible receiver volume at a distant point—no little as to be barely audible!

The same type of basic design and structure here illustrated need not be confined to a small unit such as the r.a. p.a. combination. Its inherent cleanliness can be retained, and power capability "blown up" by simply increasing size as necessary to accommodate a 6L6 oscillator driving an 814, or even an 813 at 360 watts plate input, approximately 260 watts antenna output! While it is true that using but low-frequency crystals, some loss of output will result when tak-

(Continued on page 141)

Fig. 4. Wiring diagram of the transmitter shows simplicity of design.



C₁—50-μfd. mica cond.
C₂, C₃, C₄, C₅—0.1-μfd. @ 600-v. oil cond.
C₆—100-μfd. mica cond.
C₇, C₈—0.1-μfd. mica cond.
C₉, C₁₀—100-μfd. var. cond. "APC"
Hammarlund
C₁₁—140-μfd. var. cond. "APC" Hammarlund
C₁₂—150 μfd. mica cond.
C₁₃—300-μfd. mica cond.
C₁₄, C₁₅, C₁₆—10-μfd. @ 500 v., 15-μfd. @ 450 v., 15-μfd. @ 450 v. (Single plug-in unit)
R₁—50,000-ohm, 1-w. res.
R₂, R₃—250-ohm, 5-w. res.
R₄—50,000-ohm, 2-w. res.
R₅—10,000-ohm, 5-w. res.
R₆—15,000-ohm, 1-w. res.
R₇, R₈—50-ohm, ½-w. res.
J₁—Single closed circuit "imp" jack

P₁—Jones #306 plug
P₂—Jones #306 socket
S₁, S₂, S₃—S.p.s.p. Stackpole slide switch XX insulation
S₄—S.p.s.t. toggle switch
T₁—Power trans. (Stancor P6012)
L₁—18t #20 P.E. spacewound 1", tapped 7 turns from cathode, Amphenol #24 form
L₂—45t #20 P.E.—closewound (3.5 mc.)
27t #20 P.E.—spacewound 1" (7 mc.)
9t #20 P.E.—spacewound 1" (14 mc.)
(All on Amphenol #24-5H coil form)
L₃, L₄—2.5 mh. r.f. choke
L₅—37t #20 P.E.—spacewound 1½" (3.5 mc.)
23t #18 P.E.—spacewound 1½" (7 mc.)
14t #18 P.E.—spacewound 1½" (14 mc.)
5t #18 P.E.—spacewound 1½" (28 mc.)
(All wound on Amphenol #24-4P coil form)
L₆, L₇—Filter reactors Stancor C-1709
B₁, B₂—Mazda #49 dial lamp



LET'S TALK SHOP

With **JOE MARTY**

Field Editor, RADIO NEWS

IN PREPARING for postwar operation of radio and electronic service establishments, there are a number of factors which should be taken into consideration by men who are now in the business, as well as those who intend to enter it. As you all know, competition will be very keen. The present large volume of radio repairs will be subject to a sharp drop immediately after new civilian sets are available. There will be a great influx of returning servicemen who will desire to get into the retail sales and service field of the radio and electronic industry.

The existing service shop will be "hard-put" to hold its present position in the face of this type of competition, especially since it must be remembered that a returning Serviceman will be trained at government expense. Most important, this training probably will be along the lines of advanced servicing in the ultra-high-frequency fields, in which we expect most of the progress after the war. In addition, the government will lend these men a sum not exceeding \$5,000 for the establishment of their own businesses. Therefore, you should very carefully examine your own position in your community and find exactly how you can best meet this competition and retain for yourself a fair share of the business which is available.

One of the ways that this can be accomplished is to go into the wholesale service business. By this, I mean the individual serviceman that does servicing and installation for retail sales dealers who do not have service establishments of their own. This manner of servicing is quite a bit different from the ordinary and I shall discuss at length some of the problems encountered in this type of work.

There are several things generally necessary for the successful operation of this type of business. First, you must have unquestioned personal integrity, and must have the respect of the dealers with whom you do business. Since you and the dealer both are operating in the same territory, if any attempt is made to deviate from honest business policies, the dealer, of course, will not give you his work. You must realize that the dealer takes a tremendous risk in sending an independent serviceman into the homes of his customers, unless the serviceman is thoroughly honest and will not chisel in any way. Second, no sale of radios can be permitted since this is in direct competition with the dealer. In other words, if you are in the wholesale radio service business, it generally is expected

that you will not sell radio sets, excepting for the dealers for whom you work. Third, your establishment will need more men in order that the calls and the service work can be done in an orderly and efficient manner and with as little loss of time as possible. Fourth, it is obvious that if you have more men, you must have more equipment for these men to work with. You should not under any circum-

EDITOR'S NOTE: Mr. Marty will address the Philadelphia Servicemens Association on Tuesday, February 20th. His subject will be "The Future of the Radio Serviceman."

stances stint yourself as to equipment since it is only by taking advantage of short-cut efficient servicing methods that you will be able to turn out the necessary volume to show a profit. The fifth thing that is needed is more space. If you have been operating up to this time as an individual, or a shop with one man and limited space, you must consider going into larger quarters for the new operation. Of course, a larger stock of parts is imperative where the volume is larger than you have been accustomed to in a one-man operation.

Types of Operation

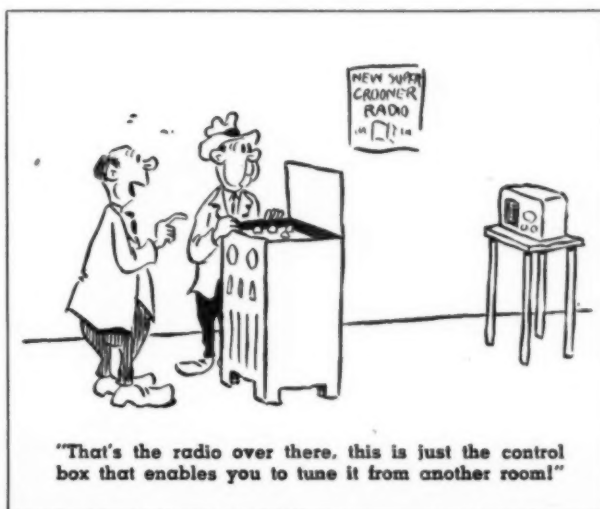
There are two types of wholesale operation, the first of which the radio serviceman picks up the sets from his dealers and takes them to his own shop for repair. This is, of course, the least involved method of operation because there is very little selling

attached to it. The jobs under this type of operation may, therefore, be handled on a fixed charge basis, charging so much per job per set, or they may be handled on a time and material basis for which the charge is made. Usually a discount is extended to the dealer in any case. This discount should be varied, depending upon the volume which any one dealer gives to the serviceman. If you have a dealer that has a relatively few sets to be repaired, I would suggest that he be placed on a lower discount rate than the dealer who gives you a large number of repair jobs. In this type of operation the serviceman furnishes tubes and the necessary parts for the repair of a receiver.

The second type of operation is one where the serviceman actually assumes complete charge of the dealer's service department. Under this plan, the serviceman makes the calls as they are received by the dealer. He estimates the amount of repair, does the repair work and returns the set to the customer's home. Immediately you will realize that this is a more complicated type of procedure yet it offers much to the dealer in the way of service, which he cannot furnish if he does not have a service department of his own. Under this method, the estimated charge to the customer is the final retail selling price. From that price, the dealer is entitled to a discount, as mentioned above, depending upon the volume of work done. This discount should be figured very accurately and fairly, in order that the dealer may make money on his service department and also provide adequate compensation for you.

Arrangements should be made with the dealer to compensate the serviceman for the sales of all radios and appliances sold on the job. Some commission, probably less than the regular salesman's commission, generally is extended.

In some cases dealers will want to furnish their own parts for the repairing of



"That's the radio over there, this is just the control box that enables you to tune it from another room!"

PRACTICAL RADIO COURSE

By ALFRED A. GHIRARDI

Part 31. Further study of spurious interfering responses that can occur in AM superheterodyne receivers. Methods of attenuating their effects are discussed.

THE remaining forms of spurious interfering responses that can occur in AM superheterodyne receivers will now be analyzed.

Local-Oscillator Radiation Interference

The function of the local oscillator in a superheterodyne receiver is to generate a stable, unmodulated high-frequency signal that is fed to the mixer or frequency-converter where it acts upon the "desired" incoming modulated signal to produce a similarly-modulated signal of specially-chosen new frequency known as the intermediate frequency (i.f.). Unfortunately, however, unless special precautions are taken in the design of the receiver all of the r.f. energy (signal) generated in the local oscillator will not be confined solely to its proper use in the mixer or frequency-converter stage. Since the oscillator is virtually a low-powered radio transmitter, interfering energy (signals) from it may find its way into neighboring receivers by any one or more of the following five different paths:

- (1) Feedback through the mixer and r.f. amplifier circuits and wiring to the antenna circuit of the receiver and subsequent radiation of the energy from this antenna circuit over a limited area to other receiving antennas in the vicinity.
- (2) Coupling between the filament and plate supply leads of the oscillator.
- (3) Direct coupling between the oscillator and antenna circuit.
- (4) Leakage back to the power supply line (in line-operated receivers only) which may either conduct it to other receivers through power line, or else radiate it to nearby antennas.

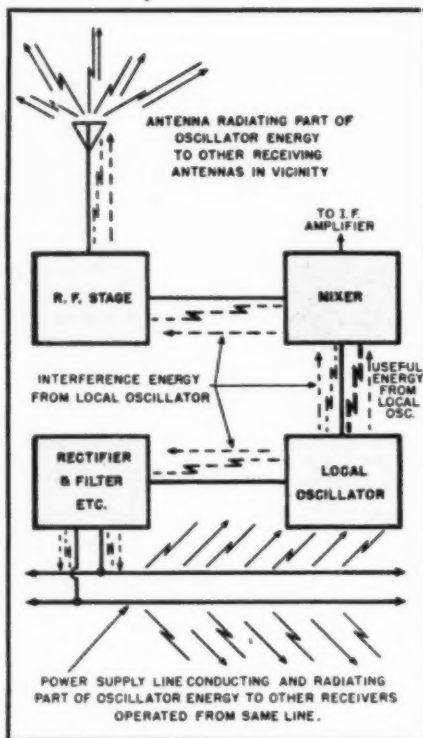
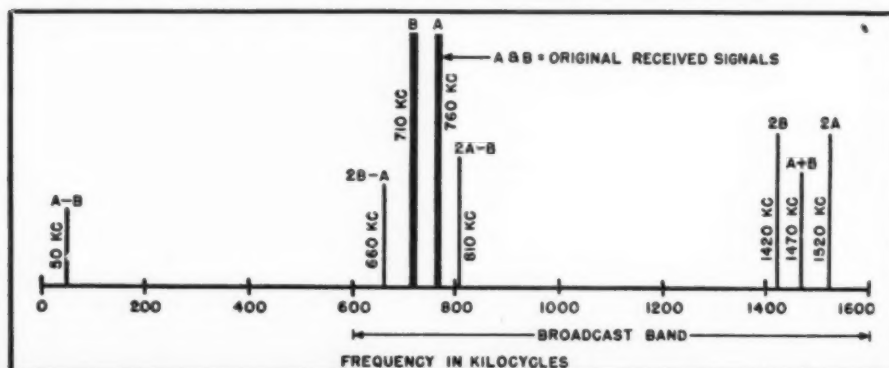


Fig. 1. How part of the r.f. energy of the local oscillator may find its way to the receiving antenna and power-supply line and be radiated from them to other nearby receivers, causing interference.

- (5) Radiation over a limited area from the metal case of the receiver.

Fig. 1 illustrates the paths by which the oscillator energy can feed back in the first four cases. The first of these usually is found to be the worst offender in causing interference, and is the most difficult to control.

Fig. 2. Cross-modulation signal frequency products obtained by rectification of the two original received signals of frequencies A (760 kc.) and B (710 kc.). The new harmonic frequencies, 2A and 2B, and the new combination frequencies, $2B-A$, $2A-B$, and $A+B$, may cause interference since they all lie within the standard broadcast band.



The interference caused in other receivers which may pick up this energy is evidenced by a "whistle" on a particular desired station, appearing, then disappearing, and changing in frequency more or less at random. This interference becomes prevalent and of special importance in congested metropolitan areas where many receivers are located close together in apartment houses, are fed from closely spaced antennas and derive their operating power from a common electric light circuit. Trouble may come about in the following way if the owners of such receivers are in the habit of listening to two stations that differ in frequency by the amount of customarily employed intermediate frequencies.

For example, in a community having a popular station transmitting at 700 kc. and another at 1150 kc., receivers using a 450 kc. i.f. when tuned to the 700-kc. station will have their local oscillators set at $700 + 450 = 1150$ kc. If these 1150-kc. local oscillators radiate energy from these receivers in any one or more of the five ways previously enumerated, it will cause a "whistle" in those nearby receivers which are tuned to the 1150 kc. broadcasting station. The whistle will change pitch as the tuning of the radiating receiver, or that of the other receivers, is manipulated about the exact tuning point. Also, when the tuning of a superhet is varied from one end of a band to the other (as is customary when "searching" for station programs) the local-oscillator frequency is being varied throughout its entire range. If the oscillator radiates appreciable energy, doing this may be the equivalent of sending out signals on 20 or 30 different wavelengths from the receiving antenna. These will be picked up by nearby receiving antennas—causing momentary interfering "whistles" to appear in the receivers.

In modern radio receivers the intensity of the radiated oscillator energy is reduced by using one or two stages of tuned r.f. amplification ahead of the oscillator and mixer, by more careful design of the oscillator coupling circuits, by better shielding of the oscillator circuits, and by use of a high-impedance type antenna coil designed so that its resonance frequency (when tuned by the average antenna capacitance) lies outside of the receiving band of frequencies.

In cases where existing receivers either are causing such interfering

radiation, or are affected by it, the following measures should be tried:

(1) Install an r.f. filter in the power-supply circuit of the receiver affected.

(2) Install a good noise-reducing antenna on the receiver causing the radiation.

(3) Realign the radiating receiver to a new i.f., also readjusting the gang condenser trimmers and low-frequency pad correspondingly.

(4) Reduce the oscillator grid-leak resistance value.

(5) Reduce the excitation (plate voltage) of the radiating oscillator.

(6) Position the leads of the radiating receiver so as to reduce oscillator-antenna coupling.

(7) Reduce the size of the antenna used with the receiver troubled by the interference.

(8) See that a good ground is used with the radiating receiver.

(9) Completely shield the oscillator stage, and filter its supply leads.

The receiver illustrated in Fig. 3, which covers the broadcast band and short waves from 5.1 to 24 mcs. is an example of what may be accomplished in the way of elimination of oscillator radiation by careful design. It is an 11-tube low-radiation superheterodyne receiver designed for shipboard use, in which are incorporated special circuits and features which prevent the oscillator from feeding into the antenna and radiating interference which could be picked up by enemy submarines or surface craft, so disclosing the position of the ship to the enemy. It is designed for use as communications equipment by the Merchant Marine, U. S. Navy, and Signal Corps. In this receiver, oscillator radiation is cut down to such a low point that it cannot be detected 25 feet away. Notice the unusually thorough shielding of the preselector and oscillator coils and circuits by means of separate shielding compartments. Of course, such thorough shielding adds materially to the cost of the receiver, so it is not ordinarily employed on medium-priced home receivers.

Over-all I.F. Feedback Interference

Superheterodyne receivers that employ an i.f. of 175 kc. often are unable to receive 700-kc., 1,050-kc. and 1,400-kc. stations without a strong interfering whistle being heard. This whistle originates through over-all feedback. Some of the harmonics of the 175-kc. i.f. energy passes from the second detector through the output system of the receiver and finds its way back to the input. The fourth harmonic of 175 kc. is $4 \times 175 = 700$ kc.; the sixth harmonic is 1,050 kc.; and the eighth is 1,400 kc.—all within the broadcast band. A receiver employing an i.f. of 465 kc. can be affected by this trouble at only one point within the broadcast band—at 930 kc.

If this trouble is inherent in the receiver, and if it is important to obtain reception at these frequencies without the accompanying interfer-

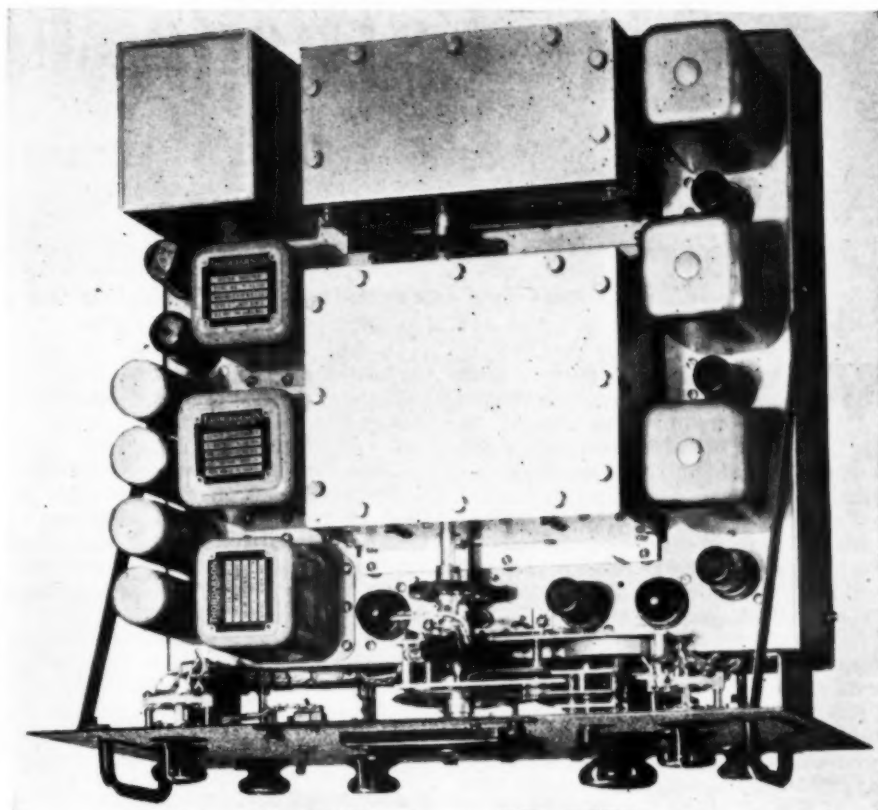


Fig. 3. Special 11-tube low-radiation superheterodyne shipboard-type receiver, incorporating special circuit and other features which prevent the oscillator from radiating to other receivers. Without these special features, radiating interferences would occur, which could be picked up by enemy submarines or surface craft, disclosing the position of the ship to the enemy.

ing whistle, slight retuning of the i.f. transformers will shift the interference to adjacent signal channels where it may not be so objectionable.

Cross-Modulation Within the Receiver

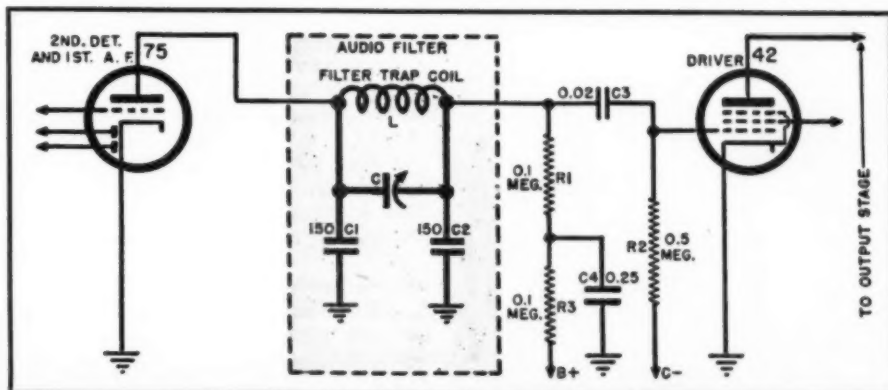
Two signals are said to be *cross-modulated* when the program of the undesired one superimposes itself upon that of the one it is desired to receive. This type of interference is distinctive in that the secondary (interfering) modulation is directly associated with the carrier being received, and is not heard except when the receiver is tuned to the desired carrier. Such cross-modulation interference is prev-

alent in metropolitan areas—in the vicinity of very strong stations. In some cases more than one station may be causing cross-modulation interference on another. Occasionally, cross-modulation even may show up by producing extra responses at random points on the tuning dial, usually appearing as a mixture of two signals and their respective modulations. Cross-modulation may occur in a t.r.f. receiver as well as in a superheterodyne.

Cross-modulation is caused basically by demodulation of a strong interfering signal somewhere in the receiver—usually in the r.f. stages. Nonlinearity of the circuit element or tube, of

(Continued on page 100)

Fig. 4. Audio filter circuit employed in the amplifiers of Philco 200-series high-fidelity receivers to attenuate the 10-kc. beat note prevalent in superheterodyne receivers. This filter cuts off sharply all frequencies over 8000 cycles.



The Cathode Follower

By G. DONALD HENDRICKS

Instructor, AAF

Functional operation of the cathode follower. This circuit will find increasing popularity in the postwar period.

WHEN the present war ends and civilian radio-electronic equipment begins to move off the assembly line, several circuit changes will be included as improvements.

Perhaps the most common circuit with which the radio serviceman, amateur, and engineer will have to contend will be the cathode follower or so-called cathode-coupled stage.

The cathode follower receives its name from the fact that the output is taken off the cathode and consequently the output voltage follows the input signal in phase. See Fig. 1.

Briefly, when the grid goes negative, for instance, the conduction of the tube is reduced. This results in a decrease in current flow through the cathode resistor. A decrease in current will cause a drop in voltage at the cathode. Therefore, it can be seen that if the cathode serves as the output source there will be no phase shift through the stage. The cathode follows the grid—thus the name, cathode follower.

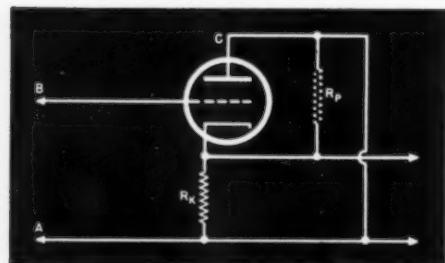
The above statements assume, of course, operation on the linear portion of the tube's characteristic curve.

First used in England, the cathode-coupled stage appears in British patent 419298 (1936), and later patent Number 529044. Its early uses were more or less confined to time-base circuits. At the present time the circuit is being used in video work and for impedance matching. Such a stage enables step-down of impedance (output-stage-to-line) from 10,000 ohms to 52 ohms, for instance, without attenuation of frequencies ranging from 15 cycles to several megacycles.

Principal applications after the war will be:

- 1.—Impedance matching to audio lines.
- 2.—Line to amplifier matching as an "inverted triode."
- 3.—Video coupling in television.

Fig. 2. A.c. condition of Fig. 1.



- 4.—FM detection circuits.
- 5.—Automatic frequency-control devices.
- 6.—Oscilloscope probe.

Gain through the stage is less than unity, yet in practice this would represent no more voltage loss than would be encountered in a conventional transformer or plate-load resistance-coupled stage designed to pass the same range of frequencies with high fidelity.

The derivations of design equations are included as appendices. This action was taken for the sake of reading ease. Elimination of derivations from the body of the article prevents clogging the presentation with material which

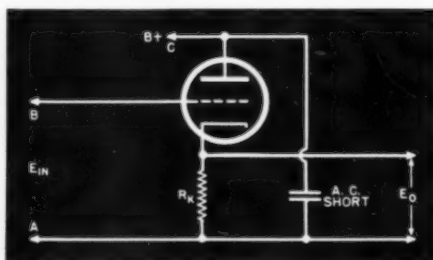


Fig. 1. Cathode-follower circuit.

might cause the average radio man to pass up the article as too difficult. It no doubt will be the average reader who will find the greatest need for a complete mastery of the cathode follower.

It will be seen from an examination of Fig. 1 that the plate is by-passed to ground. This by-pass represents an a.c. short to earth, therefore we are enabled to redraw the circuit as shown in Fig. 2. Fig. 2 shows the a.c. conditions in a cathode follower.

In Fig. 2 it will be noted that a dotted resistor is shown between cathode and plate. This resistor, represented by R_p , is the internal resistance of the tube. In view of the fact that the resistance is between cathode and plate, and the plate is shorted directly to ground (as far as any signal voltage is concerned), it will be seen that the so-called plate resistance is effectively in parallel with the cathode resistor. The cathode resistor will be known henceforth as R_k .

A tube's amplification factor is known as μ (Greek letter mu) and is the ratio dE_p/dE_g at a stated I_p . Expressed in ordinary language μ represents the rate of change in plate voltage with change of grid voltage, with

the plate current remaining constant.

The d is often replaced by Δ (Greek letter delta) and means a change, decrement or increment . . . a differential.¹

The μ of a tube may be found in a tabulation of its characteristics as provided by the manufacturer, or it may be found by simple measurements taken from certain circuits, or calculated from a set of tube curves.

Consider a triode whose μ is 10. Plainly stated, adding 50 volts to the plate might change its plate current 2 ma. It would require but 5 volts change on the grid to create a 2 ma. change in the plate current. It is quite logical, therefore, to assume that a voltage change on the grid has the same effect as a voltage change on the plate if the plate voltage is μ times the grid voltage. Thus a voltage E_g when it reaches the plate of a tube is equal to μE_g .

The foregoing explanation has been made to prepare the reader for an equivalent circuit of the cathode follower. Since it has been shown that a voltage change E_g on the control grid multiplied by the tube's amplification factor represents a certain plate voltage change, we can say that the voltage between points BC in Fig. 2 is equal to the voltage AB times μ .

Therefore we are justified in replacing the tube with a fictitious generator between points BC and giving the generator a voltage μE_g . See Fig. 3a.

Fig. 3a is an equivalent circuit which most radio students find easy to understand, while Fig. 3b is the textbook method of showing the same circuit.

Reduced to the equivalent circuit it is much more simple to shake out the necessary design equations and study the theory of operation. Polarity may be assigned to various points in the circuit, and certain voltages or results calculated.

A clear method of considering feedback in the cathode follower is as follows:

When the input signal goes positive, the grid is given a plus potential with respect to the cathode. An increase of grid voltage, however, causes the tube

¹ The mathematically rigorous d represents an infinitesimally small change while Δ represents a larger change. Δ is most common in graphical representations relative to vacuum tube equations. Thus we state the equation as $\Delta E_p / \Delta E_g$ with $I_p = K$ (K is a constant.)

to conduct more heavily. Greater conduction causes an increase in cathode potential. When the cathode goes positive it effectively reduces the initial upward swing of the grid by reducing the actual potential difference between the grid and cathode. Thus we say that degeneration takes place. Controlled degeneration reduces distortion and therefore improves the output fidelity of the stage. Degenerative feedback is an important feature of the cathode follower.

For the sake of identity, feedback in the stage will be called e' (e prime). Taking e' into account, and calculating stage gain, we find the following relations, from the equivalent circuit:

$$e_g = e_{in} - e'$$

$$i_p = \frac{\mu e_g}{R_p + R_k}$$

$$e_o = i_p R_k$$

Gain is a ratio of output voltage to input voltage, or

$$G = \frac{e_o}{e_{in}} \cong \frac{R_k}{\frac{1}{G_m} + R_k} \dots \dots \dots (1)$$

Equation (1) is approximate and serves for design purposes. Appendix 1 and 2 give two rigorous derivations of

E_p	Plate voltage
e_g	Grid voltage
e_{in}	Input voltage
e'	Feedback voltage
e_o	Output voltage
μ	Amplification factor
G_m	Mutual conductance
R_p	Plate resistance
R_k	Cathode resistor
G	Gain (voltage)
d	Differential
Δ	Change in
i_p	Plate current
Z_o	Output impedance
Z_i	Impedance to be worked into
\gg	Much greater than
\therefore	Therefore
\sim	Alternating signal source
\cong	Approximately equal to

Table 1. Definition of symbols used.

the expression for gain as worked out using Figs. 3a-b. Both evolve into equation (1) when certain assumptions are made.

In fact, it may be shown that the gain of a cathode-coupled stage is equivalent

Fig. 5. Circuit which may be used to couple a low-impedance source into a high-impedance circuit.

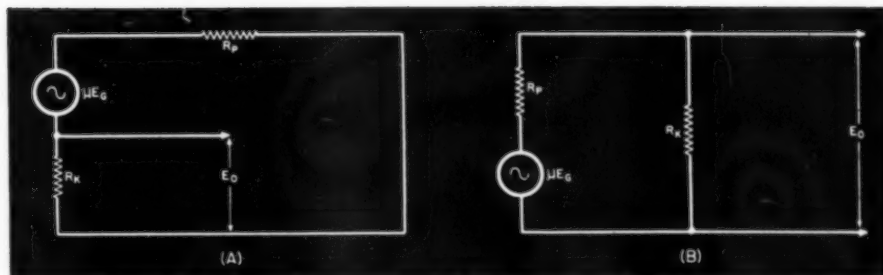
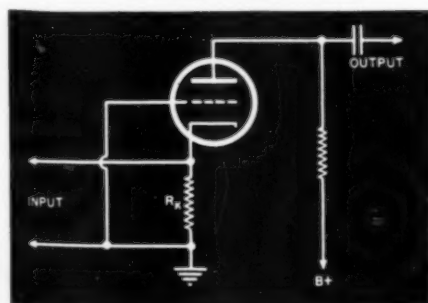


Fig. 3. Equivalent circuits of Fig. 1. (A) The form familiar to most radio students; (B) The same circuit as it appears in present-day textbooks.

to an ordinary plate-load coupled stage using a tube whose amplification factor is $\mu/(\mu+1)$, or less than unity, and whose plate impedance is $1/(\mu+1)$ times the normal plate impedance.

While the above statement is obviously true upon inspection of appendix 1, the simple substitutions are given here for the benefit of the reader.

The equation for gain in an ordinary plate-load coupled stage is:

$$G = \mu \cdot \frac{R_k}{R_p + R_k} \dots \dots \dots (2)$$

If the amplification factor (μ) of this stage is $\mu/(\mu+1)$ and the plate resistance is $R_p/(\mu+1)$, then substituting in equation (2) gives:

$$G = \frac{\mu}{\mu + 1} \cdot \frac{R_k}{\frac{1}{\mu + 1} \cdot (R_p + R_k)}$$

$$= \frac{\mu}{\mu + 1} \cdot \frac{R_k}{\frac{R_p}{\mu + 1} + R_k} \dots \dots \dots (3)$$

If $\mu \gg 1$, then we may say without appreciable error that $\mu/(\mu+1) = 1$ and that $R_p/(\mu+1) = R_p/\mu$. This assumption is made by considering μ much greater than 1. It is known, however, that μ/R_p equals G_m . Therefore R_p/μ equals $1/G_m$.

Completing the rewriting of equation (2) we find that gain is equal to

$$\frac{R_k}{\frac{1}{G_m} + R_k} \text{ which is found to be identical with equation (1), the expression for the gain of a cathode follower.}$$

It is found from the above expressions that the gain approaches unity as the cathode resistor (R_k) becomes large compared to R_p . It is noted in experiments with both high- and low- μ triodes (6SF5 and 6L5-G with a μ of 100 and 17 respectively), that the stage gain changes very slowly with varying values of cathode resistances.

From equation (3), it can be seen that the resistive circuit is equivalent to two resistors in parallel—the fictitious resistance $R_p/(\mu+1)$, and R_k . See Fig. 4.

If R_k is much greater than $R_p/(\mu+1)$, and μ is much greater than 1, then

$$Z_o \cong R_p/\mu \cong 1/G_m$$

This expression affords a convenient

method of determining whether a particular tube will offer the required output impedance.

The above conditions have led to bold statements that an impedance match to low-ohm lines will be close enough to enable almost any cathode resistor to be used. This is untrue, however, since it is quite obvious that the tube must be operated upon the straight portion of its curve.

It is possible to apply the calculated equations only as long as the stage is operated class A. It is also known that a correct impedance match for video frequencies must result in the output stage presenting an image of the line's impedance looking back into the stage.

A new analysis would be necessary if improper bias were used, or if the stage is to be driven to the extent that the grid draws current.

The equation for R_k is worked out

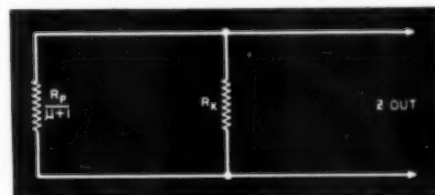


Fig. 4. Circuit used to determine the output impedance of the cathode follower.

in appendix 3. It is found that in order to match an impedance Z_i we must make the impedance of our circuit equal to Z_i . Therefore $Z_o = Z_i$.

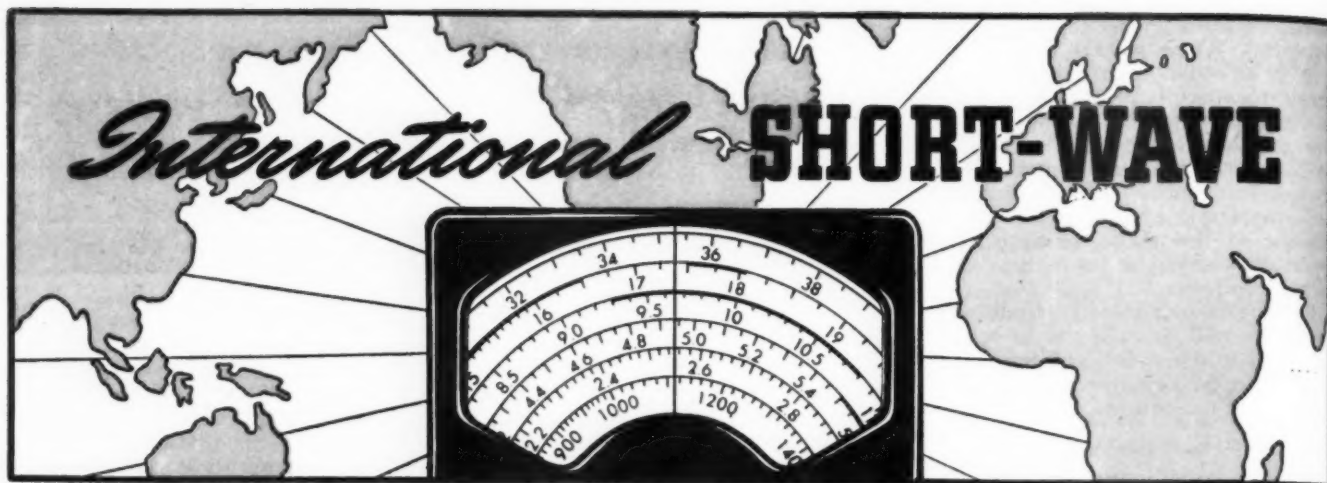
Setting up the expressions and working through we find that in order to make Z_o equal Z_i we must change the variable R_k . Solving for R_k , the equation which will satisfy the above statement is:

$$R_k = \frac{Z_i}{1 - Z_i \cdot G_m}$$

An interesting basic sidelight on the cathode follower is to be found in a statement by F. P. Kenyon in 1938. Mr. Kenyon in one of a series of Ken-o-Talks (No. 9) discussed a preamplifier for low level-high gain stock use.

Mr. Kenyon said, in part: "The circuit possesses numerous advantages over the conventional preamplifier. The first two stages are of the standard resistance-coupled type, but the output stage is somewhat different. This stage is of the type sometimes called a cathode follower. The plate is connected directly to "B" plus and

(Continued on page 98)



Compiled by **KENNETH R. BOORD**

ONE of the most interesting reception reports yet received by INTERNATIONAL SHORT-WAVE is that which came in a few days ago from W. N. Caldwell, Riley Street, Suva, capital of the far-distant Fiji Islands in the Pacific. He writes:

"As station identifications frequently are missed, not all are recorded; it would take weeks to get them all. San Francisco comes in very strong, especially the Philippine Commentator and the Armed Forces programs. The one from Australia is especially strong. There are so many stations broadcasting in German, French, Italian, Japanese, Hindustani, Chinese, and other languages that it is difficult to say which one you are tuned to unless you 'hang on' to the end—in which case you may miss other stations, broadcasting in English. This listener confines himself to news in English. Morse is used on practically all the broadcast bands at present and makes it very difficult, but it's wartime and we must expect this."

Mr. Caldwell writes that he uses a Hammarlund HQ-120, with an ordinary "L" Marconi antenna about 75-feet high, directed North.

Here is a two-day log of newscasts in English picked up in October, 1944, submitted by Mr. Caldwell. Fiji time is 12 hours ahead of GMT; I have converted his local time to EWT in the following:

15.33—San Francisco, daily, 9, 10, 11 p.m. (S-3, good).

9.51—London, daily, 12:30 a.m. (S-2).

15.12—Tokyo, 12:45 a.m. (S-2, jammed).

15.20—Tokyo, 12:45 a.m. (S-3, good).

9.50—Various Spanish-speaking stations, 1 a.m. (S-2 to S-5).

9.67—South American and Mexican stations, 1 a.m. (S-2 to S-5).

9.85—U.S.A., daily, jammed by Morocco, 1 a.m. (S-3).

15.12—Tokyo, daily, 1:15 a.m. (het., S-2).

11.90—Tokyo, daily, 1:15 a.m. (S-2 and S-3, clear).

9.65, 9.69, 12.04, 7.12, 15.42, 11.95,

and 11.82—London, heard daily, 2, 3, 4, 5 a.m. (S-1 to S-4); some London stations are always heard well at 1:45 a.m.; the 9.65 frequency is jammed by Chungking.

7.60—WNRA, New York, heard with news in German, French, and Italian at 2:15, 2:30, and 2:45 a.m., respectively (S-3).

9.50—San Francisco, daily, 2.45 a.m. (S-3 and S-4).

11.90—Tokyo, 2:45 a.m., *messages to Canada from prisoners of war* (S-3-4).

11.72—Armed Forces Radio, San Francisco, 1 a.m. (S-5).

15.23—Berlin, Germany, 4, 5 a.m. (S-1).

7.29—San Francisco, Philippine news, 6 a.m. (S-3).

11.78—Saigon, French Indo-China, 6:30 a.m. (S-5).

15.29—San Francisco, 3, 4 p.m. (S-1 and S-3).

7.30—New Delhi, 3:30 p.m. (S-3).

9.63—New Delhi, 3:30 p.m. (S-3).

9.63—London (General Forces Program), 7 a.m. (S-4).

9.25—Australia Armed Forces Radio, sports news, 3:15 a.m. (S-4 and S-5).

7.30—San Francisco, for Philippines, 3:15 a.m. (S-6).

9.60—San Francisco, for Philippines, 3:15 a.m. (S-5).

11.87—U.S.A., 3 a.m. (S-2).

Moscow in the 25-, 19-, and 31-meter bands heard with news at 8 a.m., 5 a.m., and 7:30 a.m.

(EDITORS NOTE: We expect before long to have details concerning the operations of VPD2, Suva, 6.135 mc., which is now heard best with an English newscast at 4 a.m. EWT, Sundays only.)

• • •

RADIO EIRE

Radio Eire was heard recently coming on at 4:58 p.m. Asked for reports and that they be sent to "Radio Eire," Chrysler Building, New York City. Reports addressed there will be forwarded by the Consulate General of Ireland to the Department of Posts and Telegraphs, Dublin, by which the Irish radio service is operated. Canadian listeners can write to "Radio Eire," Ottawa, Ontario, Canada (which

we presume is the address of the Consulate General of Ireland for the Dominion of Canada).

This station is reported regularly by Harris, Massachusetts, and others in the eastern United States. It is heard irregularly by your short-wave editor. The station seems to come on the air any time between 4:58 and 5:10 p.m., and signs off any time between 5:14 and 5:35 p.m. The news is generally given at the beginning of the broadcast, and is followed by sports news. The news is worldwide in nature. This appears to be the only short-wave transmission from Ireland at the present time, and it is believed this station is located in Athlone.

Leo T. McCauley, Consul General in New York, informs me that the transmissions are at present on an experimental basis. My inquiry to "Radio Eire" in New York has been forwarded to Dublin, and I hope to have details on the Irish short-wave service shortly.

• • •

REPORT FROM CANADA

The first report received from a reader in Canada comes from Albert E. Bromley, Toronto, Ontario, who reports as follows:

ZNR—12.100, Aden, Arabia, heard with a terrific signal of 15 decibels above S-9, at 1 p.m. to signoff at 1:16 p.m.; identification in English at 1:15 p.m. as ZNR, and wavelength in meters. Stated they were on every night. The program consisted of stringed-instrument orchestra and a man singing in the typical wailing voice of the East. Have received this station twice since then, but not quite as strong.

CR6RA—9.470, Angola, Portuguese Africa, very weak at 3:45 p.m. Signal faded away at 3:55 p.m.

TAP—9.465, Ankara, Turkey, heard at 3:20 to signoff at 3:56 (Sunday), 5 decibels above S-9. No English spoken; the program consisted of piano selections and then a woman announcer followed by two men announcers giving the news. Slight interference.

PCJ1—5.930, Netherlands West In-

(Continued on page 84)

AROUND THE CLOCK WITH THE WAR NEWSCASTS IN ENGLISH

EWI	LOCATION	CALL	FREQ.*	EWI	LOCATION	CALL	FREQ.*	EWI	LOCATION	CALL	FREQ.*
MORNING											
7:00 a.m.	London	GSB	9.51	1:00 p.m.	Tokyo	JVW3	11.725	10:30 p.m.	Melbourne	VLC4	15.315
		GWC	15.07	1:00 p.m.	London	JZK	15.16	10:45 p.m.	Leopoldville (Relays BBC)	RNB	9.783
		GWE	15.43			GRY	9.60				
		GSV	17.81	1:30 p.m.	Winnipeg	GVW	11.70	10:45 p.m.	London	GRH	9.825
		GSF	15.14			GSJ	15.26			GSL	6.11
		GRG	11.68	2:00 p.m.	Tokyo	CKRX	11.72			GSU	7.26
		GSH	21.47	2:00 p.m.	London	JVW3	11.725			GRC	2.88
		GRF	12.09			JZK	15.16	11:00 p.m.	Colon (Panama)	HPSK	6.005
		GSD	11.75	2:00 p.m.	London	GRY	9.60	11:00 p.m.	Berlin	DXJ	7.24
7:40 a.m.	Moscow		11.80	2:30 p.m.	Moscow	GVW	11.70	11:30 p.m.	Winnipeg	CKRO	6.15
			15.75			GSJ	15.26	11:40 p.m.	Tokyo	JZJ	11.80
			10.44	2:45 p.m.	Brazzaville	FZI	9.44			JLT3	15.225
			11.94	3:00 p.m.	Berlin		9.590			DXJ	7.24
8:00 a.m.	Shepparton (Australia)		9.615	3:30 p.m.	New Delhi	VUD5	7.30	12:00	Berlin	DXP	6.03
8:20 a.m.	Moscow		15.75	3:45 p.m.	Bern	HEO4	10.338	midnight		DXB	9.61
9:00 a.m.	Manila	PIRM	6.14	4:45 p.m.	London	GSJ	15.26	* * * *			
			9.64			GVW	11.70	AFTER MIDNIGHT			
9:00 a.m.	Tokyo	JVW3	11.725	4:45 p.m.	Brazzaville	GRY	9.60	12:30 a.m.	London	GSL	6.11
		JZI	9.535			GRJ	7.32			GSU	7.26
9:00 a.m.	London	GSP	15.31	5:45 p.m.	London	FZI	11.97			GRH	9.825
		GSV	17.81				9.44	12:30 a.m.	Leopoldville (Relays BBC)	GRC	2.88
		GWC	15.07			GRH	9.825			RNB	9.783
		GWE	15.43			GVZ	9.64	1:00 a.m.	Tokyo	JZJ	11.80
		GSF	15.14			GSU	7.26	1:00 a.m.	Berlin	JZK	15.16
9:00 a.m.	Hongkong	GSH	21.47	* * * *						DXJ	7.24
		JZHA	9.47	EVENING				1:15 a.m.	Shepparton	VLC4	15.315
9:30 a.m.	Berlin	DJB	15.20	6:00 p.m.	Quito	HCJB	9.958		Melbourne	VLC3	11.71
		DXR	11.763				12.445	1:30 a.m.	Hsinking	MTCY	15.33
10:00 a.m.	Saigon	R.S.	11.78	6:20 p.m.	Tokyo	JLT3	15.225	2:00 a.m.	Suva (Sun. only) (Fiji Islands) (Relays BBC)	VPD2	6.135
10:00 a.m.	Tokyo	JVW3	11.725	6:45 p.m.	London	JVU3	11.897				
		JZK	15.16			GVZ	9.64	2:00 a.m.	London	GSD	11.75
10:00 a.m.	Chungking	XGOY	9.646			GRH	9.825			GSB	9.51
			7.155			GSU	7.26			GWC	15.07
10:00 a.m.	Berlin	XGOA	9.73			GSL	6.11			OVU	11.78
		DJR	15.340				11.94			GSP	15.31
10:00 a.m.	Hsinking	MTCY	5.710	6:47 p.m.	Moscow		15.20			GRG	11.68
			6.125				15.10			GVZ	9.64
10:15 a.m.	Melbourne	VLG	9.58				15.20			GRM	7.12
10:45 a.m.	Sydney	VLI9	7.28	7:00 p.m.	Berlin	DJD	11.77			GWD	15.42
10:45 a.m.	Saigon	R.S.	11.78			DXJ	7.24			GRU	12.04
11:00 a.m.	Tokyo	JVW3	11.725			DXP	6.03			GRH	9.82
11:00 a.m.	Chungking	JZK	15.16	7:20 p.m.	Tokyo	JLT3	15.225			GSU	7.26
11:00 a.m.	Chungking	XGOY	9.646	7:25 p.m.	Brazzaville	JVW3	11.725				
			7.155			FZI	11.97				
11:00 a.m.	Ceylon (Relay of BBC)		4.90				9.44	2:00 a.m.	Brisbane	VLQ3	9.66
11:00 a.m.	Stockholm	SBT	15.155	7:30 p.m.	Winnipeg	CKRX	11.72	2:30 a.m.	Hsinking	MTCY	15.33
11:00 a.m.	Shepparton	VLC6	9.615	8:00 p.m.	Berlin	DJD	11.77	2:00 a.m.	Tokyo	JZJ	11.80
11:00 a.m.	Melbourne	VLG	9.58			DXP	6.03			JZK	15.16
11:00 a.m.	London	GRV	12.04	8:00 p.m.	Moscow		11.94	3:00 a.m.	Tokyo	JZJ	11.80
		GSP	15.31				9.48			JZK	15.16
		GWC	15.07	8:15 p.m.	Chungking	XGOY	11.905	3:00 a.m.	London	GSB	9.51
		GVU	11.78							GSD	11.75
		GRG	11.68	8:15 p.m.	Leopoldville	RNB	9.783			GRG	11.68
		GSV	17.81							GSW	7.23
		GSH	21.47	9:00 p.m.	Berlin	DXJ	7.24			GSP	15.31
		GRF	12.09			DXP	6.03			GRD	15.45
		GSD	11.75	9:00 p.m.	London	DJD	11.77	4:00 a.m.	London	GRM	7.12
		GWD	15.42			GSL	6.11			GVZ	9.64
11:00 a.m.	New Delhi	VUD2	6.19			GSU	7.26			GWD	15.42
11:45 a.m.	Berlin		9.590			GRC	2.88			GRV	12.04
						GRH	9.825			GRH	9.82
						RNB	9.783			GRN	11.82
* * * *				9:10 p.m.	Leopoldville			4:00 a.m.	Suva (Sun. only) (Fiji Islands)	VPD2	6.135
AFTERNOON				9:20 p.m.	Budapest	HAT4	9.125	5:00 a.m.	American Broad- caster Somewhere in Australia	VLC2	9.68
12:00 noon	London	GRP	17.87	9:30 p.m.	Bern		7.38		Melbourne	VLR	9.58
		GVW	11.70	(or 9:45)		HEI4	6.345		Perth	VLW3	11.83
		GSP	15.31	9:45 p.m.	New Delhi	VUD5	9.539	6:00 a.m.	Shonan (Singapore)		9.555
		GSJ	15.26	9:45 p.m.	Melbourne	VLC4	7.300	6:30 a.m.	Saigon	R.S.	11.78
12:00 noon	Chungking	XGOY	9.646					6:30 a.m.	Shonan (Singapore)		9.555
			7.155	10:00 p.m.	Berlin	DXJ	7.24				
12:00 noon	Moscow		15.75	10:15 p.m.	Djarkarta	DXP	6.03				
12:00 noon	Tokyo	JVW3	11.725	10:25 p.m.	Budapest	HAT4	18.135				
		JZK	15.16				9.125				

*To convert frequency to meters divide 300,000,000 by the frequency in cycles-per-second.

THEORY AND APPLICATION OF U.H.F.

By MILTON S. KIVER

Part. 9. Covering the principles and operation of commonly employed methods used to obtain energy from cavity resonators.

IN THE previous article on cavity resonators their development from either wave guides or transmission lines was shown, methods of excitation were explained, and the electric and magnetic field distribution investigated. In the present article more of the properties will be examined in order to complete the picture of cavity resonator action in ultra-high-frequency apparatus.

As pointed out in the last installment, electrons passing through the grid-like structure of a cavity resonator will induce electric and magnetic fields within the enclosure of the resonator and if the period of the exciting electrons bears a direct relation to the natural frequency of oscillation of the cavity resonator, then large standing waves will be obtained and correspondingly large amounts of power may be drawn from the enclosure. This power then may be used to excite an amplifier or it may be connected directly to the antenna for radiation.

Output from a cavity resonator that is being excited can be accomplished in three ways. And surprisingly

enough, each method has the same action whether at the ultra-high frequencies or merely on an ordinary low-frequency transmitter. The simplest and most obvious method is to just allow the energy in the cavity resonator (or coil and condenser) to radiate from the apparatus itself. This, of course, is generally undesirable, but nonetheless represents a transfer of energy from the tuned circuit (or resonant chamber) to some outside receiver.

A better method of obtaining energy from a cavity resonator is comparable to the capacitive method used on low-frequency circuits and illustrated in Fig. 1A. Here the wire from the condenser is placed at a point on the coil where the r.f. voltage is high in order that the most energy may be transferred. Moving the tap down toward the grounded end of the coil will decrease the amount of voltage taken off, and thus enable us to have any voltage, from a minimum of zero to a maximum that is determined by the voltage fed to the coil.

To apply this analogy to a cavity resonator, it is first necessary to find a point of high value in the electric field, this being analogous to a high r.f. voltage. From what has been mentioned in the article on wave guides and the last article, it is safe to assume that a high electric field would not be found near any of the conducting walls. To illustrate this, refer to the diagrams that have been reprinted here from a previous article. Fig. 2A shows the electric field distribution across the width of a cavity resonator, while Fig. 2B represents the same distribution for the length, in this case a half wavelength long. The output device may be placed at any point where the electric field intensity is other than zero.

The device itself that is used to receive the energy is drawn in Fig. 3. To make this type of probe, all that is needed is a coaxial transmission line with the inner conductor extending a little beyond the outer cylindrical conductor. The hole in the resonator through which this cable actually may pass is usually threaded so as to enable the outer conductor of the coaxial line to be screwed firmly into place and at the same time make electrical contact with the inner surface of the cavity resonator. The inner coaxial rod then extends well into the chamber itself and so comes into contact with the electric field. The electrons in this center rod then will be acted on

by the electric field and thus enable energy to be transferred from the resonator. The other end of the coaxial cable may be attached to the device that will receive this energy, as stated above. In an oscillator, if the cavity

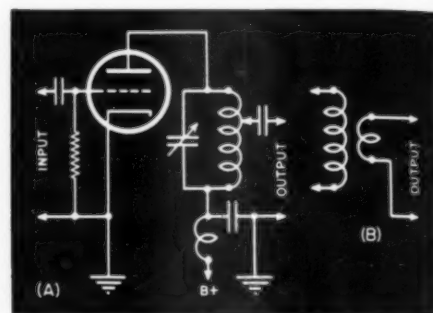


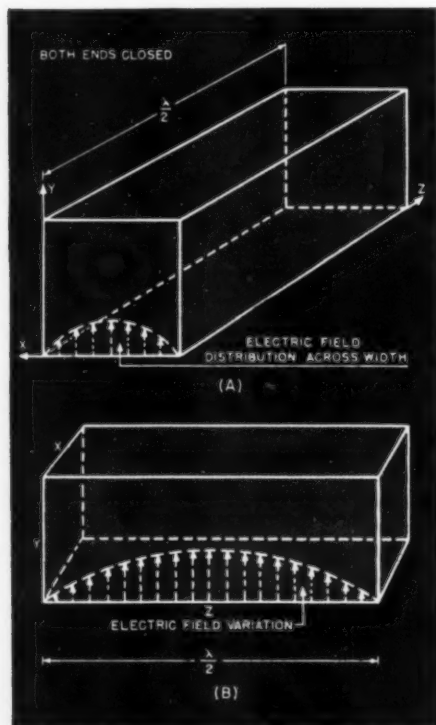
Fig. 1. Methods of obtaining low-frequency energy transfer: (A) capacitive coupling, and (B) inductive coupling.

resonator happens to be the catcher, this energy may be fed back to the buncher resonator and complete the oscillating action. In this case another coaxial line then will be attached to the catcher resonator for output energy.

In the low-frequency capacitive coupling, less energy was taken for the output circuit if the tap was moved down. To accomplish the same results here, all that is necessary is that the probe be moved to a region where the electric lines of force are less intense. This would mean bringing it closer to one of the walls and away from the center of the resonator. This is somewhat difficult to do as it requires that another hole be drilled in order that the coaxial line can be inserted. This detail is merely a mechanical one and whether the process of changing the amount of energy output is more or less difficult at the ultra-high frequencies, the comparison to the action at the lower frequencies is quite evident. In one case there is an actual voltage that is being dealt with; in another there is an electric field of force.

There remains one more method of coupling at the low frequencies and that is by inductive means. Placing a small coil close to an oscillator inductance will transfer energy, as shown in Fig. 1B, from the circuit on the left to the output circuit on the right. Moving the coil closer will result, up to a certain point, in more energy being available at the antenna. Increasing the distance between the coils naturally will produce the opposite effect.

Fig. 2. (A) Cavity resonator, showing the electric field distribution along the X axis. (B) the same resonator as in (A), showing how the electric field varies as the wave travels down the enclosure.



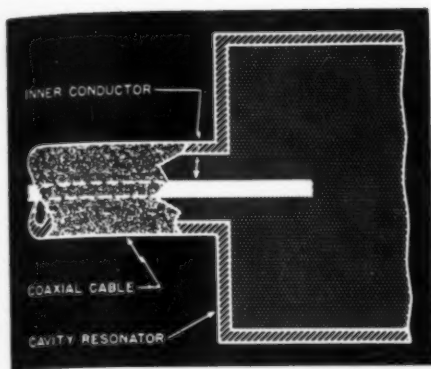


Fig. 3. An ultra-high-frequency method of capacitively coupling a cavity resonator.

This is the well-known action at the low frequencies. The high-frequency analogy means that magnetic lines of force will have to be considered. These form closed loops within the resonator and at the same time are everywhere at right angles to the electric lines of force. This has been mentioned in previous articles and is referred to here to bring these thoughts back to mind.

Now, in order for a changing magnetic field (such as might be obtained in a resonator) to induce a voltage in a metallic probe, best results usually will be had if this conductor is in the form of a loop. The more turns of wire in this loop, the greater the induced voltage. Experimentally this loop can be moved about in the cavity resonator until the point of maximum coupling takes place with the magnetic field. By moving the coil either back or forth about this position, less coupling may be obtained in a manner quite analogous to the low-frequency apparatus. A diagram of a magnetic probe that may be made from a coaxial cable is given in Fig. 5. Although it might be desirable to use several loops, these are not made to fit easily within the small volume of a cavity resonator. One loop, as pictured, usually will provide enough pickup for most purposes.

Both methods of coupling to cavity resonators may be used to remove energy. Which is actually chosen depends, as at the low frequencies, on the particular circuit in use. Actually, neither method exists by itself. With capacitive coupling, we get some inductive coupling and with the latter method, a great deal of capacitive coupling likewise exists. For best operation, loose coupling is desirable. By inserting this metallic probe deeply into the cavity resonator, it is possible to alter to some extent the configuration of the fields here and the end result will be a change, sometimes not too slight, in the resonant frequency of the resonator. To take this into consideration, the resonant frequency of the resonator is determined with the probe in position.

For the final comparison between cavity resonators and the more familiar tuning circuits, let us determine the components of the Q of these ultra-high-frequency tuners. It will

be recalled that one reason ordinary coils and condensers are not used here is due to the fact that the Q or selectivity (and efficiency) of these units decreased to small values. This has been explained in detail in previous articles. It might be interesting, however, to see just how the Q of a cavity resonator is deduced since nowhere in its construction can any inductance (as such) be found. Of course, from what has been given on transmission lines, it can be seen easily that what we actually have in a resonator is distributed resistance, capacitance, and inductance, which take the place of lumped constants.

Returning to the symbol Q itself, it was shown previously that this was equal to the ratio:

$$\frac{\text{Inductive Reactance}}{\text{Resistance (a.c.)}}$$

or stated in a simple mathematical formula:

$$Q = \frac{\omega L}{R}$$

The above resistance is not what would be read with an ohmmeter, since this reading would pertain only to d.c. resistance in the coil. It is the total resistance, both a.c. and d.c., and increases with frequency. The increase is brought on by a combination of the following causes:

1. Skin effect, which causes the current to concentrate near the surface of the conductor as the frequency rises.

2. Dielectric losses causing leakage since insulators at low frequencies may (and often do) become conductors at high frequencies.

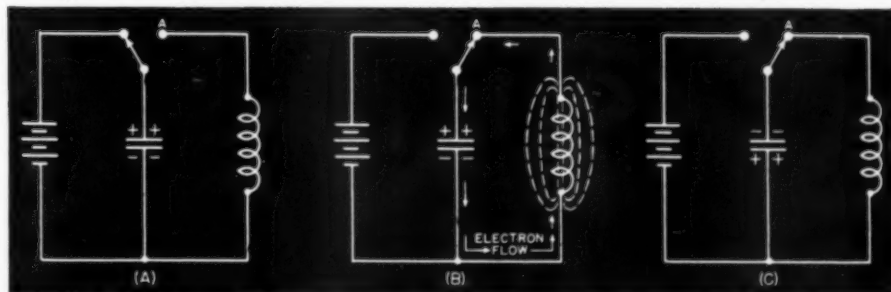
3. Distributed capacitance between turns.

4. Eddy currents in the conductors.

Now, it is possible to take the above definition of Q and to express it in slightly different terms, having the same meaning. This follows from the fact that the energy put into the coil is divided into two parts: that which is stored in the magnetic field due to the action of the coil, and that energy which is lost because of the inherent resistance of the wires that form the coil. It can be shown by mathematical reasoning that the following ratio:

$$\frac{\text{Energy stored per cycle}}{\text{Energy dissipated per cycle}}$$

Fig. 4. The sequence of energy transfer between magnetic and electric fields in a low-frequency circuit. (A) Condenser being charged from battery source. (B) Discharge of condenser through an inductance coil, setting up a magnetic field. (C) Showing condition after the magnetic field has collapsed and condenser polarity has been reversed.



also can be made equal to Q . From this it can be deduced that a coil that has a high Q is more efficient (has less loss) than one with a lower Q , a fact previously brought out. Here, however, it is a little more obvious. Again the matter of convenience prevents the use of the formula at the lower frequencies.

To apply the above formula to a cavity resonator, it is necessary to determine where the energy is stored and where it is lost. The first condition is simple, since any energy that is contained in a cavity resonator can be found in the electric and magnetic fields. The energy is contained first in one field and then it changes over gradually into the energy of the other field. This self-same situation is obtained at the lower frequencies also,

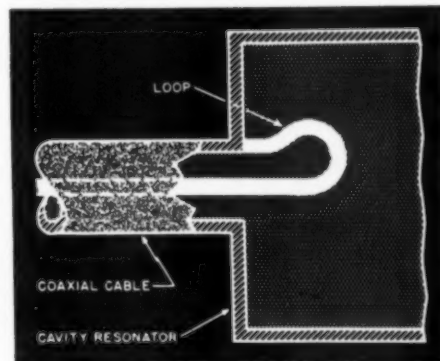


Fig. 5. Using a coaxial cable as a means of inductively coupling a cavity resonator at the ultra-high frequencies.

as can be shown quickly by the following simple example. In Fig. 4 is shown the circuit of a parallel coil and condenser combination. By means of a switch it is possible to introduce energy into the circuit from a battery. In this case the condenser is the recipient of this energy. If the switch is opened then, the condenser retains its charge and energy may be considered as residing in the electric field between the plates. By moving the switch over to position A, the electrons will flow from the condenser to the coil and a magnetic field will build up around this coil. In a short period of time the entire energy that was contained in the condenser will be found in the magnetic field about the coil. The first phase of our process thus has taken place.

As soon as the current stops flowing, (Continued on page 150)



By CARL COLEMAN

A NEW class of license was announced by the Federal Communications Commission to be known as the "Temporary Emergency Radiotelegraph Second Class Operator License." The new license should not be confused with the "Temporary Limited Radiotelegraph Second Class Operator License" which has been known as the "TLT." The new "TET" grade license was announced by FCC in order to relieve the present shortage of radiomen with radiotelegraph tickets and also because of the shortened training course offered at the Maritime Radio Training Schools which may not equip students to pass the higher examinations. The new license restricts the operator from transmitting except for "emergency communications directly related to the safety of life and property at sea."

This license shall be issued to any person who passes the FCC commercial radio operator International Morse Code test of 16 code groups per minute; in addition, obtains a rating

of fifty percent or better on elements 1 and 6 of the commercial radio operator examination; and is found otherwise qualified to hold a radio operator license. This license will be valid only for operation of a ship radiotelegraph station on board a vessel that carries at least one Limited Radiotelegraph Second Class radio operator holding a Temporary Operator License, or a radio telegraph license of higher grade, who maintains at least eight hours of the required watch per day, or one-third of the required watch per day on board such ships and supervises, subject to authority of the master, operation of the ship station.

This license will expire one year from date of issue unless previously terminated by the Commission, and unless otherwise provided for by the Commission, will not be renewed.

The measure, in other words, is a temporary expedient to provide radio operators for the emergency communications which might be necessary

under present conditions aboard U.S. cargo vessels. However, when the need is no longer acute, the Commission will most likely cancel this grade of license, so if you obtain one of these "TET" tickets get started on your way to obtain a "TLT" or regular 2nd class radiotelegraph license.

R. MURISON was in recently for a short vacation while his craft was being refitted. E. K. MacDowell has been "looking into things" up at a new television station operated by Dumont and seems to like that better than some of the other branches of radio. R. Krohem was in with his cargo vessel recently for a few days.

S ELECTIVE SERVICE in New York recently has announced that all former seamen up to 38 years of age who were granted deferments as seamen and then quit, face reclassification into 1-A and immediate induction, unless they return to active sea duty. Shortage of manpower in the merchant marine was responsible for the statement of Col. A. V. McDermott, local Selective Service director, who addressed local boards and appeals agencies.

"The situation has been developing progressively over the last three months and promises to grow even more serious as time goes on."

The chief offenders, he asserted, were men over 30 years of age who have left the sea because of the liberalization of the classification policies in their age group.

A NDREW C. JORGENSEN, recently elected vice president and general manager of Mackay Radio, joined MRT in 1924 as a radio operator. Murray Crosby who has been with RCA as a research engineer has joined Press Wireless. H. Harris has returned to the East Coast again.

After seventeen months of public hearings, the House committee investigating FCC suddenly voted late in November for secret sessions. The broadcast division has been interested in the outcome of the investigation into the sale of WMCA by Donald Flamm to Edward J. Noble. The station was sold four years ago at a price that was reported to be several hundred thousand dollars below its actual value and was claimed by some to have been sold under duress.

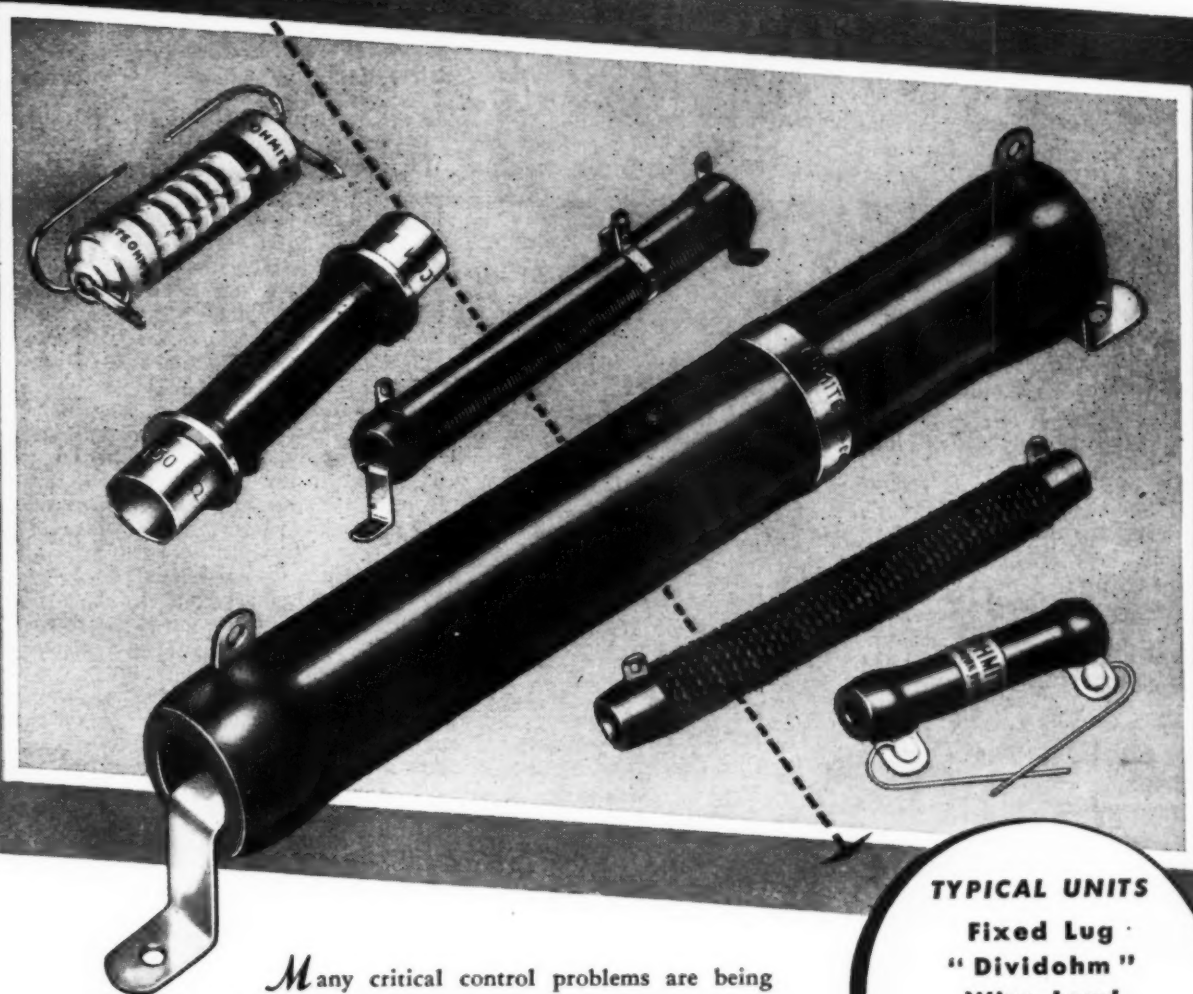
A IRWAYS flight radio officers will be interested in an announcement by Boeing of the actual completion of a new postwar transport craft. The new ship is designed to carry 72 day passengers or 36 in berths, is a two deck affair with a cruising speed of well over three hundred miles per hour and a range of well over three thousand miles. It is of the four engine type. Now if they only stop doubling up on the methods of taxes for some of the airline companies maybe they can afford to open up some nice

(Continued on page 136)



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TECHNICAL BOOK & BULLETIN REVIEW

"BEHIND THE MICROPHONE,"

by John J. Floherty. Published by J. B. Lippincott, Philadelphia. 207 pages. Price \$2.00.

In this book, Mr. Floherty has presented the story of radio as seen by the announcer, producer and actor. He has recalled, amusingly, the early days of radio broadcasting when the handling of emergencies was everyday fare for the station staff.

Equipment breakdowns, temperamental performers and inadequate studios added to the "pioneer" atmosphere of this new venture called radio.

The various services of radio, including news broadcasting, sustaining programs and sponsored time, are discussed simply and nontechnically with the hope that the public will appreciate the work, thought, time, and money that is represented by the fifteen minute "serial" or the two-hour symphony concert.

The structure of the network and its function in radio broadcasting is presented in order that the listener may gain some concept of the magnitude of the job behind the international broadcast, the coast-to-coast pickup or the program originating from some remote spot.

Since Mr. Floherty is not connected with the radio industry his approach is that of the layman to whom this complicated business of radio bears a close resemblance to a three-ring circus, a county fair, and an elaborate carnival all rolled into one. His enthusiasm for his subject and his admiration for the men who "keep it on the air" is manifest in this book.

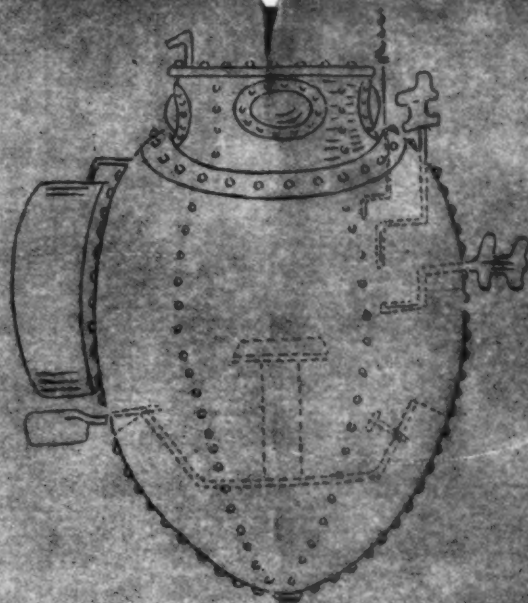
For those who like to have a "behind the scenes" view of a great industry, this book will prove to be a satisfying and pleasurable experience.

"PRODIGAL GENIUS, THE LIFE OF NIKOLA TESLA," by John H. O'Neill. Published by Ives Washburn, Inc., New York. 322 pages. Price \$3.75.

It is a sad commentary on our ability to judge genius when it is near us, that we fail to accord the honors due a man like Nikola Tesla during his lifetime and only after death do we extend the laurel wreaths and pen eulogies to his memory.

However, if the public is remiss in this matter, it is gratifying to have so sincere a tribute paid to a great man of science as is paid to Mr. Tesla in Mr. O'Neill's biography of him.

Nikola Tesla, to whom the world owes many of the advancements in power and radio engineering, was born of poor parents in a little town of Smiljan, on the Austro-Hungarian border. His father was the pastor of the village church and by the standards of the day, was an educated man. His mother was illiterate, but Tesla gives



Experience Counts

The unusual craft shown above was the first submarine of the American Navy. Built in 1776 by David Bushnell; it was used against the British warship, "The Eagle" which was lying off New York. Now, "The American Turtle"—that's what it was called—acted like a submarine all right, but that was about all. It didn't sink or damage any ships. Bushnell had a good idea but he simply did not have enough knowledge or experience to make his idea practical.

The moral of this story is: *In the development of the first submarine as in the development and*

manufacture of all products, Experience Counts.

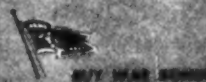
The design and manufacturing experience of THE WARD PRODUCTS CORPORATION has long ago established this company as the leader in the production of automobile and home antennas. Many important design changes pioneered by WARD, have made WARD the recognized pacesetter. All WARD products are quality products, the workmanship of craftsmen of experience, using modern equipment under ideal conditions. For the finest antennas for automobile and home applications, look to WARD!

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WM. J. MURDOCK CO.
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her credit for his inventive genius as it was her nimble brain and fingers which devised various means of labor saving in their modest home.

His formal engineering training covered a period of many years during which time he found it necessary to work to supplement the meager stipend his family was able to provide. The dynamic "will to do" which was evidenced in his early career never failed him throughout his life.

He is known as the father of the modern system of power transmission, the discoverer of the rotating magnetic field, and the principle of alternating current. During his lifetime he made a fabulous fortune, refused the Nobel Prize, yet died almost in poverty. Such was the man Nikola Tesla.

The treatment of the story is sympathetic, and in the hands of his close friend, John O'Neill, Tesla lives again in the hearts of his fellow countrymen.

-30-

FORMER RADIO AMATEURS COMMISSIONED S. C. OFFICERS

NINETEEN former radio amateurs received their commissions as second lieutenants together with other members of the 38th Class of Signal Corps Officer Candidate School at graduation exercises at Fort Monmouth, N. J. recently.

The new officers, and their call signs, follow:

K7IWH—Wendell J. Motter, St. George, Utah.

W3IEF—Richard E. Berger, Washington, D. C.

W5GDZ—Troy C. Wooddell, Houston, Tex.

W5HZ—Theodore D. Stallings, Dallas, Tex.

W6BCE—Joe Nightingale, Santa Maria, Cal.

W6PFY—Jay R. Borden, Los Angeles, Cal.

W6SKW—Richard B. Huntington, San Diego, Cal.

W7GQX—Raymond W. Williams, Astoria, Ore.

W7IFW—Kay G. Sears, Seattle, Washington.

W8EFW—Paul M. Cornell, Cleveland Heights, Ohio.

W8QWW—William R. Triplett, Bluffton, Ohio.

W8SRE—Richard A. Jamison, Cleveland Heights, Ohio.

W8TWQ—Frederick W. Walter, Lakewood, Ohio.

W8UBW—Thomas E. Tice, Huntington, W. Va.

W9GSO—Rudolph J. Rosetartitz, St. Louis, Mo.

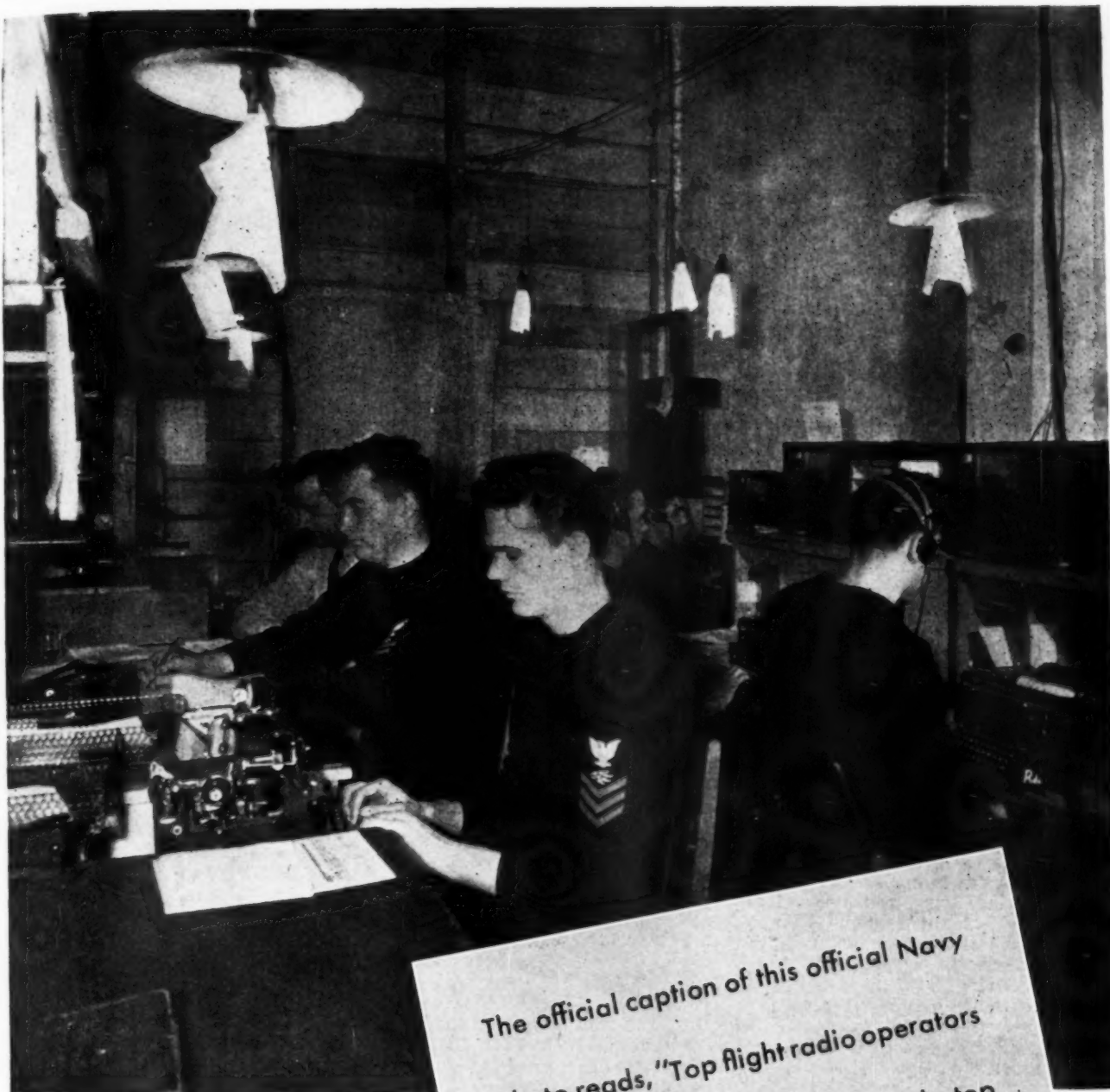
W9GZU—Ty Rensch, Ramona, South Dakota.

W9JGL—John L. Jones, St. Louis, Mo.

W9NTV—James C. Miller, Rockford, Ill.

W9QBC—James S. Joska, St. Louis, Mo.

-30-



The official caption of this official Navy
 Photo reads, "Top flight radio operators
 plus top flight equipment equals top
 flight performance at an African clear-
 ing base for the Italian Front."



NATIONAL COMPANY

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NATIONAL RECEIVERS ARE IN SERVICE THROUGHOUT THE WORLD

WHAT'S NEW IN RADIO

New products for military and civilian use.

NEW INTERCOM

In response to the Navy's request for a high speed intercommunicating system, *Executone, Inc.*, 415 Lexington Ave., N. Y., N. Y., has developed a new unit for use aboard the fleet.

The new system can have up to 11 stations and the number of individual



stations is unlimited. Any station may talk with any other station, at adjustable volume, and may communicate with as many other stations as desired. Several pairs of stations can talk simultaneously without other stations being able to overhear or cut in.

Automatic signal lamps show when other stations are busy, and also act as check-ups that the system is in working order. Volume is individually controlled. Each unit is equipped with built-in auxiliaries, such as reserve tubes and power, in case the 110 volt supply, on which the unit normally operates, is cut off. The unit is weatherproofed according to Navy specifications.

COROSEALED MIDGET RELAY

Corosealed relay, which is a midget type relay designed especially for communication, electronics, and aviation applications, has been announced by *Betts & Betts Corp.* These relays are



hermetically sealed in a metal shell, assuring perfect performance under severe conditions of temperature, humidity, pressure, dust, corrosion, and fungi. Units are normally sealed with

content of prefiltered dry air, but can be furnished with inert gas or pressurized content when desired.

This component incorporates a standard octal plug base to facilitate testing. Unit is $1\frac{1}{16}$ " long— $2\frac{3}{8}$ " including prongs.

Coil windings can be supplied for voltage ranges from 1.5- to 70-v. d.c. and are wound to exact number of turns. Every unit is subjected to a 1000-volt breakdown test. Inorganic base plastic insulation minimizes high-frequency loss and assures permanent dielectric and mechanical strength. Contact arrangements offer flexibility in arrangement and handle 2 amps. at 100 watts.

Further details of these relays may be had by writing to *Betts & Betts Corp.*, 551 W. 52 Street, New York 19, N. Y.

AIRCRAFT RHEOSTATS

Two new approved Power Rheostats for aircraft have been announced by the *Ohmite Manufacturing Co.* These new units are made in accordance with



the latest Army-Navy Aeronautical Specifications AN-R-14a (Drawing 3155). They have many well-known *Ohmite* Rheostat features plus new, improved control protection. They are rugged in design and construction to provide uniform electrical and mechanical control, and utmost dependability under all operating conditions.

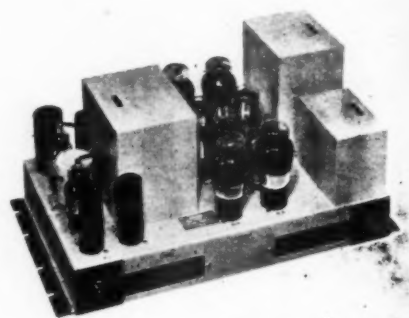
These new approved AN Aircraft Rheostats are light in weight—lighter than the allowable weight specified. They meet the salt-spray corrosion test, and other critical tests—and operate satisfactorily in the temperature range from -55° C. (-67° F.) to $+70^{\circ}$ C. ($+158^{\circ}$ F.).

There are two sizes: *Ohmite* Model "J" 50-watt, and Model "H" 25-watt. The Rheostats are Linear or Taper wirewound, in various resistances, with "off" position, as required. They are totally enclosed in a compact, corrosion-resisting metal container, complete with knob, as shown.

Further information may be obtained by writing to the *Ohmite Manufacturing Co.*, 4835 Flournoy St., Chicago 44, Illinois.

NEW AMPLIFIERS

A series of amplifiers known as the 101 Types has been offered by *The Langevin Company, Inc.*, 37 West 65th Street, New York, N. Y. These amplifiers are designed for commercial continuous service, and meet the need for medium gain, high-power bridging

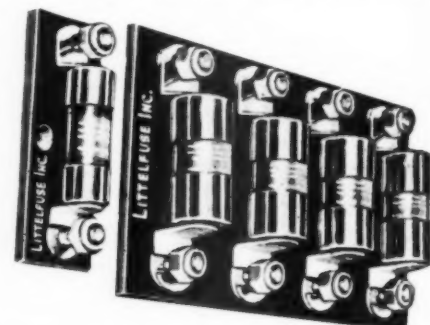


amplifiers. Where increased power is desired any number may be bridged across busses from 1 to 1000 ohms. Therefore, a complete amplification system of high quality and great flexibility is provided when used in conjunction with a program or line amplifier such as the Langevin 102 series.

All models in this 101 series will deliver 50 watts to a nominal load impedance with less than 3% r.m.s. harmonic distortion at 400 cycles. The gain control provides continuous adjustment over a 40-db. range and bridging connections. Chassis are 16-gauge welded steel, zinc plated, and bonderized. Finish is light gray baked enamel, and weight is approximately 45 pounds.

FUSE PANEL

With the increased demand for electrical fuse panels engineered to individual specifications, *Littelfuse, Inc.*,



has announced a new improved Universal Fuse Panel, No. 1505.

Blueprints of this unit are now available to engineers, draftsmen, prime contractors, and purchasing agents upon request to their plant.




The entire Detrola Radio plant is a new idea in radio manufacturing technique. All of its departments—administrative, engineering, design, production—are spacious, orderly and modern . . . and modernly equipped. This not only promotes employee efficiency, but stimulates workers to conceive ideas for ever-greater improvement of both our products and manufacturing methods. Such conditions have enabled us to achieve high quality, high volume war production. They will likewise enable us to build highest quality radio receivers, automatic record changers, record players, radio television receivers and other electronic devices when our efforts are again happily directed toward those peacetime pursuits.

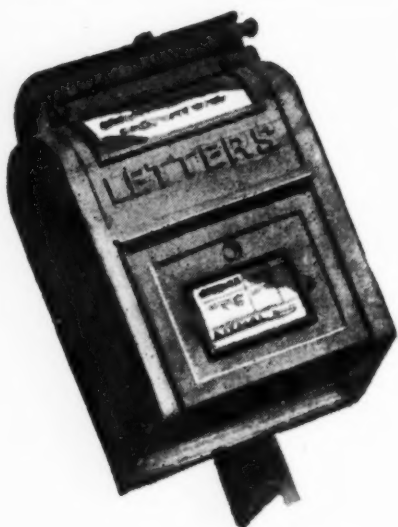
February, 1945

DETROLA RADIO

DIVISION OF INTERNATIONAL DETROLA CORPORATION • HEADQUARTERS AT CHATFIELD, DETROIT 4, MICH.

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Add CREI technical training to your present experience—then get that better radio job you want—make more money—enjoy security

CREI Practical home study training in Radio-Electronics Engineering equips you with the ability to go after—and get—a better-paying, secure radio job.

After the war will come the period of the "survival of the fittest." Employers can then once again be "choosy" in selecting the best-trained, best-equipped men for the best jobs.

In our proved course of home-study training, you learn not only *how* . . . but *why*! Easy-to-read-and-understand lessons are provided you well in advance, and each student has his personal instructor who corrects, criticizes and offers suggestions on each lesson examination. This is the successful CREI training that has trained more than 10,000 professional radiomen since 1927.

Your ability to solve tough problems on paper and then follow-up with the necessary mechanical operation, is a true indication that you have the *confidence born of knowledge* . . . confidence in your ability to get and hold an important job with a secure, promising post-war future. These jobs are waiting today for radiomen with up-to-date CREI technical training. *Investigate CREI home-study training* . . . and prepare now for security and happiness in the coming New World of Electronics! *Write for all the facts now.*



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ENGINEERING FOR PROFESSIONAL SELF-IMPROVEMENT

Dept. RN-2, 3224—16th Street, N. W., Washington 10, D. C.

Contractors to U. S. Navy—U. S. Coast Guard—Canadian Broadcasting Corp.
Producers of Well-trained Technical Radiomen for Industry.

Special advantages are to be found in aviation applications of this unit where the fuse panel can be placed at an accessible point rather than in a central junction box. Dispersal of these panels throughout the plane lessens the likelihood of complete outage due to gunfire.

The light durable panels, made to individual specifications, meet all Air Corps requirements and come ready to mount, equipped with terminals and fuse clips or terminal studs.

Panel users are invited to write to Littelfuse, Inc., 4757 Ravenswood Avenue, Chicago 40, Illinois, for copies of the blueprints.

HAND SEARCHLIGHT

A searchlight for use by maintenance groups and in industry is being offered by the U-C Lite Manufacturing Company.

This unit, the Big Beam No. 411, is completely portable and will project an intense beam of light more than 2500 feet, or provide diffused lighting by means of a snap-on lens.

The searchlight is powered by a heavy-duty, 6-volt storage battery which may be recharged from an a.c. charger, d.c. line or light plant. The lamp head can be turned in any di-



rection and stays adjusted. Other models are available powered by dry-cell batteries.

The U-C Lite Manufacturing Co., 11 E. Hubbard St., Chicago, 11, Ill., will forward details upon request.

SOLDERLESS TERMINALS

A completely new solderless terminal is being offered by the L. E. Brach Mfg. Corporation who manufactures this unit under license from the Buchanan Research Laboratories, Inc.

The Bee Terminal Block is a connector strip with various numbers of terminal posts, each terminal capable of handling from two to eight wires. The binding post stud has a slotted channel, the wires being held in this channel between a top clamp or shoe built into the nut, and a lower clamp or shoe which is secured to the base. This arrangement permits every wire



WHY WE LIKE TO "ROLL OUR OWN"

THE production of high-efficiency electrical and electronic equipment demands close control over the manufacture of most of the parts which go into it.

To be certain of accurate control over component parts, Connecticut Telephone and Electric Division manufactures an unusually high percentage of them in its own plant. For instance, we produce our own magnets, wind our own coils. Stampings and screw

machine products are turned out to our own standards, in our own shops.

These facilities for complete fabrication of the more essential elements of a piece of electrical or electronic equipment are as important to our customers as to us—they result in a better product at a "better" price . . . also assurance of our ability to keep delivery promises.

MAGNETS have a great deal to do with the efficiency of many types of electrical apparatus. Specially developed alloys treated in our own electric furnaces permit close control over the performance of C. T. & E. products.



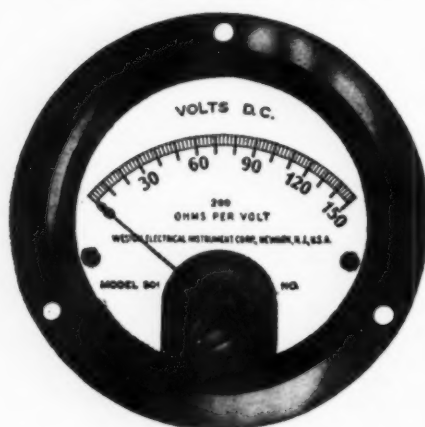
CONNECTICUT TELEPHONE & ELECTRIC DIVISION
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- American War Standard Meters in all different ranges — microammeters, milliammeters, ammeters, voltmeters, db. meters, portable instruments, etc.



Illustrated is the Weston Model 301, just one example of the wide variety of famous make meters available at HARVEY'S.

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- Precision carbon or wire wound resistors.

- 10 and 50-watt ceramic sockets.

... and hundreds of other critical radio and electronic components.

HARVEY is the complete radio and electronic supplier. Locating hard-to-find parts is but one of our many plus-services. We are prepared to answer your technical questions ... to advise you about priorities. Fast deliveries to any point in the United States.

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HARVEY also carries distinguished **AUDAK** equipment... cutters, jewel points, and pick-ups preferred by broadcasting stations and recording studios.



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to be locked to a wire, firmly in position, in a vibration proof and low resistance connection, without danger of loose strands. No lock nuts, lock washers, double nuts, lugs, or other accessories are necessary. This method obviates the necessity of soldering, crimping, pressing or insulating and requires no special tools.

This block is particularly recommended for aircraft, marine and communications applications. Samples and complete descriptive literature are available upon request to **L. S. Brach Mfg. Corp.**, Newark, 4, N. J.

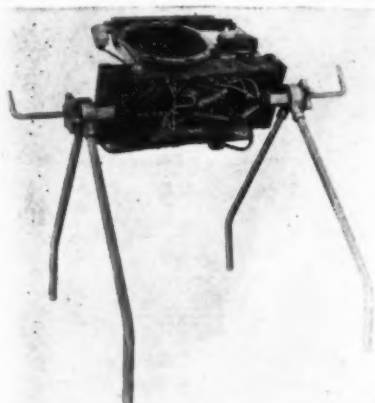
CHASSIS CRADLES

A device for speeding the handling of chassis on the assembly line is being introduced by the **Acro Tool and Die Works**.

This unit holds the assembly in an easy-to-get-at position for quick inspection and repair. This allows the workers to use both hands and permits them to position working areas to their convenience. The assemblies can be rotated and locked in position easily and rapidly.

The chassis cradle reduces the danger of damaging tubes, coils and other delicate parts due to dropping or bumping of the chassis.

The unit is made of cadmium plated steel and white metal, consisting of the supporting legs and locking clamps. The unit adjusts to any position by



means of finger-tip control and is equipped with an automatic lock.

The manufacturers are prepared to ship immediately on all orders. Write to the **Acro Tool and Die Works**, 4892 N. Clark Street, Chicago 40, Illinois, for full particulars.

INDUCTION GENERATORS

A new drag cup induction generator is being introduced in the **Elinco** line according to a recent announcement.

This unit is available in both base and frame-mounted models and is housed in die-cast aluminum alloy treated according to Army and Navy specifications.

The generators consist of laminator stator wound two-phase, stationary steel pole, and aluminum cup on the shaft rotating between the stator and the pole. When the voltage is applied to one of the two stator phase terminals, rotation of the shaft and cup in-

duces a voltage at the other terminal producing a voltage which is lineal with the speed. The torque required for rotation is approximately 25 grains at 1" radius. For increased voltage,



where linearity is not required, a copper cup may be substituted for the aluminum.

This unit is available in several models to fit manufacturing requirements. Requests for additional information and engineering data will be handled promptly when addressed to **Electric Indicator Company**, Stamford, Conn.

FENCE CONTROLLER TUBES

Two new fence controller tubes are now being manufactured by **Taylor Tubes, Inc.**

The Taylor 208 is a glow discharge tube and the other, Taylor 207, is a rectifier. Both tubes have glass envelopes and a standard 4-pin base.

The electrical characteristics of the 208 include discharge at 875 to 950 volts d.c. at 8 milliamperes. The 207 has a filament voltage of 2.5 volts, a.c., filament current 2.5 amperes, with a maximum r.m.s. a.c. voltage of 1250, maximum d.c. current 125 ma.

Taylor Tubes, Inc., 2312 Wabansia Avenue, Chicago, Illinois, will supply additional information upon request.

COMBINATION TOOL

A new hand tool which combines all the steps involved in preparing a wire for a solderless terminal and in crimping the terminal to the wire has been announced by **Aircraft-Marine Products, Inc.**

In addition to the usual crimping notches, the 6-purpose tool includes an efficient wire cutter and an insulation stripper with the correct stripping length clearly indicated. Terminal stud hole sizes are also marked on the tool for quick checking.

Three types of terminals, for wire sizes 22 to 1C, can be crimped by this tool. The crimping notches are marked to correspond with terminals to be crimped and the stripping notches are marked with Navy Shipboard and Commercial AWG wire sizes.

The entire unit is compact and easily operated. Fully insulated handles are of molded plastic with the construction of heat-treated steel with a rust-resistant finish.

Further information is available from the **Aircraft-Marine Products, Inc.**, 1591 North Fourth Street, Harrisburg, Pa. Ask for Catalog No. 49111.

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KEEP UP WITH RADIO TELEVISION and ALLIED ELECTRONICS

Get in on the new developments in the fast expanding Radio Industry. Take your place in the field of Television. Make more money as a Modern Service Expert. Own and operate Your Own Business. Learn the latest Trade Secrets and Short Cuts through

SHOP METHOD HOME TRAINING

Don't waste time! Radio, F.M., Video (television), and the whole field of Electronics is changing fast. New methods, new techniques, new equipment. Today you must solve NEW problems in servicing and repairing F.M. receivers. Tomorrow there will be thousands upon thousands of Television Receivers to handle. Right after the war science promises NEW Electronic devices for household, factory and business.

ALL THIS MEANS NEW OPPORTUNITY FOR YOU IF YOU ARE READY

The thing to do is to GET READY right now. Find out about the marvelous new method of preparation—SHOP METHOD HOME TRAINING. Fill out and send in the coupon now.

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Here is the truly modern system of training. It matches the RAPID PROGRESS CONSTANTLY BEING MADE in Radio, Television and Electronics. It is up to date in every way because it comes right from the busy radio training shops of National Schools where experiments and developments are being carried on—where discoveries are being made all the time.

It is based on real shop methods—on the handling of real shop jobs. Only National can offer you SHOP METHOD HOME TRAINING because only National has the big busy shops to develop this method. And it is time tested too. National Schools has been training men for industry, for government,

for business for more than a third of a century. In essence you get at home—in your free time—the very same kind of instruction that has helped thousands upon thousands of ambitious men to more pay and greater opportunity—that has set thousands of men up in business with little or no capital. You owe it to yourself to read the book "Your Future in Radionics"—sent to you FREE if you fill out and mail the coupon.

Now, right now, is the time to grasp the opportunity of today—a successful career for tomorrow. Radio, television and the whole field of electronics invites you. The industry is crying for trained men everywhere. A rapidly expanding industry—probably the greatest in history—holds out the promise of a rich future—prosperous security.

All This Modern Electronic Equipment and More Comes to You as Part of Your National Course



NATIONAL TRAINED MEN NOW MAKING THE BEST MONEY IN HISTORY

The real value of National training shows up in the quick progress our men make on the job. Joe Grumich of Lake Hiawatha, N. J., turned down a job most men would welcome. He writes: "My latest offer was \$5,800.00 as radio photo engineer, but I am doing well where I am now engaged. I am deeply indebted to National."

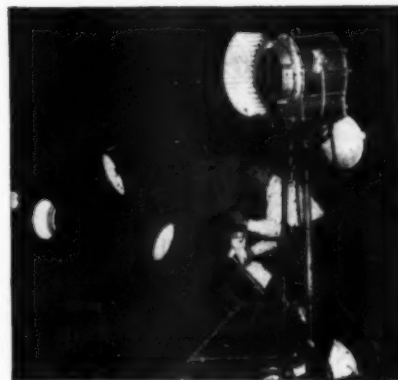
Ely Bergman, now on Station WOR, told us: "My salary has been boosted considerably and at the present time I am making over \$3,000.00 per year, thanks to National Training." And from the far-off Hawaiian Islands, Wallace Choi sends this: "I am averaging \$125.00 a month. I will say that I honestly owe all this to the excellent training I had at National."

National is proud of the progress graduates are making all over the world. Read about their records yourself in the books we send you FREE.

Get This FREE LESSON



Get a FREE lesson from National. Study it over at your convenience. See for yourself how thorough, how sound and how practical—yet how amazingly easy it is to learn and understand. NO SALESMAN WILL CALL ON YOU FROM NATIONAL SCHOOLS. National points out the opportunity—offers you the training and experience, prepares you for greater things in life. But it is up to you to act for yourself. And the first step is to fill out the Coupon and mail it. Get FREE lesson, the big Radio Book, and then decide.



GET THE REAL EXPERIENCE BEFORE YOU TACKLE A JOB

Walk into a brand new job and go to work with assurance—the assurance that comes with knowing how—that comes with handling the tools—with working with and operating actual electronic equipment sent to you from the laboratories and shops of National Schools. There's nothing to equal learning by doing. In your National training you build real sets—a superheterodyne receiver, a signal generator—literally scores of various electronic devices with your National equipment.

Learn basic principles—FIRST THINGS FIRST. Get your knowledge and experience first hand under the personal guidance of seasoned, practical National instructors working personally with you. You know the very how and why of Radio—Television, Electronics.

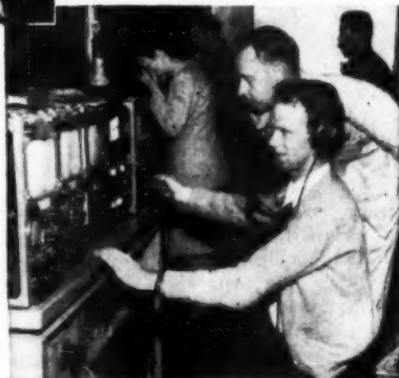
Not only do you gain marvelous actual experience by this method of learning but you have valuable equipment you will use on the job in the practice of your profession as an electronics expert. Mail the coupon and learn what this means to you.

AFTER THE WAR WHAT?

Face realities now! Is the job you're doing going to last? What is its future and yours? How are you going to meet conditions when the world returns to civilian production? There's no use in fooling yourself. Radio is a BIG, SOUND, WELL ESTABLISHED BUSINESS.

There are millions of sets in the Country that need reconditioning right now. There is a big demand for millions more that have to be built—largely by trained men. F.M. is here to stay. BUT RADIO IS ONLY ONE FIELD OF ELECTRONICS. Television is sure to come. Sets must be built, installed, serviced and repaired. Who's going to do it? Make up your mind that you are—and at a great big profit—for years and years to come.

What about facsimile? And the great new field of industrial electronics? It is established—here to stay. IT NEEDS MEN—RIGHT NOW AND MORE MEN NEXT YEAR. NEXT MONTH. TOMORROW! When your job folds up, will you step out proudly into a new field—an essential established industry?—perhaps into a business of your own?



The above pictures were made in and around a modern television studio. Think what new opportunity is open to you in this great new field if you are ready for it. Prepare now. National training includes a good foundation in Television and F.M. Get the facts. Send the Coupon.

NATIONAL SCHOOLS

LOS ANGELES 37, CALIFORNIA EST. 1905

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Mail me FREE the two books mentioned in your ad including a sample lesson of your course. I understand no salesman will call on me.

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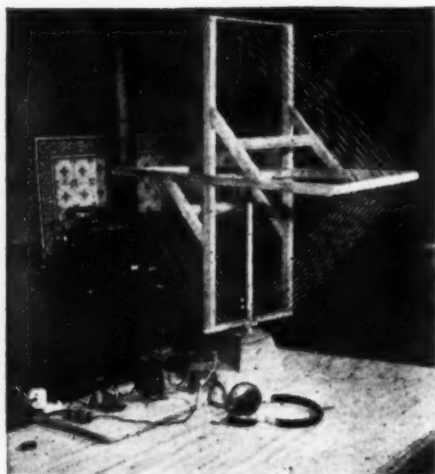
CITY..... STATE.....

Include your home number

FRENCH UNDERGROUND NETWORK during German occupation

By **KENNETH R. PORTER**

RADIO NEWS War Correspondent



Crystal detector used by the French to obtain outside news during German occupation.

PRIOR to the Allied invasion of France, members of the Maquis (French Forces of the Interior) hiding in the rugged mountainous regions of Savoy, the Ardennes forest, or the barren heaths and marshes of the Landes, maintained almost uninterrupted communications with each other and the outside world by the aid of radio equipment either improvised on the spot or parachuted from Allied planes.

This radio equipment consisted mainly of short-wave transmitters which could be picked up over a radius of hundreds of miles on any ordinary broadcast receiver having provision for the reception of the higher frequencies.

In the spring of 1943, however, the German authorities in France clamped down on clandestine listening by con-

fiscating all radio sets they could lay their hands on.

The Maquis, in turn, extended the range of their transmissions to the lower frequencies and as the radiation strength of their transmitters was necessarily limited on medium and long waves to a few miles in radius, they gradually evolved an ingenious network of secret relay stations, linking virtually all centers of underground resistance in the country.

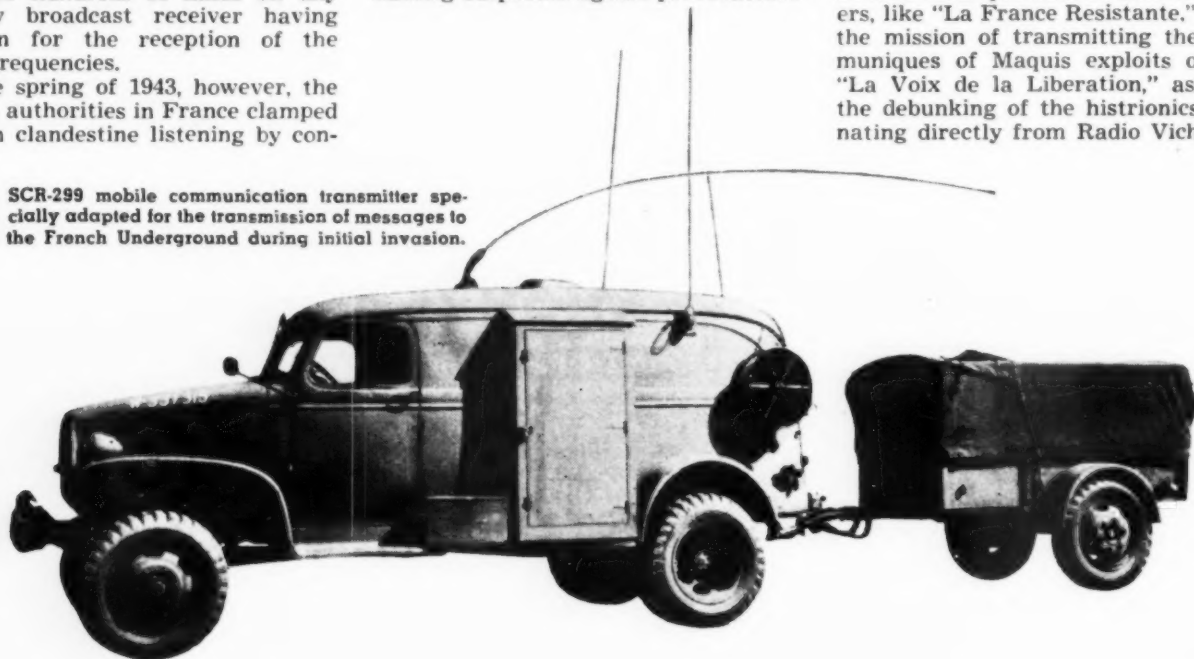
All these stations worked closely together and by transmitting messages containing warnings, instructions, or naming suspected agents-provocateurs

and collaborators from one end of the country to the other, played a most vital part in the struggle of the French underground movement against the German overlords.

The system of underground radio communications assumed such proportions, in fact, that a special control council had to be set up by the Maquis leaders for the allocation of call signs, frequencies, and assignments to these stations in order to avoid confusion.

Thus, some of the clandestine stations were detailed to maintain close liaison with Gen. de Gaulle's Fighting French Headquarters in London. Others, like "La France Resistante," given the mission of transmitting the communiques of Maquis exploits or like "La Voix de la Liberation," assigned the debunking of the histrionics emanating directly from Radio Vichy.

SCR-299 mobile communication transmitter specially adapted for the transmission of messages to the French Underground during initial invasion.



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This underground radio traffic went on continuously and almost openly despite frantic efforts on the part of Gestapo agents, provocateurs and quirlings to track down the stations and their operators.

The civilian population of France, deprived in most parts of the country of their broadcast receivers by order of General Stuepnagel, the German C.-in-C., nevertheless contrived to keep themselves informed about what was happening inside and outside their country by listening to Maquis transmissions (and BBC transmissions) on valveless little detectors of the "Cat's Whisker" type.

In fact, a spokesman of the FFI categorically stated after liberation that these crude, homemade almost without exception, sets which in peacetime used to be the pastime of children, had been the main source of news and information of millions of Frenchmen. They had fostered and sustained effectively the morale of the people of France in the darkest hours of her humiliation under the iron-fisted rule of the German conquerors.

The crystal detector shown in the photograph perched on a mat-covered wooden table was encountered by the author in the kitchen of a stone cottage somewhere on the outskirts of a hamlet not far from Paris. It illustrates strikingly the skill and ingenuity with which simple, freedom-loving Frenchmen risking imprisonment and worse, outwitted the Germans, and is typical of the many to be found nowadays in the humble dwellings of the poor as well as in the magnificent chateaux of the wealthy.

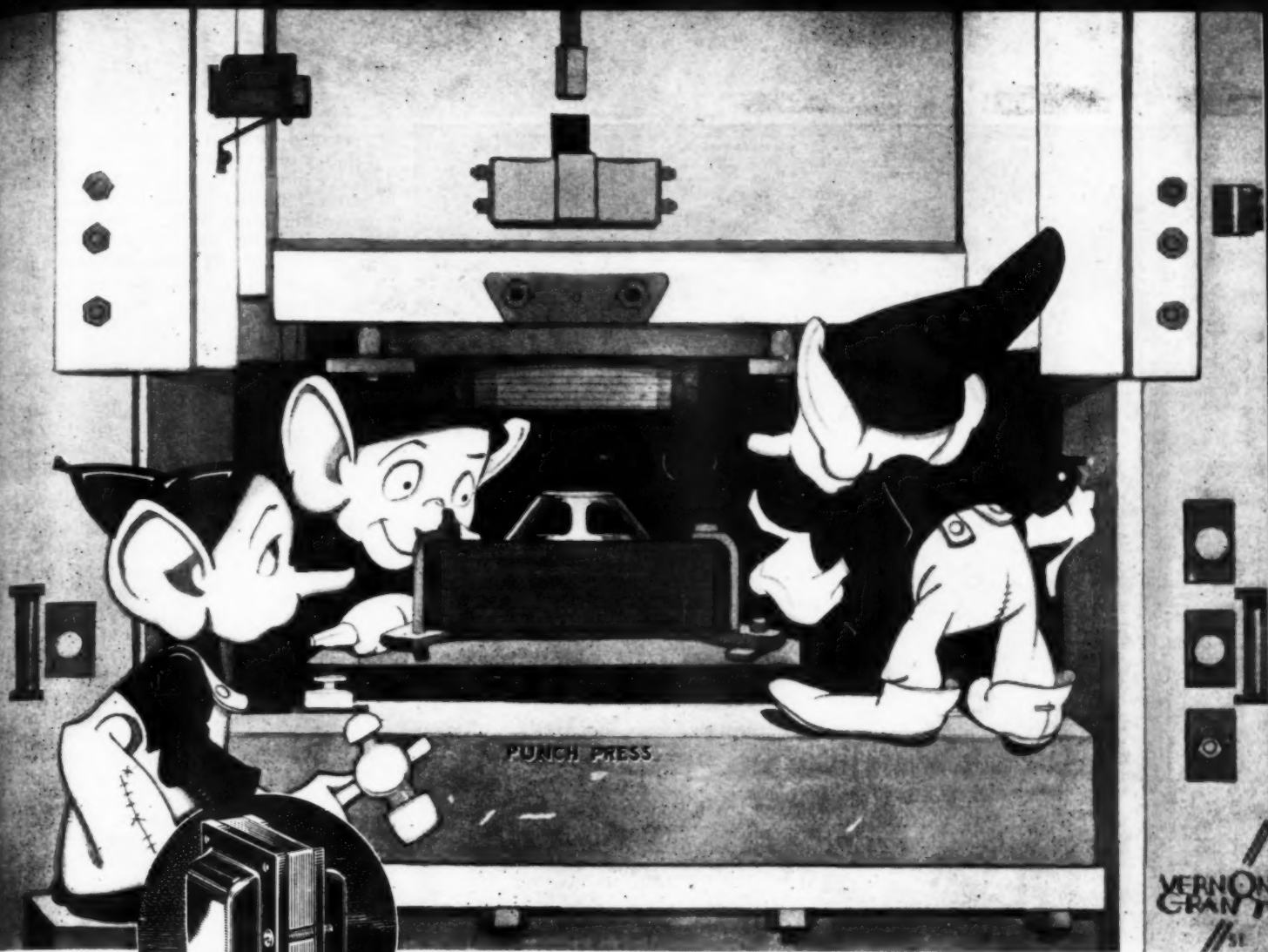
This particular unit had been built by an unassuming little Frenchman, an active member of the FFI, whom it will be best to call Monsieur Francois (because his two sons are prisoners of war in Germany), after his multitube receiver had been carted off by the S.A. to a central depot for storage early in 1943.

Monsieur Francois said that he had not mourned its loss for long but set to work as soon as possible on the construction of a crystal detector with the aid of the specifications which in those days used to be broadcast at regular intervals by the famous Col. Britten and his associates of the French section of the BBC in London.

With a volubility with which it was most difficult to keep track, Monsieur Francois then proceeded to describe how he had managed to procure a pair of high-resistance headphones smuggled out of the German supply stores by a French worker of his acquaintance and find a variable condenser by overpaying its market value many times, coupled with the employment of sundry ruses and palavers.

Insulated copper wire for the tuning coil, Francois obtained by dismantling the bobbin of a disused electric bell and a postal tube on which to wind the wire from a cardboard shoe box.

By various dubious means he even



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managed to secure a readymade crystal but only to discover that in spite of its blood red color and the trademark "Zincite" stamped upon the mounting proclaiming this crystal to belong to the zinc-oxide variety, it failed to give satisfactory reception.

Undaunted by this misfortune, the Frenchman continued his search and tipped off by another of his (numerous) friends, contrived somehow to get hold of a small fragment of coal showing yellow specks as evidence of containing crystals of copper pyrites. He mounted this into an empty cartridge case (later to be substituted by an ordinary piece of brass tubing of small diameter when this method of mounting proved rather cumbersome). A gramophone needle wound with the copper wire in spirals was used as the "cat's whisker" for making contact with the nutmeg of coal.

As no outdoor aerial customary for this type of receiver could be employed without courting disaster, Monsieur Francois stretched some lengths of copper wire inside the loft of his cottage from end to end with all the wires connected together at one end and joined to the aerial terminal of the set; a piece of wire bound tightly round the main water pipe (scraped clean with a knife) being used as a ground, completed the arrangement.

But Monsieur Francois' troubles were by no means over!

The sensitivity of the set was far from satisfactory and its selectivity deficient.

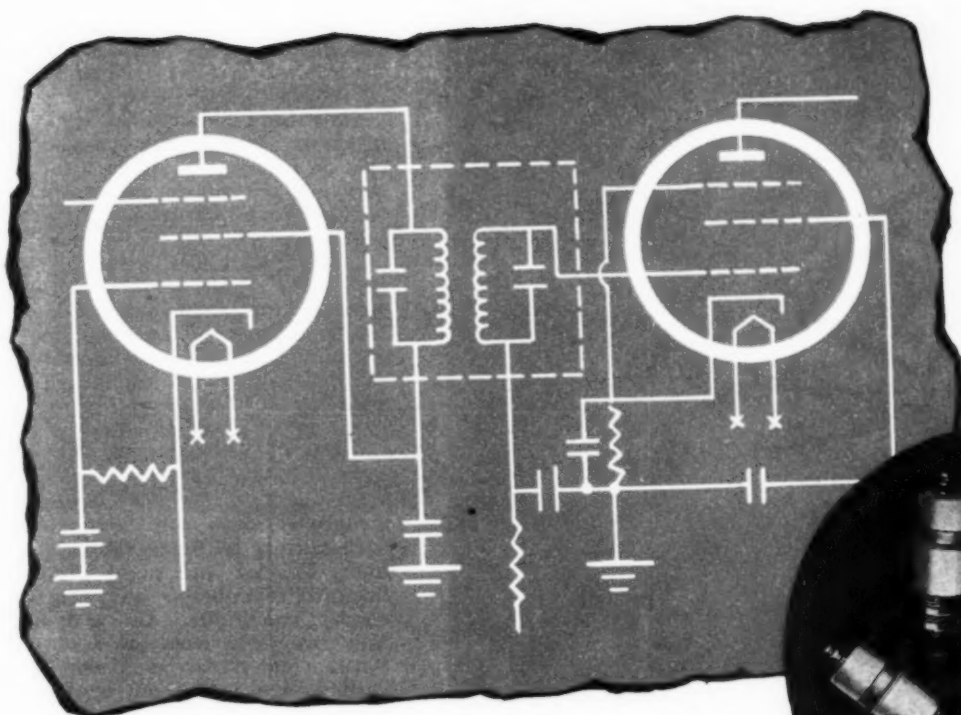
French ingenuity, however, improved station reception by the aid of an extemporized revolving loop aerial (depicted on the photographs). This eliminated adjacent and second channel interference as well as German jamming by the simple expedient of using a wave trap.

When in the end all difficulties had been overcome and the detector had passed, through the enterprise and perseverance of its owner-maker, all the vicissitudes to which these instruments appear to have been subject in occupied France could be put into operation, and the reception of Maquis and BBC transmissions on medium and long waves was excellent.

After Monsieur Francois had concluded his description of how he had built his receiver, he told me with a humorous twinkle in his eyes that actually he had gained by the exchange of the multitube model for the present one as his dependency on the electricity supply had ceased forthwith and with it the annoying practice of being cut off in the middle of important transmissions.

"Moreover," he added, "the crystal detector could be set up and dismantled in a matter of seconds without leaving a trace and it used to be great fun watching baffled German patrols searching all over the place for it in vain."

A new chapter was added to the history of French underground radio traffic at the time of the invasion when



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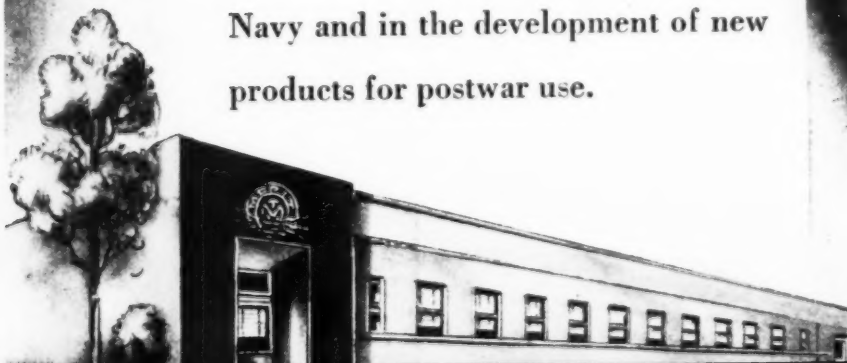
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Allied officers of the Psychological Warfare Branch following in the wake of the amphibious landing troops established direct radio contact with the Maquis groups operating in the invaded areas.

Six mobile communication transmitters were landed and put into operation on D-day plus six facilitating the carrying out of an important phase of the general tactical invasion scheme.

These transmitters were Hallicrafter SCR-299's which had been adapted specially for the purpose of transmitting signals on the standard broadcasting band (550-1600 kc.) in addition to their regularly assigned higher frequencies by U.S. Signal Corps engineers under the command of Major-General W. S. Rumbough, Chief Signal Officer, ETOUSA.

Members of the FFI received instructions sent out through these transmitters within a radius of many miles by day and night despite the limitations imposed on radiation by combat conditions. Acting upon these they promptly went over to the offensive and began such work specifically assigned to them by the Allied command operations as the blowing up of railway bridges, marshalling yards and ammunition dumps in the German rear, the derailment of trainloads of enemy soldiers and supplies bound for the invasion beaches and the cutting off from base of their isolated garrisons.

In addition, SCR-299 transmitters also were employed for a variety of miscellaneous purposes and used as impromptu broadcasting stations on frequencies occupied by regular French stations put out of action by the retreating Germans (as in Cherbourg), for relaying BBC and ABSIE (American Broadcasting Station in Europe) programs in combat areas. They were used as well for the dissemination of news and announcements over p.a. systems on the so-called "Milk Routes."

One SCR-299 transmitter has been credited even with persuading a German garrison at an unidentified submarine base to surrender unconditionally!

-50-

OVERCOMING PRECIPITATION STATIC

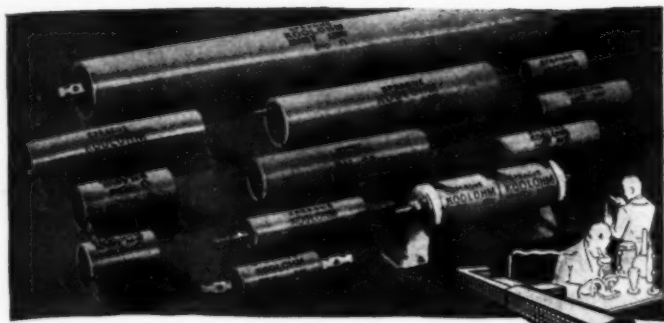
SIGNAL experts have discovered a way to overcome precipitation static, it has been disclosed by the Air Service Command in Britain.

Baffled for many months by radio noises resulting from the build-up of static electricity in the aerials and skin of aircraft, Air Service Command technicians solved the problem by the simple addition of a resistor across the antenna circuit of the receiver, which drained excess static electric charges before they could discharge and cause interference in the radio sets. This method has been adopted throughout the Air Forces.

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TEST EQPT. NEEDED—Prefer Hickok HF4 Oscillograph; PSQ-15 Microvoltage gen.; T53 or 51X tube tester; Model 4008 zero current voltmeter or #5348 tube tester and zero current set analyzer; also 4758 appliance tester. Any good late model eqpt. bought. Sumner Radio & Motor Service, 6709 N. E. Sumner St., Portland 16, Oregon.

FOR SALE OR TRADE—Carter 6v-400v, 250 MA Generator; Pioneer 6v-300v MA Generator; DuPont 164 Oscilloscope; 4 Jensen PM12C speakers in parabolic baffles. **WANT:** Audio oscillator, Supreme 582-A Signal Generator. Henry's Radio, 410 Thames St., Newport, R. I.

WANTED FOR CASH—Discharged veteran needs signal generator; V.O.M.; tube tester; Rider's chanalyst; voltchymyst, etc. Also 1.4v, 6v, 12v, 35v, 50v, 117v series tubes, any quantity. Ben A. Guzzardo, R.O.S. Radio Service, Stratton-Stricker Bldg., Waco, Texas.

FOR SALE—RCA AC-DC modulated phonograph oscillator with RCA 12A7 tube; Hoyt 300 DC voltmeter range, 0-30-300-v; Readrite 55 AC voltmeter range, 0-10-140-v; Readrite #55 milliammeter range 0-15-150 MA; 3 filament transformers, 6.3-v; power transformer; 2 1/2-v filament, 5-v filament, 250-v high voltage secondary; Filter Choke, 200 ohms resistance; Stancor 15 henry filter choke, 40 MA; Stancor henry filter choke, 150 MA; RCA multirange wave trap; Astatic 5-M scratch filter, bi-polar 6 position tap switch; two 2-circuit, 5-tap switches; Super Akra 100,000 ohm wire-wound resistors, also 300,000 ohm; Philmore Dyna-mike, O. F. Sterneman, Box 3260, Honolulu, T. H.

WANTED—F-M tuner for high-frequency police bands, 30-40 MC of 116-120 m.c. Al Birch, Box 13, Parkland, Wash.

FOR SALE—Supreme 570 signal generator, de luxe series; 125 K.C. to 60 M.C. Has 400 cycle audio output; frequency input jacks; external modulation jack. Factory reconditioned, accurately calibrated. Martin Radio Service, 142 Ralph Avenue, Brooklyn 33, N. Y.

FOR SALE OR TRADE—For test equipment, such as signal generator; or what have you, 6-tube superheterodyne without cabinet, 10-inch Rola speaker? Henry C. M. Bursun, 1-984 E. 70th St., Cleveland, Ohio.

DISPOSAL SALE—Short wave receiver parts; 00014 Var. condensers; resistance coils; Thordarson, Maxin and Karas power audio, straight or push-pull trans. Cannonball head phones; 6" & 9" loud speakers; sockets; panel mount meters and many other parts, brand new, in original wrappers, at one-half cost. P. E. Chapman, 5029 Osage Ave., Philadelphia 43, Pa.

FOR SALE—Small lot of tubes in sealed cartons OPA List. (Whole group only.) 1R5, 1LN5, 1LH5, 12J5, 12SK7, 25L6, 80, Success Radio Service, 122 Motor Ave., Salt Lake City, Utah.

WANTED—Test and service equipment of all kinds—at once—with instructions on how to use. William J. Croft, R. D. No. 5, Bedford, Va.

WANTED—Hallcrafters Sky Champion model S-20-R. C. E. Riley, 32 Davis Ave., Cranston 10, R. I.

WANTED FOR CASH—3-inch Dumont or Supreme "scope. Also good SX28 receiver. Woodrow F. Wroton, Hotel Yankee, Grand Island, Neb.

FOR SALE—Factory reconditioned Astatic mike T3 with floor stand, \$25; Astatic mike D2, \$15; power shifter from 6v battery to 1.4v, 300 m.a., B90V 10 m.a., \$12.50; and new radio tubes at 40% off list, including 6V6GT, 6Z7G, 6BK7GT, 6L6G, 1J5G, 6BJ7GT, 54, 46, 12J5GT, 12A5, etc. Doerr Radio Service, 1165 Breedlove, Memphis, Tenn.

WANTED—Superior set tester analyzer. Hillinski Radio Service, 51 Leopere St., Buffalo 12, N. Y.

FOR SALE—Tubes, at O.P.A. list price. Willie K. Patterson, 636 Chipley Ave., Greenwood, S. C.

WANTED—Readrite meters of all types. Dave Mate, 1122 College Ave., Alameda, Calif.

WANTED—Test equipment for radio servicing—also tubes. What have you? Phillips, 1410 N.W. 26th St., Oklahoma City, Okla.

FOR SALE—RCA 150 oscillator and 151 scope; Instructograph, Jr.; Rider's 3, 4, 5, 6, 7, 8 and 9; Radio News June '36 to date; QST, January '39 to December '41; Centralab standard controls; Centralab switches; heavy duty mike stand; and wood lathe. Howard Abernathy, Batavia, Iowa.

FOR SALE OR TRADE—Two 955's and 2-185's both with sockets. Want 1" scope, 6G8GT tubes; also issues QST and Electronics magazines. Art Kirschoff, 209 Brackenridge St., Ft. Wayne, Indiana.

FOR SALE OR TRADE—Melsner 12-tube, 5-band (long and shortwave), \$95, urgently need Jensen bass reflex speaker enclosure (12") No. CA-12 or BR-121; good signal tracer with V.T.V.M.; Hallcrafters SQ22H or S-29; Echophone EC-1, 2, 3, or 4; oscillograph. Mike Blackwell, 360 West California Ave., Memphis 3, Tenn.

FOR SALE—Scarce tubes such as 12SA7, 12SK7, 35L6, 35Z5, 6F6, 1N5, 1H5, new and used. Want Webber oscillator, 8 mm. movie projector and camera, N. C. 44, 45 or similar receiver, and vibrator unit. J. M. Fraser, Box 95, Binscarth, Man., Canada.

URGENTLY NEEDED—Tube tester, preferably American, Precision or Radio City. Will accept combinations. Dorsey H. Corbin, P. O. Box 173, Braddock Heights, Md.

FOR SALE—Universal Weston Master Exposure Meter and leather case, A-1 shape. \$23 cash or trade for equal amount in the following tubes: 1A7GT, 117L2, 117P7, 50L6, 35L6, 12SA7 and 12K7GT. Radio Engineering Service, 2659 Valentine Ave., Bronx 58, N. Y. C.

FOR SALE—Power transformers for Radiola and G.E., audios for Radiola and Acme, fil. X-former, speakers with outputs, variable condensers, etc. Frederic H. Crownfield, Jr., 29 Reed St., Abington, Mass.

WANTED—AC voltmeter, tubes and sig. generator. T. Pruitt, 2512 Gray Manor Terrace, Dundalk 22, Md.

FOR SALE—Test instruments, supplies and tubes, including 6BA7, 6BK7, 80, 12SK7, 12SQ7, etc. John Trowbridge, Dept. 8F., 7936 Farnell, Chicago 20, Ill.

FOR SALE—5 output transformers and 135 new radio tubes, including 1LN4, 6J5, 6X5, 6AR, 6SA7, 6SK7, 78, 25L6, 80, 1R5, 1R4, 174, 384, 6L6, 3Q5, 35Z5, 7A7, 7B7, etc. United Radio Service, Box 194, Centreville, Miss.

URGENTLY NEEDED—Phono-recorder complete with radio tuner—must be A-1. Frank Andrich, Jr., 403 E. 16th, Vancouver, Wash.

FOR SALE—Used radio supplies. Write for list. J. C. Thimijan, 715 N. 7th St., Lake City, Minn.

FOR SALE—One each of the following tubes (in lot only): 1A4, 1C5, 1E7G, 1LH4, 1N6G, 3Q5, 5V4, 6A6, 6ASB, 6B4G, 6C5, 6K7M, 6N7, 6R7M, 6BA7, 6SK7, 6V6, etc. Goodwin Radio Shop, Hanks, Ill.

WANTED—Analyzer and condenser tester. Will pay cash, or cash and following: Delco 3/4 h.p. motor; 1C5, 1H5G, 6BA7, 71A, 80 (2), 27 (2) tubes; 5" p.m. dynamic speaker; radio texts. C. A. Wilans, Morris, Ill.

URGENTLY NEEDED—A-1 pocket type multimeter or small test meters—Readrite 3-meter tester or equivalent. Fred C. Oldenburg, 1242 Roslyn Road, Grosse Pointe Woods 30, Mich.

FOR SALE OR TRADE—2-468 kc Xstals with holders, 2-P. E. cells and many other parts. What have you and what do you want? Urgently need instruction sheets or data (will buy or rent) concerning Superior V.T.V.M. #1260. Anthony Pusateri, 1101 Fleming St., Cosopolis, Pa.

WANTED—Filament transformer and instructions for Preceptor tube tester K. Will buy for cash or trade tubes, power trans., phono amp., etc. Stanley J. Zuchera, 2748 Meade St., Detroit 12, Mich.

FOR SALE—6-12SF5, 5-12J5GT, 7-6U5 tubes (all new), and 1 Elmac 250h (used). L. B. Cox, Box 447, Shelley, Idaho.

WANTED—35A5 tube and good voltchym-meter. Can also use all types 50, 35 and 12 v. tubes. Hank's Radio Service, Box 13, Easton, Minn.

FOR SALE—Philco #27-38 6 tube battery receiver, one short wave band; Philco #16 11-tube all wave receiver; and several BH and 01A tubes. Harold W. Hower, 835 Susquehanna Ave., Sunbury, Pa.

WILL EXCHANGE—Simplex tube tester, 3 battery sets (good for parts), old table speaker and Flewelling tube checker for what have you? Norton Saik, 78 Homer St., Providence 5, R. I.

WANTED—Professional dual speed Presto recorder. Roger B. Warren, 213 N. Aurora St., Ithaca, N. Y.

WILL TRADE—Simpson 0-5 mil milliammeter, 2 3/4" dia., and a quantity of 6L6G, 6N7, 6SU7 and 6C5 tubes; also other tubes suitable for P.A. work. Want an all-wave sig. generator. Joseph Swartz, 231 Vaughan Rd., Apt. C-11, Toronto, Ont., Canada.

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Obviously, Sprague cannot assume any responsibility, or guarantee goods, services, etc., which might be exchanged through the above advertisements.

Flight Recorder

(Continued from page 27)

diameter of about $\frac{1}{4}$ ". Three iron washers are used for the side walls of the coils, and an iron sleeve, slotted for the passage of the wires, is slipped over the assembly. Thus each coil has a complete iron path for its field, except for the section through the core. Into the core is fitted an aluminum plunger, on which there is a small iron ring. The ring serves to increase and decrease the inductance of the two coils, providing a bridge balance in conformity with its position. Ranges of operation are adjusted by means of resistances which shunt the coils—much the same as in the case of the potentiometer. The coils generally have an inductance approximately four millihenries each. The plunger can be operated by various types of moving mechanisms located in the plane during a test flight, such as airspeed and altitude diaphragms or Bourdon tubes.

The instruments are scanned in rotation by a sequence switch, Western Electric Type RA 120K, which switches two points to 80 positions in single controllable steps, or in continuous rotation at a variable rate of about one revolution (80 instruments) per second. As each instrument is connected through the switch, it is compared with two permanent "legs" of the bridge, which are precision set to within .01%. The bridges are energized by a stabilized 1000-cycle oscillator, which delivers three volts

across a 20-ohm bridge; then the "off-balance" signal from the instrument is amplified, rectified, filtered, and used to control the frequency of an 884-type relaxation oscillator. This oscillator is set to deliver 1000 cycles at "zero balance" (i.e., with no voltage from the rectifier), and 3000 cycles at maximum "off balance" of the instrument; it is continuously variable between the two limits.

From the oscillator, the signal is fed to a "limiter" type amplifier tube, which holds all frequencies to the same output level and modulates the transmitter to full modulation. Because they are direct generators, tachometers are fed into the system in a different way; each generates a signal whose frequency is adjusted by means of the number of poles on the armature, and this signal is fed into an amplifier tube which replaces the above-mentioned limiter amplifier by means of relay switches; thereafter, the signal modulates the transmitter in lieu of the converter signal.

How is synchronization produced and maintained? One point of the sequence switch is used to insert an identification signal of 400 cycles, the signal being generated by a second 884-type relaxation oscillator. At whatever point it is to be inserted into the sequence, the switch shorts the converter signal to ground, and introduces the 400-cycle signal into the transmitter through the tachometer amplifier. (The transmitter employed is a frequency-modulated Link Type 35-UFM, operating at about 33 megacycles and delivering approximately 35 watts to the antenna.)

Perhaps the most important part of the flight recorder ground equipment is a Link receiver, matched by crystal control to the transmitter frequency and delivering two watts of audio power through a 500-ohm line to the recording equipment. This input may be divided into the following three ways:

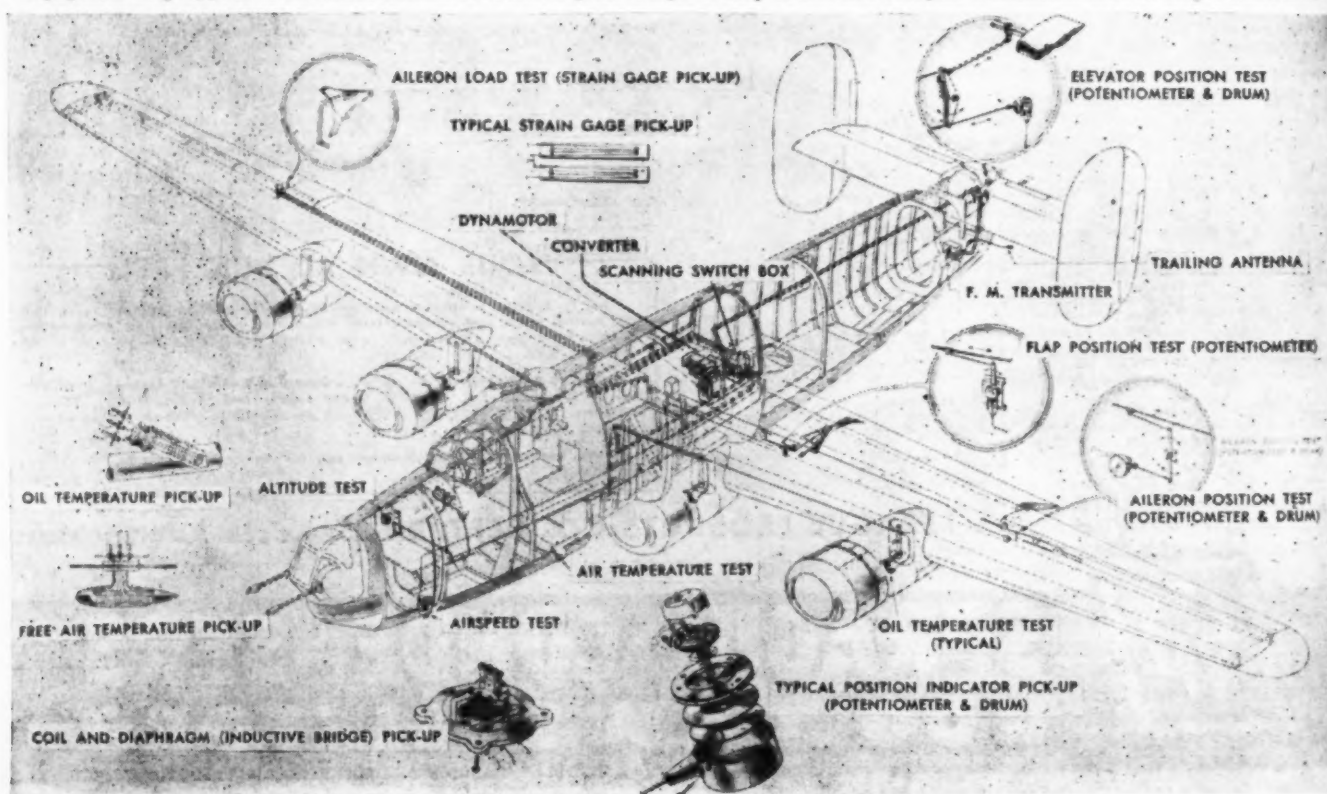
1. First, to a pair of 884-type relaxation oscillators, operating as a limiter. Limiter output is fed to a discriminator-rectifier which changes the signal frequency to a direct-current electromotive force which is proportional to the input frequency. This direct current is impressed upon a condenser and later matched against a varying direct-current voltage by means of a comparison method.

2. Second section of the input is amplified and fed through a 400-cycle filter into a switch, which contacts each of 80 neon lights in succession. The lights are used in banks of 10, which are switched manually from 0 to 80. Thus, when the manual switch is on No. 20, the lights indicate 20-29, inclusive. When the 400-cycle impulse is fed into the plane's transmitter, the consequent signal will light the neon bulb contacted by the ground switch at that time. The 400-cycle filter automatically eliminates all other frequencies.

3. We can best understand the third division of the signal by examining the nature of the signal fed into the transmitter which is located in the plane.

As it rotates, the sequence switch swings each instrument into place in succession; and each instrument

This drawing details the aircraft portion of the new flight recorder as it might be installed in a Liberator B-24J Bomber. Although this equipment may appear to be rather extensive, it has a gross weight of only 55 lbs. and occupies a maximum area of only 4 cubic feet.



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produces a signal of a characteristic frequency in the converter output. During the change from each instrument to the succeeding one, a special contact in the sequence switch shorts the modulation line, cutting the modulation to zero. This shorted time is approximately one-fifth of the time between switch contacts; hence, if the switch is scanning at the rate of 80 instruments per second, the duration of the signal from each instrument is 15 milliseconds and the duration of the zero modulation is 4 milliseconds. (It has been found that the system operates most efficiently at about 60 contacts per second.)

When the signal reaches the ground, the third stage into which it is fed consists of a rectifier and filter. The rectifier converts all of the signal-section to half-wave pulsing direct current, and the filter is tuned to 60 cycles so that out of it comes a 60-cycle voltage which has been formed by the alternations of signal and zero-signal. The 60 cycles are amplified through push-pull parallel 807's to about 100 watts in a 500-ohm line, and fed to a 1/20 horsepower synchronous motor. This motor is used as a brake on a universal motor (110 v.a.c.) which drives the main switch and comparator potentiometer. The main motor is controlled by a variable voltage transformer to a speed slightly greater than that of the aircraft switch, and the synchronous motor brakes the system down to the exact speed desired.

We have found this system to be highly accurate and capable of maintaining synchronism through radio noise which was loud enough to disrupt intelligibility. The instrument switching rate of 60 cycles is purely nominal, because it has been found that the system will maintain itself at 40 to 90 instrument readings per second.

In the input of the recording circuit

is a condenser to which the direct-current voltage from the first input path is switched. This potential is in direct ratio to the original instrument position, and is used as the bias on the control grid of a type 2051 thyratron tube. The positive end of the condenser is connected to one of 80 wiping arms on a potentiometer.

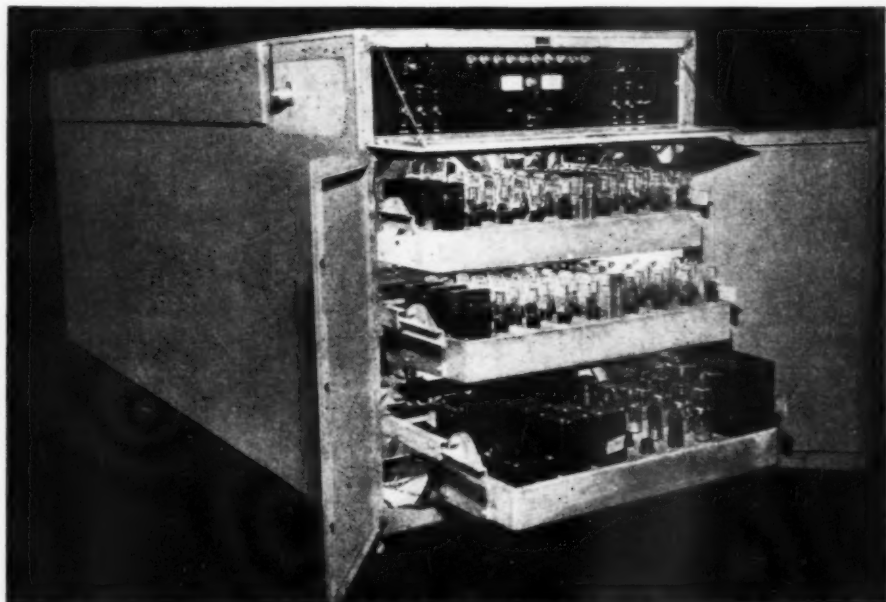
At the instant the potential is impressed, the wiping arm is at the ground end of the potentiometer; and at the time after the switch has moved on to successive condensers, the arm starts riding up the potentiometer, the opposite end of which is maintained at a positive potential slightly greater than the greatest anticipated signal of direct-current voltage (in this case about 40 volts).

When the arm reaches a positive potential of a dimension to neutralize the bias maintained on the tube by the condenser charge, the tube becomes conductive and causes another condenser to discharge through a special paper, where a mark is left. The paper is a brand called Teledeltos Type "L," manufactured by Western Union Telegraph Company. It has three elements so laminated that, when current passes through the paper, the top layer is destroyed, leaving a black underlayer showing through and indicating a spot.

Two parallel rollers are included in the mechanism for measuring the above-mentioned signal potential. Each carries a 30-inch strip of recording paper. Each 30-inch strip of paper is divided into five 6-inch sections, and each section is close to and facing a 5 1/4" trolley, which represents the actual height of each chart and which carries the discharge-marking current.

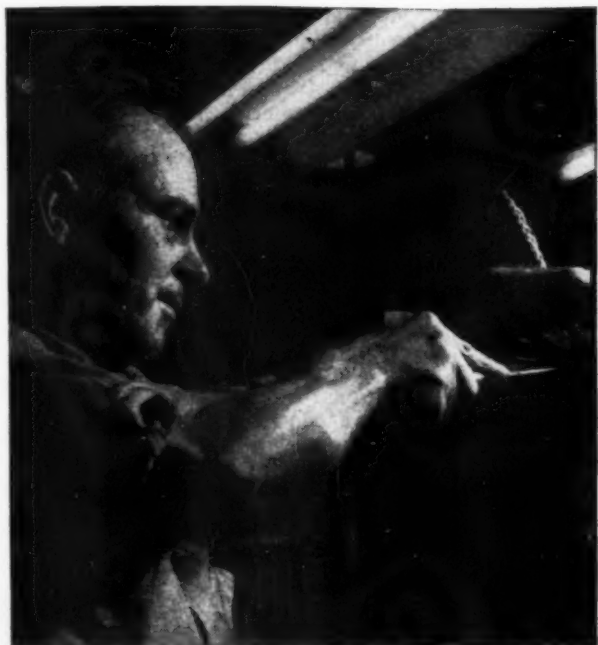
A thin steel belt is located between the paper and the trolley. This belt supports the "pens," small flexible elements which make electrical contact between the trolleys and the recording paper. The belt moves around the

The front portion of the ground-based receiver unit of the flight recorder. It is a Link receiver, matched by crystal control to the transmitter frequency.



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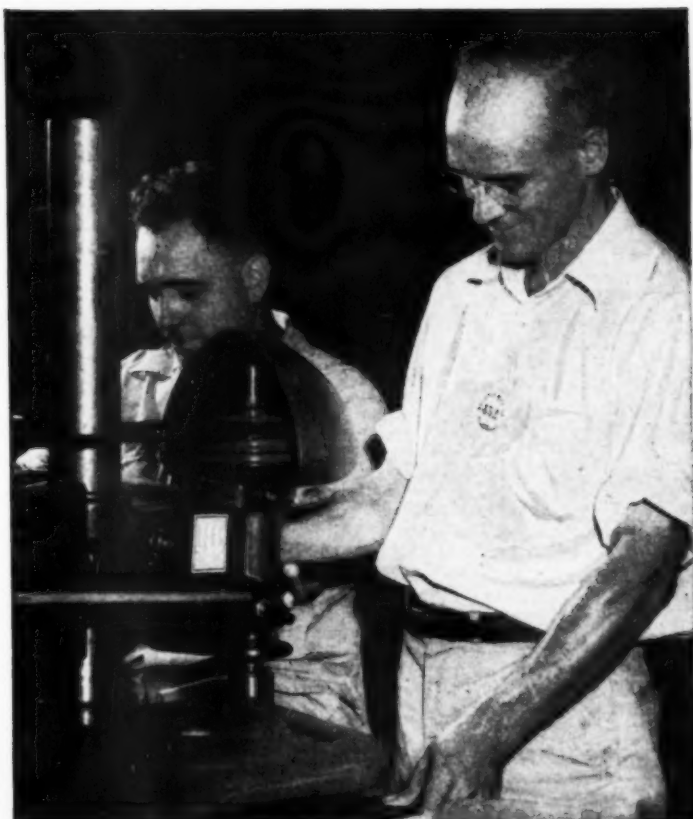
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SKILLS LIKE THESE?



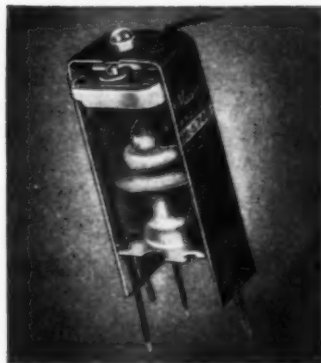
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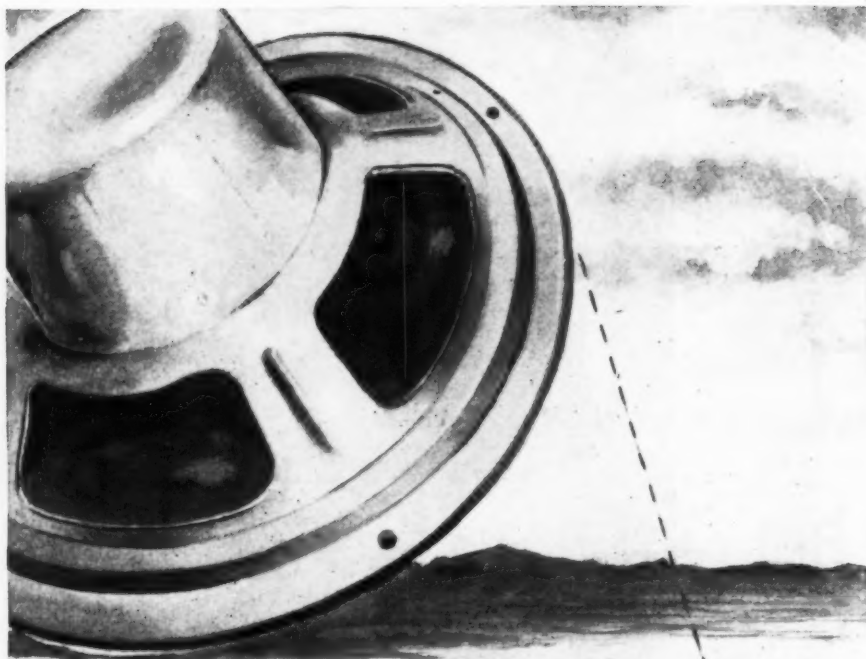
Designed primarily as original parts in high-gain receivers, these Meissner Ferrocort I. F. Input and Output Transformers get top results in stepping up performance of today's well-worn receivers. Their special powdered iron core permits higher "Q" with resultant increase in selectivity and gain. All units double-tuned, with ceramic base, mica dielectric trimmers, thoroughly impregnated Litz wire, and shield with black crackle finish. Frequency range, 360-600. List price, \$2.20 each.



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pulleys at either end of the unit, carrying the pens across each chart position in succession; and the pens are spaced and so positioned that, as the pot wiper arm starts its climb, a pen starts moving across the corresponding chart.

When the wiper arm reaches the high end of the pot, the pen will have reached the high end of the chart. Then, while the pot wiper is moving across the dead (ground) space of the pot, the condenser in the grid circuit of the 2051 receives its charge and the next pen in sequence moves into position to start its travel across the chart. Accordingly, when the charge on the condenser is neutralized by the pot voltage, the 2051 will "fire," causing the condenser in the plate circuit to discharge. This discharge is carried through the circuit comprising the condenser, trolley, pen, paper, and tube; and a mark is left on the paper at that point. Therefore, the distance of the spot from the low end of the chart is directly proportional to the original charge on the condenser of the 2051. As it is set up and now operating, this system gives an accuracy between the condenser charge and the spot location of plus or minus less than .0025 per cent. The paper is "rolled" transversely to the direction of the pen motion at the rate of about 1/32" per second; and, when signals are being transmitted at the rate of 80 per second, the spots appear about 1/32" apart, forming an almost continuous line as the plot for each instrument.

Together, these give us the composite picture of the airplane, instantaneously and accurately. Once we relied upon motion pictures and "magic eye" cameras to record instrument indications. If an experimental airplane crashed, odds favored the records being mutilated. Now, thanks to electronic recording, we can know what took place up to the instant of crash, and perhaps find from those records how to avoid a repetition. In any event, electronic recording marks great progress in flight-testing of aircraft.

-30-

International Short-Wave

(Continued from page 56)

dies, heard at 8:45 p.m., S-5 and S-6.

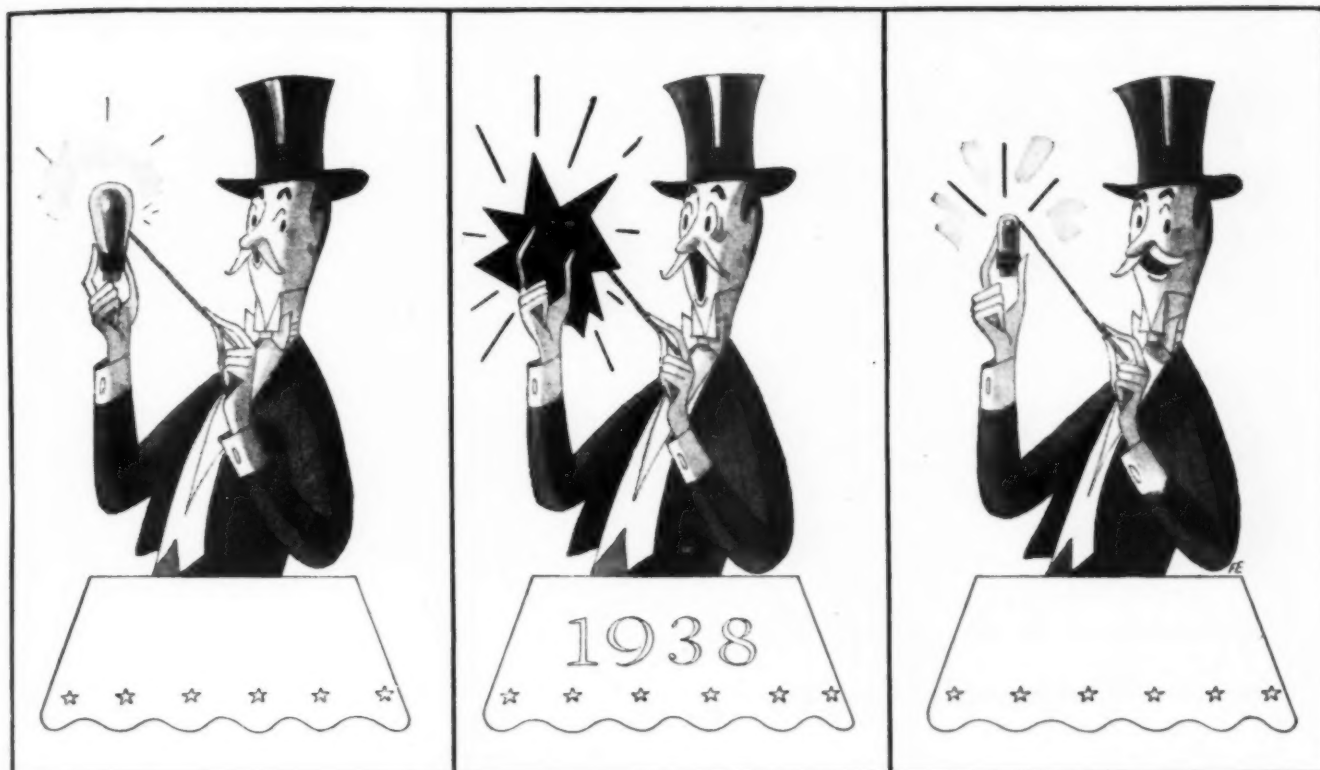
"Voice of Free Arabs"—10.005, heard weakly at 2:40 p.m., Sundays.

Radio Eire—9.595, Athlone, Ireland, heard with good signal of S-7 to S-9, at 5:15 p.m. to signoff at 5:18 p.m., giving soccer scores and sports news. Asked for Canadian and U. S. reports.

JLT3—15.225, Radio Tokyo, heard S-8 to S-9, at 7:10 p.m. with news in English.

HER4—6.340, Bern, Switzerland, heard 30 decibels above S-9, very strong at 10:10 p.m. Signoff was at 11 p.m.

Mr. Bromley added that he also receives Leopoldville, Brazzaville, fairly regular. He occasionally hears SUX,



THEY SAID IT COULDN'T BE DONE!

Back in 1938, Hytron began designing new dies and converting production machinery for the first BANTAM GT tubes. The industry said in effect: "You're crazy; it won't work. You can't telescope standard glass tubes to BANTAM size and get the same results." Beam tetrodes, such as the 50L6GT, particularly were considered impossibilities. The intense heat developed during normal operation would warp the elements and crack the small glass bulb.

But Bruce A. Coffin, originator of the BANTAM GT, stuck to his guns. In a few short years, Hytron developed over fifty GT types. The GT became the most popular receiving tube.* Short leads, low capaci-

ties, advantages of shorter bombardment at lower temperatures, ruggedness of compact construction plus both top and bottom mica supports, smaller size, standardized envelopes and bases—all contributed to that popularity.

The BANTAM GT permitted new space economies in pre-war receivers. Only its universal acceptance as standard by all manufacturers makes possible fulfillment of the Services' demands for receiving tubes. In increasing numbers, as this war draws to its ultimate conclusion, Hytron will continue to supply you with the popular BANTAM GT tubes which everyone said just couldn't be made.

**1941 industry production figures: GT—52,000,000; metal—27,000,000; standard glass, G, and octal—56,000,000.*



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Cairo, on 7.860 mc., around 4 p.m. with Oriental music. Two or three other African transmitters are heard irregularly. "I regularly pick up most of the South American stations, and usually can hear the British, French, Spanish, and German stations almost daily," he continues. "I can generally count on bringing in India two or three times a year; I hear the Japanese transmitters fairly often also, but as yet have not brought in any of the Chinese stations, or the Philippines. My location and antenna are only fair. My aerial is a 20-foot long one, running northeast by southwest. My Hammarlund HQ-120X has done good work. I have a high static level here and therefore the weaker stations are very hard to pull through," Mr. Bromley concludes.

PRISONER-OF-WAR MESSAGES

GERMANY—Prisoner-of-war messages from Americans interned in Germany are heard after the news, 10 minutes after the hour to the half-hour, from 9 p.m. on during North American service (5:30 p.m.-1 a.m.) over DXJ, 7.24, DXG, 6.19, and sometimes over DXP, 6.03, and DJD, 11.77; also reported over DXB, 9.61.

JAPAN—Radio Tokyo relays messages from American prisoners-of-war interned in Germany during the German hour each Saturday only, 12:30-1 a.m. over JVU3, 11.897, and JZI, 9.535. Messages from American prisoners-of-war interned in Japan are heard now 2-2:30 p.m. over JZI, 9.535 and JVW, 7.257, as well as JVW3, 11.725. Messages from Japan also are heard, 12:12:30 a.m. and 2:30-3 a.m. over JVU3, 11.897, JZJ, 11.80, JZI, 9.535 ("Humanity Hour" and "The Postman Calls" heard 2:30-3 a.m.).

WEST COAST REPORT

From August Balbi, Los Angeles, we have the following report this month: VLC2, 9.68, 12:15-12:45 p.m. to Britain; news, 12:15 p.m., replacing VLC8, 7.28, Shepparton, Australia. JVU3, 11.897, JZJ, 11.80, JZI, 9.535, Tokyo, 8:30-10:45 p.m., Home Service. JLT, 6.19, 7-8:15 a.m.; English news, 8:45 a.m. on 8:30-10:40 a.m. transmission; also heard, 11 a.m.-2:40 p.m., with news at 2 p.m. for Far East.

J—?, 6.11, heard 1-5 a.m., or later in Home Service.

XGOI, 7.48, Shanghai, 7:15-11 a.m., news, 8:15 a.m., Home Service.

XGOO, 9.66, Shanghai, 8-11:30 a.m., heard irregularly; bad QRM most days.

XGOY, 6.17, Chungking, was on 6.07 and 6.04 for one day recently but is now back for good on 6.17, strong signal; also heard on 7.15 with fair signal; bad QRM. The transmission is from 7:35-11:40 a.m., with English news at 10 a.m. On 9.646, XGOY now is heard, 12 noon to 1 p.m., with news in English at noon.

XGOA, 9.725, Chungking, is still on this frequency, but is seldom heard now.

PIRM, 6.14, Manila, heard 4-9 a.m., with English news at 8:30 a.m.; fair.

Delhi, India, 7.30, now heard 7:30-10:30 a.m., with news at 9:30 a.m.; signal fair to good. On 7.21, heard 9:10-10:30 p.m., BBC news at 9:45 p.m., weak to fair. On 6.19, heard 10:50 a.m. to noon; news, 10:50 a.m. followed at 11 a.m. by BBC news relay; QRM'd badly by JLT Tokyo; also heard 8:30-10 p.m., with BBC news relay at 9 p.m.; relays General Forces Program in English from London, badly QRM'd by DXG, Berlin; strong signal some days. On 6.06, Delhi is heard 9-11 a.m., replacing 6.01; some QRM, fair signal. Alma Ata, USSR, 8.815, heard 8 a.m. on-midnight, in parallel with 9.565 often; Home Service.

Petropavlovsk, Kamchak Peninsula, USSR, 6.07, 5-6 a.m., daily, and Sundays only, 1:13-2:40 a.m., Home Service; best SW signal ever heard here.

RW15, Khabarovsk, USSR, 5.935 now heard midnight-10 a.m. or later; strong, some code QRM; Home Service.

Madagan, USSR, 5.715, heard from 3:30 a.m. on; Home Service; fair signal.

Moscow-Komsolmosk, USSR, 11.885 and 15.23, 6.47-7.25 p.m., to U. S. in English; best on 11.885, strong signal; modulation very poor; barely understood.

Komsolmosk, USSR, 9.565, heard 2:30-3:15 p.m., 3:33-5 p.m., 10 p.m.-1 a.m.; Home Service; good signal; seldom heard now after 2:45 a.m.

VE9AI, Edmonton, Alberta, Canada, 9.54, has a new schedule of 10:15 a.m.-8 p.m.; and on 6.005, 8:15-10:15 a.m., 8 p.m.-2 a.m.; news at 10 a.m.; 1 a.m. Berne, Switzerland, 7.38, 6.34, 6.165, heard 9:30-11 p.m., off Saturdays; all in parallel; bad code QRM on 7.38, 6.34; also 6.165 QRM'd by CBRX; fair at times.

DXJ, Berlin, 7.24, is now back in operation to North America, 5.50-12 midnight; strong, irregularly.

DXG, Berlin, 6.19, a new station to North America, 5:30 p.m.-1:15 a.m.; very strong at times.

Radio Shonan (Singapore), now is heard, 6-7:30 p.m., with news in English at 7 p.m., on 15.45 mcs.

VDP2, Suva, Fijis, 6.135 now heard 1:55-5:30 a.m., with news in English at 2, 4, and 5 a.m.

LRS1, Buenos Aires, Argentina, heard 7 p.m.-12:30 a.m.

LAST MINUTE TIPS

LRU, Buenos Aires, 15.29, heard at 5:30 Sunday afternoon with concert; announcements of program in Portuguese, with station identifications in English. Algiers to New York heard S6 on 15.165 mcs. at 10:45 a.m. GRO, London, 6.180, ABSIE station, ends transmission at 9:45 p.m. (Richards, New York).

VLG3, Melbourne, 11.71, and VLC6, Shepparton, 9.615, beamed to the West Coast in the 2nd transmission to North America, 11:00-11:45 a.m., with English news at 11:00 and 11:35 a.m.; identified by the call of the Kookaburra bird; excellent. Radio Centre, Moscow, beamed to America, 6:48-7:25

(Continued on page 130)

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Bomber's Ears

(Continued from page 41)

take"—saved the lives of thousands.

Most people know the part radio plays at sea, but very few realize the important role radio has in combat flying. On a 15th AAF heavy bomber, the radio operator is a jack of all trades, a combination technician and combat man. As a result of an intense course in an Air Forces radio school, he knows the theory of radio, how to tune the sets in, and how to repair them; he must know code and how to quickly decode a message. Life moves quickly in the air, there's no room for second guessing; the radio operator has to do

everything right—the first time.

The radio operator also has been to an Air Forces gunnery school. In a Flying Fortress, he works a .50 machine gun mounted on top of the radio hatch. In the B-24 Liberator bomber, the radioman doesn't have his own gun, but usually takes over the waist or top turret guns in an emergency. Of the two, the Liberator man has the hardest job—he has to sit at his radio, sweating out the flak and fighters around him, without the solid satisfaction of shooting back that the B-17 man has.

Operating radios and guns is only a part of the radio operator's duties. He also may be called upon to use a camera over the target.

To understand the part radio plays in air battle, let's follow a Flying

Fortress as it takes off from its Italian base to bomb one of the Nazi oil refineries in the Balkans.

Before the plane takes off, the radio operator checks his own set, the command and v.h.f. sets of the pilot, and the navigator's compass radio set. There are several other radios on the plane that are used in case of an emergency.

Once in the air, the radio operator monitors his set, tuned to the frequency of his home base. He keeps a log of all messages, which of course are sent in code—a new code being used for each mission.

Over the target, or as soon as they encounter enemy fighters, he mans his gun, still monitoring the radio. The pilot may cut in, via the interphone, and call out, "Bandits at 3 o'clock!" Meaning that enemy fighters are coming in from the right.

"See them, sir," the radioman answers, tracking the approaching fighters with his machine gun.

As they make the bomb run, the radio operator looks into the bomb bay and tells the bombardier that all bombs are away, or that a bomb is stuck and will have to be salvaged.

If the fighter escort keeps enemy fighters away from the formation, the radioman uses his camera to take pictures of the bombs striking the blazing oil below. No matter what his job, he monitors his special frequency set at all times—the only connection between the bombers and their original base.

As the bombers head for home, the radio operator on the lead plane often radios the base, giving the results of the bombing. Except in cases of extreme emergency, the radio operator will not send a message while on the way to the target. It would be a dead giveaway as to course and target, and the Nazis would have a welcoming party of fighters waiting.

The command pilot in the lead ship may radio his bombers or the fighters special instructions, or order a change in formation—the pilot receiving this on his v.h.f. set—but this is done only in an emergency or when the enemy has already sighted the planes.

Returning to base, the pilot receives landing instructions—his position in the traffic pattern—via his command set. If there is a wounded man aboard, the pilot may drop a flare, or give instructions over the radio for an ambulance to meet them.

Only when wheels finally touch the runway does the radio operator turn off his set.

Should the heavy bomber become separated from the formation, perhaps crippled and lost in the clouds, the navigator uses his compass radio set to get his bearings. If forced down at sea, the radio operator sends out an S.O.S. on a special set.

The combat radio operator-gunner is probably the busiest man in the bomber crew, and radio communications are as necessary to a big bomber as are the wings or the four motors!

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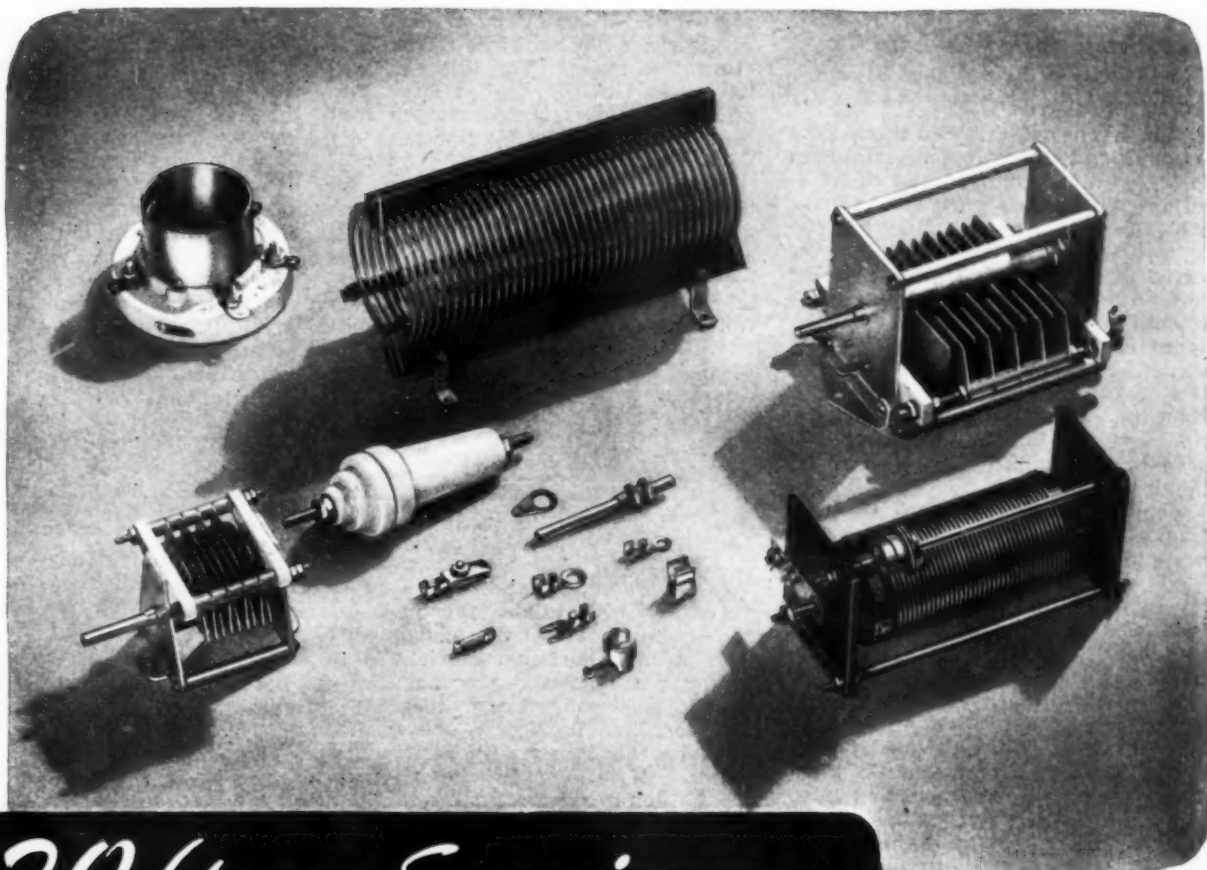
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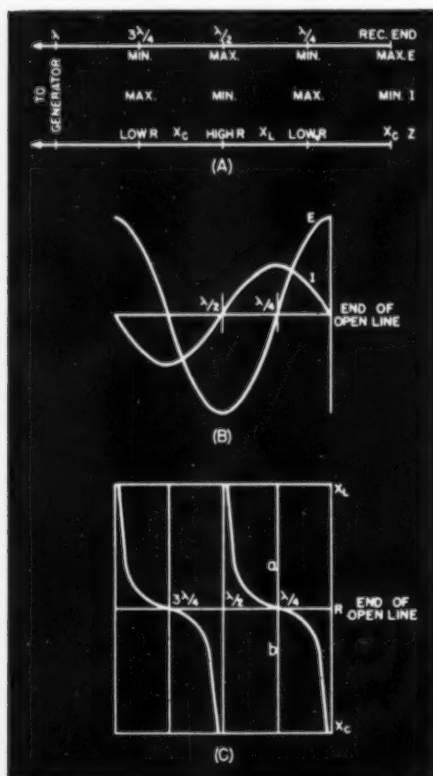
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Transmission Lines (Continued from page 31)

in this manner will do two things: the ratio of maximum voltage to minimum voltage will be changed and their locations will be shifted. The relative values of V_{max} and V_{min} may be read on the type of meters previously referred to as A or B, bearing in mind that with meter A the crystal must be calibrated and with meter B, the square root of the meter readings must be used. The location of V_{max} and V_{min} may be designated as so far from the receiving end and may be expressed in linear units (cm. or inches) or angularly in degrees or radians.

A special case exists when the terminating impedance is equal to the characteristic impedance. Here V_{max} equals V_{min} and there are no standing waves on the line. This is known as a matched or flat line and is the one we generally strive to attain. Since standing waves are caused by waves being reflected back from the load, they represent a certain amount of power not available to the load, hence a loss. Also, standing waves in high Q circuits give large current and voltage values, thus requiring the use of larger conductors and more insulation and therefore are undesirable. They also represent phasing problems when several antennas are fed from the

Fig. 9. (A) Showing the variations of voltage, current, and impedance points along a transmission line. (B) Illustrating the 90° phase shift between the voltage and current. (C) Illustrating graphically the impedance variation along the transmission line.



same line. Then again, ohmic losses are less in a flat line since the average current is lower. The line also will have less tendency to radiate. Another important consideration is that the impedance of a flat line does not vary with its length.

No standing waves will be found on the line under two conditions. The first is where the line is infinitely long and the voltage and current values become 0 before the end of the line is reached. Since we can have no reflection under this condition we will



Fig. 8. Illustrating an open-end transmission line several wavelengths long.

have no standing waves and also no power will be available for the load. The second is where the load impedance equals the characteristic impedance and maximum power is available to the load. Under these two conditions we have but one choice but even this is not without its difficulties. If we apply the formula $Z_0 = 276 \log b/a$ and attempt to match the 73 ohms which a half-wave dipole antenna presents to the line, we find it physically impossible.

Matching Methods

It therefore becomes necessary to use a greater value of Z_0 , say several hundred ohms, and use some impedance-matching device. There are several ways of doing this. It could be done by using a closed quarter-wave or odd multiple section and tapping. See Fig. 5.

Stub Matching

Another, and one of the most important methods of matching a line to an antenna (see Fig. 6) is by means of stubs. The stub is a section with the same dimensions—except length—as the line. It is placed on the line usually at right angles to it and is so designed as to match the impedance of the line with terminating impedance. In this case the terminating impedance consists of the stub, the line beyond the stub and the antenna. It is complex, consisting of resistive and reactive components. The stub is placed on the line where the resistive component equals Z_0 . The reactive component may be either inductive or capacitive and must be cancelled by using an open or shorted stub which gives an opposite reactance of the same magnitude. We will endeavor to explain the technique of this operation at 200 mc., giving an example using figures taken with the equipment previously described.

Load the transmission line with a dipole, a quarter-wave on either side of the line, and make the following measurements, using meter B. 1. Location of V_{max} . 2. Magnitude of V_{max} . 3. Magnitude of V_{min} . 4. The wave-

length. The wavelength may be found by measuring the distance between two adjacent parts of V_{max} and multiplying the result by 2.

Great care should be exercised in making the measurements of V_{max} and V_{min} because the results depend largely upon them. The quarter-wave lines on the meter may be moved along the line at an angle, but when the readings are taken they should be at right angles. It must be remembered that the square root of the meter readings are to be used on account of the characteristics of the meter.

The calculations in the simplest form follow:

$$Q = V_{max} / V_{min}$$

$$K = \frac{Q - 1}{Q + 1}$$

where K is the reflection coefficient.

The location in degrees from V_{max} toward the sending end for the shorted stub may be found from:

$$\frac{(-\cos^{-1}K) \text{ plus } 180^\circ}{2} \dots \dots \dots (1)$$

The length in degrees for the shorted stub would then be:

$$\tan^{-1} \frac{\sqrt{Q}}{Q - 1} \dots \dots \dots (2)$$

For those not familiar with these notations, the first formula reads

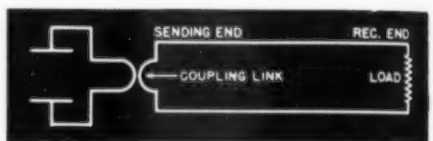


Fig. 7. A two-wire balanced transmission line, using 3/8-inch copper tubing.

"minus the angle whose cosine is K plus 180° divided by 2." The second reads "the angle whose tangent is $\frac{\sqrt{Q}}{Q - 1}$." All you have to do is figure the value of the fraction and look up the corresponding angle in a table of natural trigonometric functions.

The distance to an open stub from V_{max} toward the sending end will be:

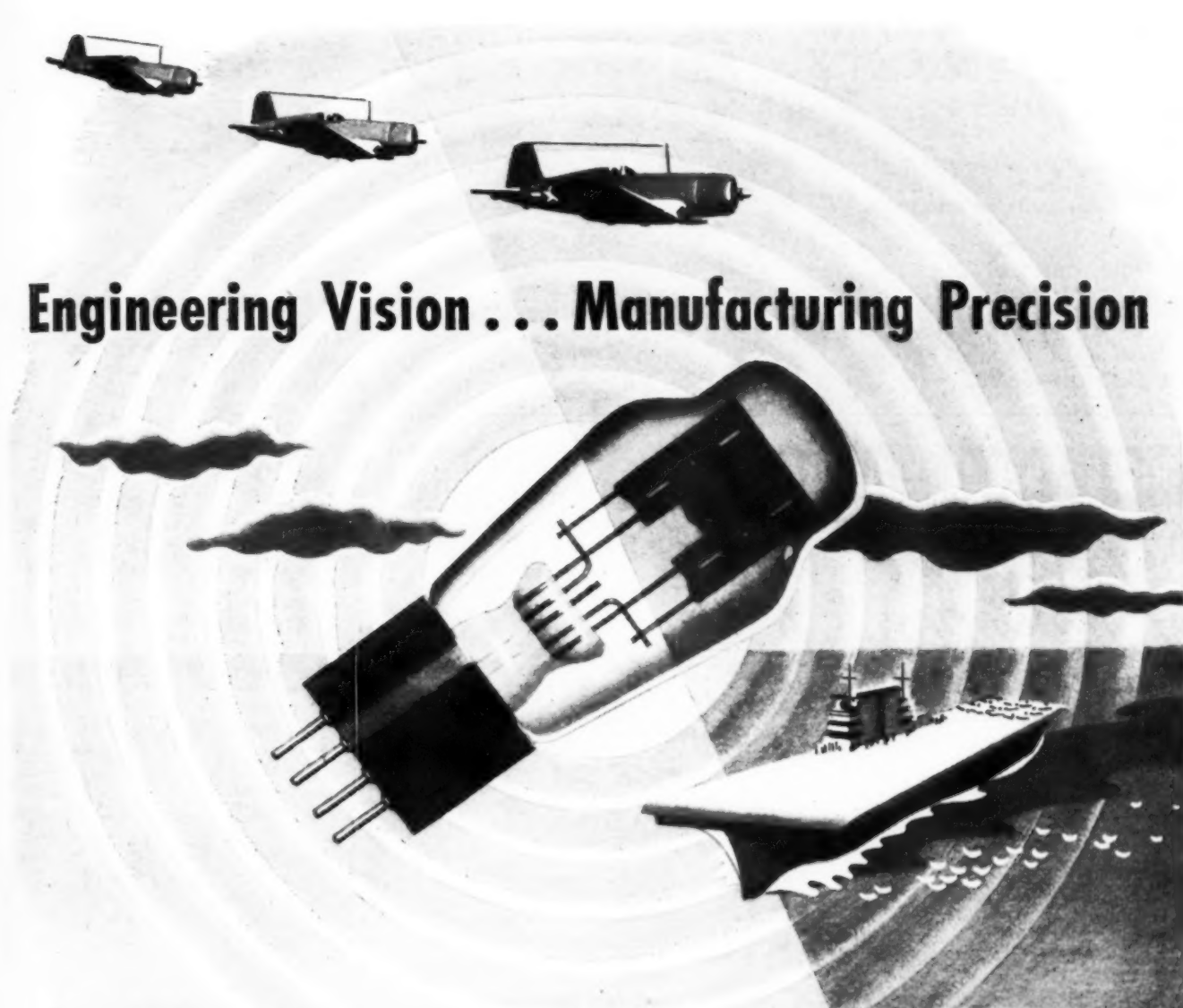
$$\text{distance in degrees} = \frac{(\cos^{-1}K) \text{ plus } 180^\circ}{2}$$

and the length of the open stub is found from:

$$\text{length in degrees} = \tan^{-1} \frac{Q - 1}{\sqrt{Q}}$$

Meter C should be placed near the sending end and the length of the quarter-wave line on meter B should be adjusted for minimum deflection on meter C as meter B is moved along the line.

It will be noticed that the results



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are given in degrees. This makes the method flexible so that it may be applied to any wavelength. To convert to linear units such as centimeters or

inches, use $\frac{x}{360} \lambda = D$

where:

x = length or position in degrees

λ = wavelength

D = linear units as selected

Here is an actual example taken with the equipment described. The measurements were

1. V_{max} from the receiving end was found at 38 and 113 cm.
2. Magnitude of V_{min} was $\sqrt{9}$

3. Magnitude of V_{min} was $\sqrt{9}$
4. Wavelength from (1), $(113 - 38) \times 2 = 150$ cm.

The calculations were:

$$Q = \sqrt{\frac{75}{9}} = 2.88$$

$$K = \frac{2.88 - 1}{2.88 + 1} = .485 = \cos 61^\circ$$

Position of shorted stub

$$\frac{-61 + 180}{2} = 59.5^\circ$$

Converting to cm. $\frac{59.5 \times 150}{360} = 24.8$ cm. from V_{max} , or

$24.8 + 38 = 62.8$ cm. from antenna

Length of shorted stub =

$$\tan^{-1} \frac{2.88}{1.88} = \tan^{-1} 0.902 = 42.1^\circ = 17.5 \text{ cm.}$$

Similarly, using the formulas for the open stub, the position was calculated to be 50.25 cm. from V_{max} and the length 20 cm. The position of the stub from the antenna is $50.25 + 38 = 88.25$ cm. Since this is more than a half wavelength, we should move the stub 75 cm. toward the receiving end and place it at 13.25 cm. This is possible because all the conditions on the line recur every half wavelength, the preferred positions being nearest the antenna.

Hints and Kinks

Persons with limited experience with ultra-high frequencies probably will be bothered by all sorts of manifestations not usually encountered at lower frequencies. For instance, a person moving in the room where the work is going on, may cause the deflections on sensitive detector meters to vary. There is no way of avoiding this except to have all the conditions surrounding the equipment as stationary as possible.

In tuning up the oscillator, it may be found that the plates will get red due to excessive current. Try adjusting the L-C ratio of the plate tank circuit. Try to get a no-load current of 50-60 ma.

Getting the so-called quarter-wave lines on meter B to offer enough impedance so that there is little effect on the line, is sometimes difficult. The reason for this is that we are never sure just what our meter adds to the circuit. It may add inductance or capacitance depending on the construction of the meter. The solution is to place meter C near the sending end and adjust the lines for minimum change on meter C as meter B moves along the line.

Watch out for over-coupling when the line is being used as a Lecher system. All points of V_{max} must be equidistant without minor humps in between.

When taking readings of relative voltage using a crystal and d.c. meter, the crystal must be calibrated. The method is to terminate the line with a resistance and use an amount of coupling which will give a V_{min} near the bottom of the meter and a V_{max} near the top. Plot the readings on the meter against degrees along the line, for a half wavelength. Then superimpose a sine wave on the crystal curve using the same maximum and minimum points. The readings on the crystal curve should then be projected on the sine curve to get their true relative values.

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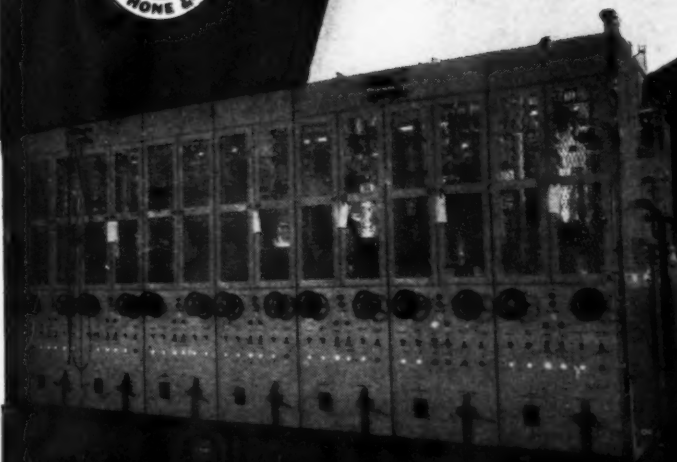
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A few more do's and don'ts. Keep line meter probes at right angles to the line. The probes must make good contact. Keep the line and antenna as far away as possible from other objects. Do not separate the lines more than 1.5 inches for 200 mc. Fluorescent lamps when fired take power from the line and therefore should be separated from the line as far as possible. Another way of using the lines as a Lecher system is to place meter C near the sending end and move a shorting bar along the line.

There is a great deal more to this subject, but this much will keep you busy for a while and you will have learned the basic theory of transmission lines.

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Filter Design

(Continued from page 40)

ous rectifier tubes such as the 866, the load current should not exceed about 25% of the rated peak current of one tube when a full-wave rectifier is used, or $\frac{1}{3}$ the rating with half-wave rectification.

A bleeder resistor should be used with both a condenser input and a choke input filter to keep the voltage from rising to its peak value and so provide better regulation, and to discharge the filter condensers in case the load is removed before the power is turned off. The bleeder should have a resistance such that it draws from 5% to 10% of the full load current. The actual value is not critical. The resistor should be capable of dissipating the heat generated without being damaged. The power dissipated in the resistor is given by the equation:

$$W = I^2 R = E/R \dots \dots \dots (7)$$

where I is the current through the resistor, and E is the voltage across it. The actual wattage rating should be about twice that calculated to avoid excessively high resistor temperatures.

The filter condensers should have a d.c. working voltage rating at least equal to the peak voltage of one half the transformer secondary and preferably a little higher to provide a safety factor. As with the choke input filter, two or more condensers may be connected in series to give an adequate working voltage rating. In general, electrolytic condensers are used where the voltage does not exceed 450 volts, as they are much cheaper and smaller than paper condensers of the same capacity rating.

If the current drain from the power supply is rather small as in the case of small a.c.-d.c. receivers, the filter choke may be replaced by a small resistor. This impairs the filtering action somewhat, but with large condensers, the filtering may still be adequate for the particular location. The decrease in cost and weight more than makes up for the necessary increase in the size of the condensers.

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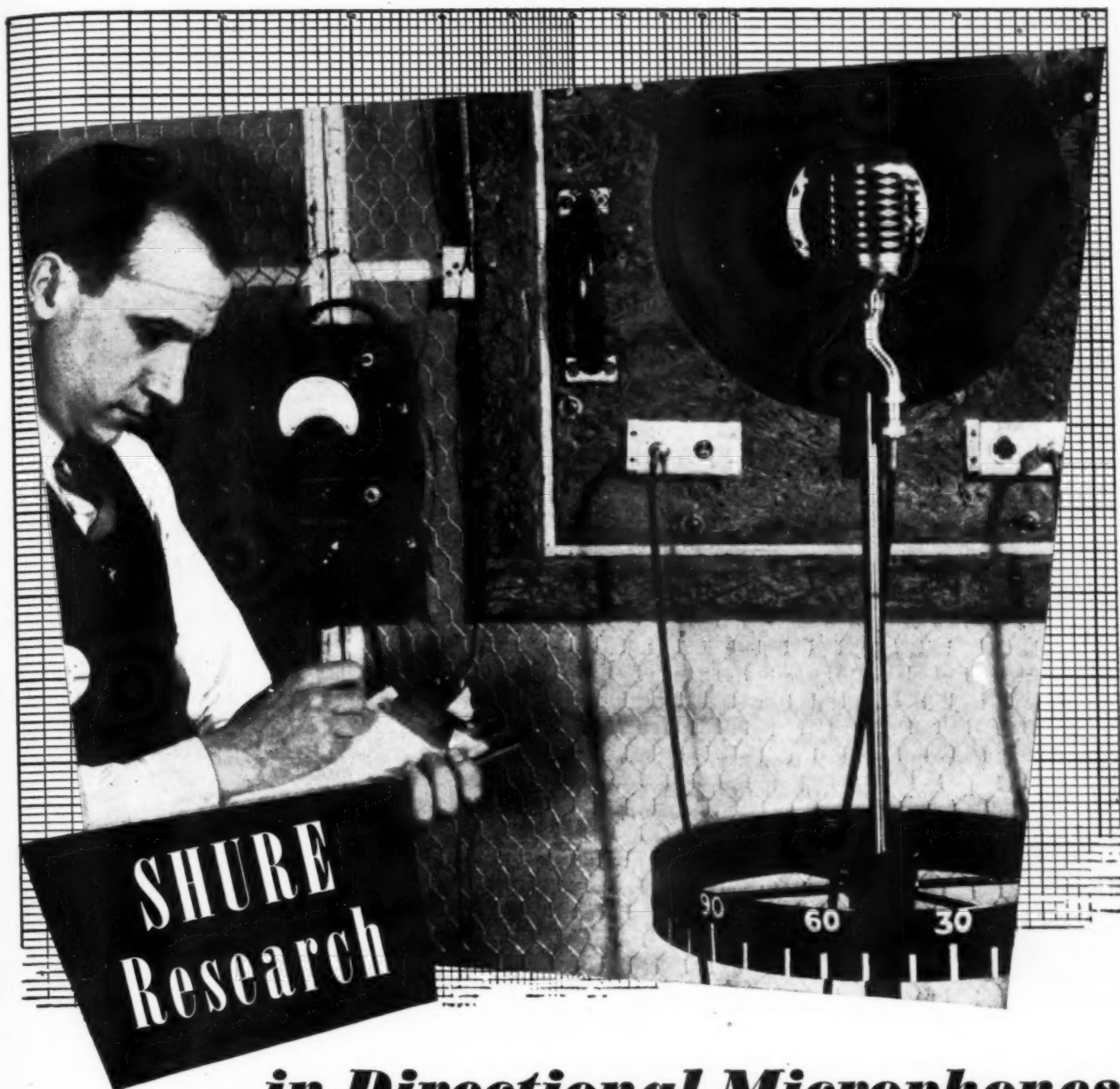


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The properties of condenser and choke input filters are somewhat different, and their applications are correspondingly different. For a given rectifier, the output voltage from a choke input filter will be lower than from a condenser input filter, but the regulation will be better. Consequently, choke input filters are ordinarily used where good regulation is desirable, as in applications where the load may vary over quite wide limits. Also, choke input filters are used to keep the peak rectifier current down, a condition which is desirable when mercury vapor rectifier tubes are used. Condenser input filters are widely used in low-voltage, low-power applications where high-vacuum rec-

tifier tubes are used. Such applications are domestic radio receivers, small public-address systems, low-power transmitters, phonograph amplifiers, and similar devices.

In all the above filter designs, care should be taken to see that the LC combinations are not resonant at the ripple frequency, or some harmonic, as this may introduce an excessively high ripple voltage in the output, and may puncture the condensers. The resonant frequency for the choke input filter is $1/2\pi\sqrt{LC}$. For normal values of inductance and capacity, the resonant frequency of a filter will be well below the ripple frequency.

It is possible to design resonant filters which are effective, but the

values of the components are quite critical, and any change in either inductance or capacity would greatly reduce the effectiveness of the filter. Resonant filters usually are designed with a parallel resonant circuit in series with the high-voltage lead to provide a high impedance at the ripple frequency, or a series resonant circuit across the supply to short circuit the ripple frequency. Resonant filters are not recommended for normal applications, such as radio receivers.

Sufficient information has been given above for designing a power supply filter for most normal applications. However, an example might serve to clarify the procedure.

Suppose a low-power audio amplifier is being designed. The power requirements are 350 volts at 75 ma. A full-wave rectifier operating from a 60-cycle supply line is to be used.

Because of the small power requirement in this case, a condenser input filter with a high-vacuum rectifier is chosen. An input condenser of 8 to 10 μ fd. will be satisfactory, and the d.c. working voltage should be at least 400 volts, and preferably 450 volts. The peak voltage rating should be 600 volts, as the peak value of the transformer secondary will approach this value.

A bleeder resistor which will draw between 5 and 10% of full-load current must be provided. This will mean approximately 5 ma. at 350 volts, or 70,000 ohms. The power dissipated in this resistor will be, from Eq.(7), $(.005) \times 70,000 = 1.75$ watts. A 5-watt resistor, two 2-watt resistors (140,000 ohms each) in parallel, or two 2-watt resistors (35,000 ohms each) in series, would be suitable.

To determine the size of the output condenser, the total load resistance must be calculated. The total load current is $75 + 5 = 80$ ma., the voltage 350 volts, so from Ohm's Law ($R = E/I$), the load resistance is $350/.080 = 4,375$ ohms. From Eq.(6), assuming a minimum frequency response of 50 cycles per second, the output capacity should be $C = 10^7/\pi \times 50 \times 4,375$, or about 15 μ fd. A 16- μ fd. condenser should be very satisfactory.

A choke with a value of about 20 henrys at 80 ma. will give adequate filtering for the amplifier. From Eq. (4), it is seen that the choke and second condenser alone would reduce the ripple to about $1/4$ of 1%, and the input condenser will bring the ripple well below this value.

There is one other factor which should be considered in purchasing a choke. Since it is connected to the B+ supply and the frame is invariably grounded, the choke winding must be well insulated from the core.

In designing a filter for any purpose, it always pays to purchase quality parts with adequate current and voltage ratings in order to get satisfactory performance over a long period of time.



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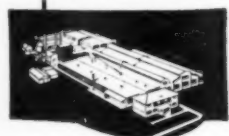
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Cathode Follower

(Continued from page 55)

the load is connected in the cathode circuit. From an arrangement of this sort, a low-impedance output may be obtained.

"The principle of operation is degenerative; that is, a signal of approximately 100 volts peak may be applied to the cathode-follower grid. The cathode, not being tied to ground, follows this voltage to such an extent that the grid is never positive with respect to cathode. The available output voltage is therefore less than the input voltage.

"The output of the preamplifier is low impedance . . . the line may be run any desired distance to the modulator chassis. This allows the driver transformer to be at the grids of the power tubes."

Grid to ground capacitance in the cathode follower is unaffected by the negative feedback voltage and this advantage enables one to use the circuit as a probe for measurement of wave shapes with a scope. Some circuits used in producing certain pulses are so easily upset that the capacity of conventional test leads destroy the original wave shape before it is viewed on the scope. Thus, a true picture of the wave under test is not obtained.

By feeding the test wave directly into a cathode follower we are able to pass the original signal on to a scope without creating any unbalance.

Working backward from the original use of a cathode follower it has been found that such a circuit may be used

to couple a low-impedance source to a high-impedance input circuit with a good match, no distortion, and no phase shift. Such a use might occur where video signals were involved and no transformer of the desired characteristics could be located.

By placing a steady bias on the grid of a cathode follower and feeding the low-impedance source into R_k , the resulting plate output voltage of the stage may be fed into the high-impedance circuit with the proper match and correct frequency response. See Fig. 5.

APPENDIX 1

$$e_{in} = e_g + i_p R_k$$

$$e_o = i_p R_k$$

$$i_p = \frac{\mu e_g}{R_p + R_k}$$

$$G = \frac{e_o}{e_{in}} = \frac{i_p R_k}{e_g + i_p R_k}$$

$$= \frac{\frac{\mu e_g}{R_p + R_k} \cdot R_k}{e_g + \frac{\mu e_g}{R_p + R_k} \cdot R_k}$$

$$= \frac{\mu e_g R_k}{e_g R_p + e_g R_k + \mu e_g R_k}$$

$$= \frac{\mu R_k}{R_p + R_k + \mu R_k} = \frac{\mu R_k}{R_p + R_k (\mu + 1)}$$

$$= \frac{\mu}{\mu + 1} \cdot \frac{R_k}{\frac{R_p}{\mu + 1} + R_k}$$

If μ is much greater than 1, then

$$\frac{\mu}{\mu + 1} = \frac{\mu}{\mu} \text{ or } 1 \text{ and } \frac{R_p}{\mu + 1} = \frac{R_p}{\mu} \text{ But}$$

$$\frac{\mu}{R_p} = G_m \therefore \frac{R_p}{\mu} = \frac{1}{G_m}$$

$$\text{Thus Gain} \cong \frac{R_k}{\frac{1}{G_m} + R_k}$$

APPENDIX 2

$$i_p = \frac{\mu e_g}{R_p + R_k}$$

$$e_g = e_{in} - e' \therefore i_p = \frac{\mu (e_{in} - e')}{R_p + R_k}$$

$$e_o = i_p R_k = \frac{\mu (e_{in} - e') \cdot R_k}{R_p + R_k}$$

$$e' = e_o \therefore e' = \frac{\mu (e_{in} - e') \cdot R_k}{R_p + R_k}$$

Solve for e'

$$\begin{aligned} e' \cdot (R_p + R_k) &= \mu R_k (e_{in} - e') \\ e' R_p + e' R_k &= \mu R_k e_{in} - \mu R_k e' \\ e' R_p + e' R_k + \mu R_k e' &= \mu R_k e_{in} \\ e' (R_p + R_k + \mu R_k) &= \mu R_k e_{in} \\ e' &= \frac{\mu R_k e_{in}}{R_p + R_k + \mu R_k} = \frac{\mu R_k e_{in}}{R_p + R_k (\mu + 1)} \end{aligned}$$

$$e' = \frac{\mu}{\mu + 1} \cdot \frac{R_k e_{in}}{\frac{R_p}{\mu + 1} + R_k}$$

$$G = \frac{e_o}{e_{in}} = \frac{e'}{e_{in}} = \frac{\mu}{\mu + 1} \cdot \frac{R_k}{\frac{R_p}{\mu + 1} + R_k}$$

APPENDIX 3

$$\begin{aligned} Z_o &= \frac{R_p}{\mu + 1} \cdot R_k = \frac{R_p R_k}{\mu + 1} \\ &= \frac{R_p R_k}{\frac{R_p}{\mu + 1} + R_k} = \frac{R_p R_k (\mu + 1)}{\mu + 1} \\ &= \frac{R_p R_k}{R_p + R_k (\mu + 1)} \end{aligned}$$

$$Z_I = \frac{R_p R_k}{R_p + R_k (\mu + 1)}$$

$$Z_I [R_p + R_k (\mu + 1)] = R_p R_k$$

$$Z_I R_p = R_p R_k - Z_I R_k (\mu + 1)$$

$$Z_I R_p = R_k [R_p - Z_I (\mu + 1)]$$

$$R_k = \frac{Z_I R_p}{R_p - Z_I (\mu + 1)}$$

If μ is much greater than 1, then Z_I is small compared with μZ_I , and

$$R_k = \frac{Z_I R_p}{R_p - Z_I \mu} = \frac{Z_I}{1 - Z_I \frac{\mu}{R_p}}$$

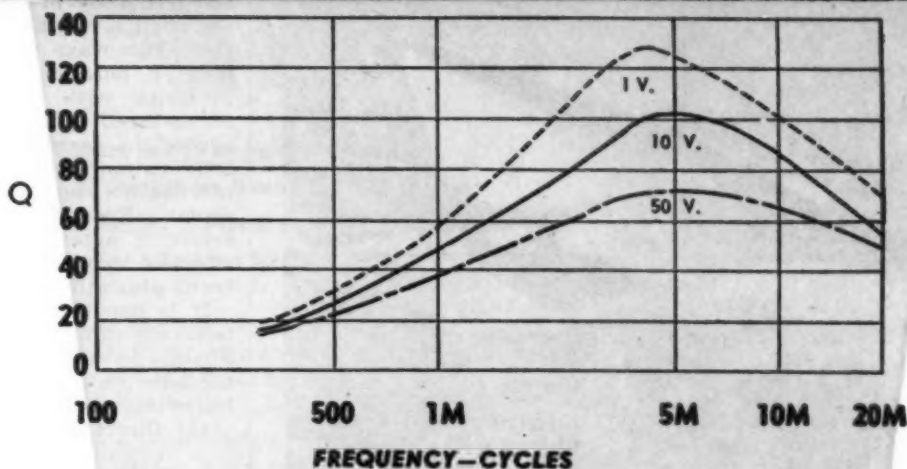
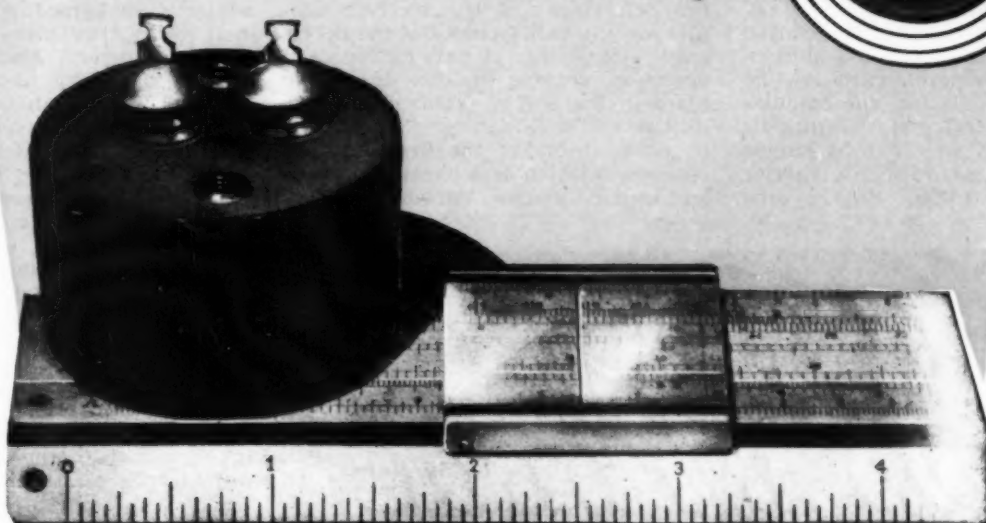
$$R_k = \frac{Z_I}{1 - Z_I G_m}$$

-30-

British and American amateur radio operators meet at Mostyn A.R.C. Club, London. All nine districts of the United States are represented by (left to right) T/Sgt. Albert Savage, Pawtucket, R. I., W1CPV; Cpl. Fred Roden, West Lebanon, N. Y., W2KED; Dan Stevens, O.W.L., Upper Darby, Pa., W3CBY; Chap. J. B. Andres, Skyland, N. C., W4EFG; Cpl. Mitchell Wiseman, Indianapolis, Ind., W5KSU; T/Sgt. John B. Barclay, Taft, Cal., W6OIT; Cpl. William Garbutt, Greybull, Wyo., W7GZI; T/Sgt. Omar H. Mitchell, Charleston, W. Va., W8KFZ; and T/4 Lloyd C. Dothe, Barnum, Minn., W9SYX.



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Practical Radio Course

(Continued from page 53)

course, is essential to this process. The action may occur in this way: If an undesired station (or stations) delivers an extremely strong carrier voltage to the tube, that tube may act as a rectifier. Therefore, overload of the tube will introduce rectification where it is not desired, and since a rectifier may eliminate a carrier while retaining its modulation, the modulation of this interfering station may be present distinctly in the tube circuit and become *mixed* with the carrier of the desired station. So the tube

acts as a rectifier and a mixer, and the audio component of the undesired carrier is modulated upon the other. Hence, the carrier of the *desired* station brings in the desired program but since it is also modulated by the audio pulses extracted from the *undesired* cross-modulating carrier, interference results.

When cross-modulation occurs, the first r.f. stages of the receiver usually are the guilty ones, but the necessary interfering signal pickup and detection causing it can also take place in the audio system if the conditions are satisfactory. The degree of vulnerability of the first stage to cross-modulation is a matter of tube and circuit design. Variable-mu (su-

per-control) type r.f. pentodes which have a much more extended cutoff characteristic than do screen-grid tubes (see Fig. 5), thus enabling larger input signal voltages to be applied and making possible the application of a higher bias for reduction of signal strength (volume control) without increasing the susceptibility of the stage to detector action or cross-modulation, are a great help when they are employed in the first r.f. stages. Also, providing sufficient selectivity *ahead* of the first receiver stage (ahead of the place where detection can occur) so that the presence of the undesired signals on the grid of the first tube is avoided, is probably the most effective preventative. In some receivers, extra link circuits are included in the antenna-stage tuning circuits especially for this purpose.

If an existing receiver is troubled by cross-modulation interference, the identity and carrier frequency of the interfering station should be established first. If the receiver design already provides a reasonable amount of selectivity in the antenna end, an ordinary wave trap having good attenuation characteristics and tuned to the frequency of the station causing the trouble will be effective. In some cases two wave traps may be necessary; a parallel-tuned rejector trap in series with the antenna and a series-tuned acceptor trap shunted across the receiver input is the best combination for obtaining the utmost attenuation against the interfering signal. Reducing the length of the receiving antenna, or the use of an effective type of noise-reducing antenna also will help.

It is possible, however, for the interfering signal to enter the receiver directly by way of circuits other than the antenna input. These may be the following:

- (1) Direct pickup by exposed grid circuits and wiring associated with early tuned stages.
- (2) Direct pickup by the tubes of the receivers (if not properly shielded).
- (3) Direct pickup by the power supply line.
- (4) Direct pickup either on the chassis or the ground circuit where this is mutual to an r.f. circuit.

Filtering the power line; shielding all exposed grid leads and wiring of the first stages (including under-chassis wiring); having ground of low r.f. impedance and short length; and even a change of the applied voltage or operating characteristic of the stage affected so as to reduce the level of the interfering signal voltage—or its effect—are effective remedies.

With the increase in the number of high-powered transmitting stations that are frequently located within comparatively short distances of each other (10 miles or so) another type of cross-modulation interference—occurring entirely *external* to the receiver (either t.r.f. or superhet type) has be-



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come prevalent in the vicinity of these stations—especially where exposed open-wire power lines are in use. This type of interference is called *external cross-modulation*.

When two radio waves of sufficient strength encounter any elevated system of electrical conductors in which system there exists anything that causes rectification or detection—even though it be a relatively poor rectifier—numerous new spurious combination and harmonic radio frequencies are created. This is illustrated in Fig. 2 for the case of rectification of two original frequencies, A and B of 760 kc. and 710 kc. respectively. These new frequencies radiate from the system to nearby receiving antennas, and thereby are introduced into the receivers associated with them. When one or more of these interfering frequencies happens to fall at a desired station frequency, interference results. Since this cross-modulating action takes place entirely outside of the receiver, it causes interference that no receiver can avoid. Such interference is generally localized in a particular community.

Observation and experience have shown that the offending electrical system, whether it be power distribution, telephone system, or other aerial network of conductors (and particularly any network or system which is resonant to the local station frequency), can produce this interference if it has a rectifying tendency. Rectification may occur from poor joints or contacts, from an oxidized copper conductor in contact with another copper surface (producing a rectifier), from certain types of lighting arresters, special nonlinear devices, intermittent or poor contacts to earth or to other objects, and rectification due to chemical action at a joint or splice.

The "neutral" or "grounding" system for power circuits of the exposed overhead type is a frequent cause for generation of this type of interference. Also, it has been found that the trouble can be caused by contacts between electric conduits, plumbing pipes, and even from contacts of such piping with metal lath in walls through which they pass. In short, any electrical conductors exposed to very strong signals, and having a rectifying contact, can generate the spurious frequencies. Incidentally, a great many cases arise from faulty contacts in the antenna and ground circuit wiring of the receiver installation itself.

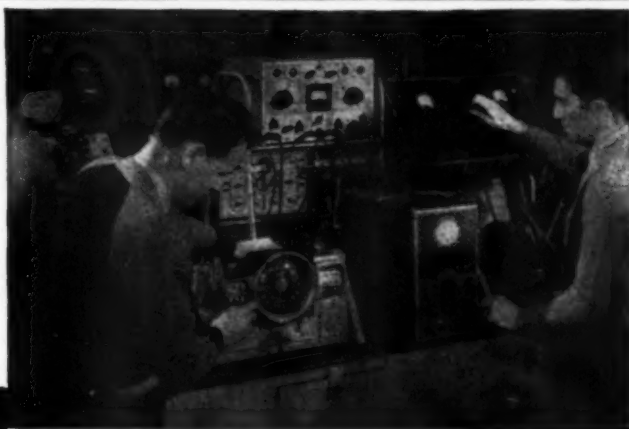
Familiar experiences of this type are those in which the interference changes with weather conditions, or where the output of the receiver varies in accordance with whether certain light switches are turned on or off. Cases also have been reported where the cross-modulation effect was so related to the lighting circuit that it was produced only when a certain switch was closed.

If this type of interference is experienced, it definitely should be iden-

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tified by checking with a small battery-operated loop-antenna type receiver (or one equipped with a short antenna). With its aid the place where the interfering frequencies are being produced often may be determined.

If the source of the trouble cannot be isolated easily, the procedure to follow is to eliminate any rectifying elements or contacts and also to remove all r.f. potentials from the power lines of the house. The first step is to eliminate all poor contacts and joints which may be present in the antenna and ground circuits. These connections should be clean and preferably soldered. If the cross-modulation still persists, one or more of the following remedies probably will clear up the situation:

- (1) See that the power line and telephone line grounds are secure.
- (2) Ground the neutral of the house wiring at the house, in addition to retaining the ground at the distribution transformer.
- (3) Ground all conduits solidly.
- (4) Use an improved ground at the receiver.
- (5) Install an r.f. by-pass condenser from each side of the power line to ground at the point where it enters the house, near the receiver, or in both places.
- (6) In some cases, it is necessary to install r.f. chokes in the line, as well as the by-pass condensers.
- (7) Relocate the antenna so that there is less pickup from the power line to the antenna or leadin. Use a shielded leadin or an effective type of noise-reducing antenna where necessary.
- (8) Orient loop antenna for minimum pickup from the interfering station or stations.

Same-Channel Station Beat Interference

In areas remote from a usable assortment of strong stations, or wherever signals of two stations on the same channel are received at comparable strength, a flutter, waver, or growl due to one of the stations may be heard in the background when tuned to the other. This is due to the slightly differing carrier frequency of the undesired received station signal. Receivers having high sensitivity and extended bass response are especially susceptible to such interference.

Remedies for this type of interference lie in the use of a directive or loop antenna aimed so the interfering station is received with minimum strength; reduction of the sensitivity of the receiver; or reduction of the bass response.

Adjacent-Channel Station Beat Interference

In localities where a received adjacent-channel station signal is strong

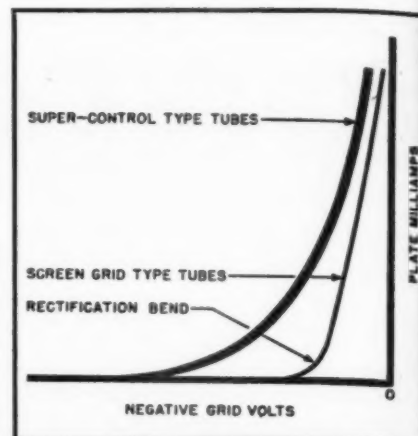


Fig. 5. Super-control-type tubes have an operating characteristic that permits wide input voltage swing with little detection, thereby reducing cross-modulation effects. Screen-grid-type tubes cause cross modulation on strong signals when they are used in the early r.f. stages of either t.r.f. or superheterodyne receivers.

compared to that of the desired station, a steady 10,000 cycle note or "whistle" will be heard due to the carrier of the adjacent-channel station (which is 10 kc. removed from that of the desired station) beating with the carrier to which the receiver is tuned. This type of interference can occur both in t.r.f. and superhet receivers—especially those having limited selectivity and wide range of audio response. Remedies for this type of interference lie in:

- (1) Careful realignment of the receiver tuned circuits—especially those of the i.f. amplifier, for it is in this part of the receiver that most of the adjacent-channel selectivity is obtained.
- (2) Suppression of the adjacent-channel interfering signal by means of a sharply-tuned antenna-circuit wave trap.
- (3) Reduction of the high-frequency response of the audio system.
- (4) Use of a directive or loop antenna so aimed as to reduce the strength of the received interfering signal.

Monkey-Chatter

In localities where the signals of adjacent-channel stations are strong, or where these stations employ higher-frequency-response transmitters, t.r.f. or superhet receivers having wide-band selectivity and audio response (high-fidelity receivers) may be troubled by unintelligible modulation superimposed upon the signal of the desired station, this modulation having the character of "inverted speech" sounding like "monkey chatter."

Let us see what causes this. When two received signals occupy adjacent channels, with a carrier-frequency separation of 10 kc., the extreme side-band frequency of one station is very close to that of the adjacent-channel station. If either station is modulating more than 5 kc. of audio range, the two side-bands will over-

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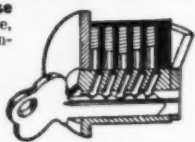
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lap. In such a situation, if the side-band of one signal enters the second detector stage along with the side-band and carrier of the other signal (as will be the case in a high-fidelity receiver operating with its full broad-tuning and audio response, allowing a passage of frequencies $7\frac{1}{2}$ kc. on each side of the carrier—a total band of 15 kc. width), a peculiar combination of frequencies will result. The most troublesome frequency formed by this combination is that which is produced by the *difference* between 10 kc. and the modulation frequency involved. For example, in the case where a 3000-cycle note is modulating the adjacent undesired channel, it will produce an interfering side-band which will be superimposed upon the desired signal as a 7000-cycle note. That is to say, the side bands of the adjacent-channel station form a *difference* beat against the carrier of the desired station, or the one to which the receiver is tuned. This beat will be in the audible range and will have the character of "inverted speech." This means that a low-frequency modulation on the interfering station signal will create an audible signal of 10 kc. *minus* this frequency, or a resultant high frequency. High-frequency modulation, conversely, produces a low-frequency audio signal.

Since this interference is therefore an inversion of the adjacent-channel modulation, it appears as an unintelligible mixture, commonly termed "monkey chatter." Receiver selectivity discriminates against this type of interference. It is also limited by proper restriction of the high-frequency audio response. The selectivity ahead of the second detector is, of course, the principal factor in preventing response to the adjacent-channel signal modulation.

Most limited-fidelity receivers automatically suppress the 10,000-cycle beat from adjacent carriers because of their high degree of selectivity, or by the customary design of their audio amplifier or loudspeaker to have sufficiently limited upper-audio frequency response to prevent reproduction of such a high-frequency note. In "high-fidelity" receivers the situation is somewhat different. If the high-fidelity receiver is designed to cover an audio range up to say 7,500 cycles, a *total* band of frequencies 15,000 cycles wide must be passed by the i.f. amplifier. Under these conditions, the i.f. tuning must be so broad that it is almost a certainty that a filter will be required *after* the i.f. amplifier to eliminate the 10-kc. beat note caused by interference by carriers on adjacent channels, since the i.f. amplifier will not discriminate against these carriers enough to suppress them sufficiently when the full high-fidelity i.f. band width is employed. Therefore, the 10-kc. beat note must be prevented from reaching the loudspeaker. This is commonly accomplished by means of a suitable low-pass audio filter which cuts off sharply at around

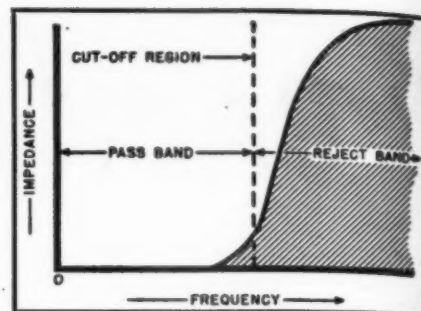


Fig. 6. Frequency-response characteristic of the audio filter circuit shown in Fig. 4. Note that it is a low-pass filter, passing all frequencies up to cutoff and offering a much higher impedance to all frequencies above this value.

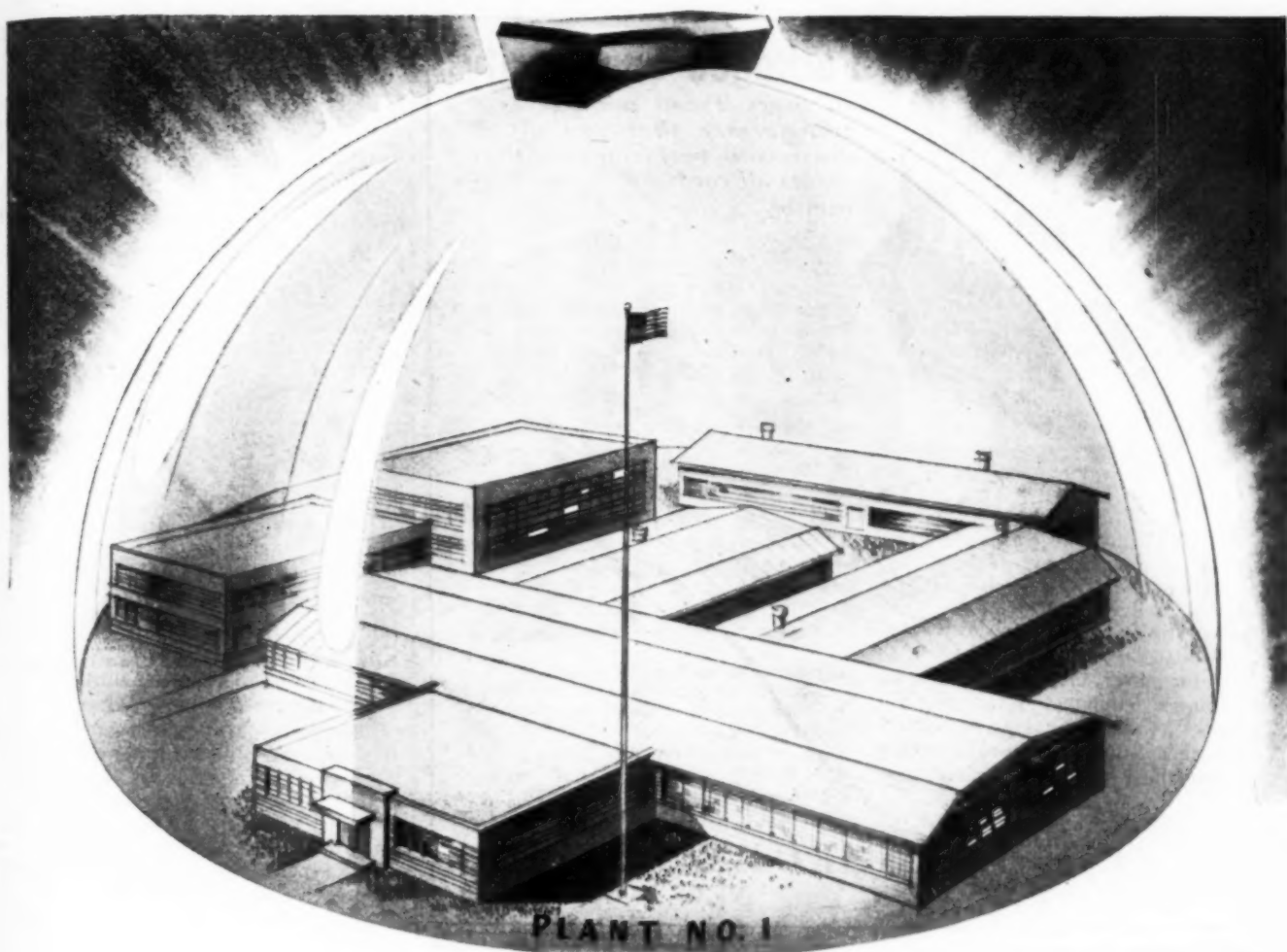
7,500 or 8,000 cycles. This filter is located in the audio amplifier.

The details of such a filter arrangement, as used in the Philco 200-Series high-fidelity receivers, are shown in Fig. 4. The filter consists of an anti-resonant circuit composed of *L* and *C* (resonant at 10-kc.) connected in series with the circuit between the 75 second detector and the 42 driver tube. Two condensers *C*₁ and *C*₂ act as shunt arms. Since the filter works out of the plate circuit of the 75 second-detector tube, it is terminated in a resistor *R*₁ and a low impedance audio frequency bypass condenser *C*₃. The frequency characteristic of a filter of this type is essentially as shown in Fig. 6. It presents a very-low impedance to the passage of all currents up to the cutoff frequency (about 7,500 cycles in this case). At this frequency the response cuts off sharply so that all currents of higher frequency than this meet with a high opposition and are greatly attenuated. In this way, the 10-kc. beat note from interfering adjacent-channel stations is effectively prevented from getting through the audio amplifier and reaching the loudspeaker. This particular filter has a discrimination of about 25 db. at 10-kc. The condenser *C* is made adjustable to allow for the various conditions of interference that might arise from adjacent-channel stations in different localities.

Another very effective method of accomplishing the same end is through the use of a tertiary circuit, consisting of a parallel-tuned coil associated with the loudspeaker matching transformer. This coil is tuned to a frequency slightly below 10,000 cycles and gives a sharply defined attenuation and cutoff of the higher audio frequencies.

High-fidelity receivers usually contain a control for the high-frequency end of the audio band, and also a control for reduction of selectivity, which makes possible two degrees of fidelity. Where interference from an adjacent channel beat note exists, this control may be reduced to effect its elimination.

When "monkey-chatter" is encountered in an existing receiver, there are two methods of treatment:



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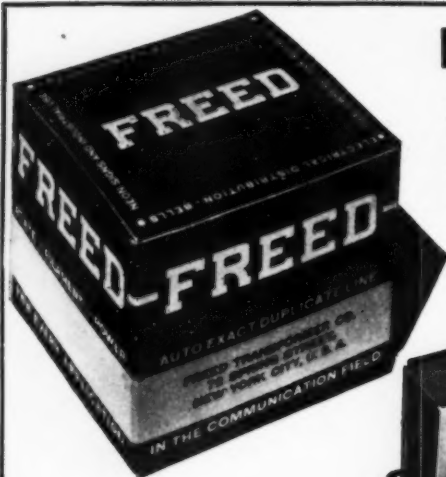
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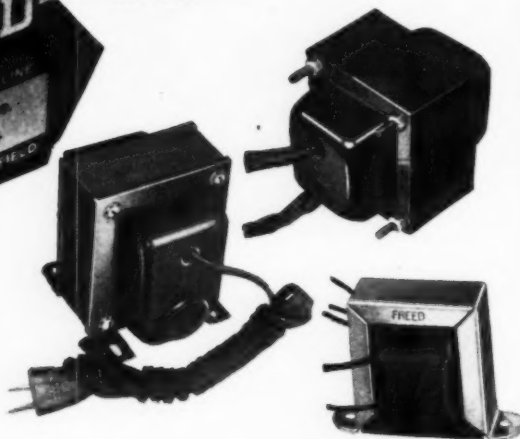
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- (1) Suppression of the adjacent-channel interfering signal either by precisely aligning the receiver to make it more selective, or by adding a sharply-tuned wave trap (or pair of them) to the antenna circuit.
- (2) Reducing the high-frequency response of the audio system of the receiver.

In general, "monkey-chatter" interference will be more prevalent at more points on the tuning scale in localities where the number of popular stations is limited, and where such stations are at relatively great distances.

Overmodulation of the adjacent channel station accentuates the interference due to "monkey-chatter" because of the higher frequency sidebands which are generated by such overmodulation. Overmodulation however, is an unusual condition and usually should not be suspected as the most likely cause for this type of interference.

Summary of Reasons for Including a T.R.F. Amplifier in the Superheterodyne Receiver

The principal purpose of including the t.r.f. amplifier in a superheterodyne receiver is mainly to provide sufficient selectivity ahead of the mixer to effectively preselect the desired signal and suppress "image" and several other types of interfering frequencies before they reach the mixer. The r.f. amplifier is *not* used primarily to obtain adjacent-channel selectivity, for the i.f. amplifier provides most of that. Its main function is to prevent signals 20 or more kilocycles removed from the desired signal frequency from causing the various types of spurious interferences we recently have been studying.

It also serves to isolate the local-oscillator circuits from the antenna circuit, thereby reducing interference caused by oscillator radiation. A single high-gain stage of sharply-tuned t.r.f. amplification is generally sufficient for these purposes. The selectivity and sensitivity of the superheterodyne can be increased greatly, however, by the use of two stages of t.r.f. amplification when it is permissible, and at the same time the signal-to-noise ratio is appreciably increased thereby. The mixer or frequency-converter stage usually introduces more noise than an r.f. stage of amplification. This noise is amplified, together with the desired signal, by the i.f. amplifier; therefore, if the signal strength is increased *before* mixing, less amplification is required in the i.f. amplifier and a greater signal-to-noise ratio is obtained. Since there also is some noise inherent in the r.f. amplifier, the amount of amplification before mixing will be limited by the noise present in the first r.f. stage.

Super-control r.f. pentode type tubes are used in the r.f. stages of practically all modern superheterodynes, as such tubes ordinarily are not subject to cross-modulation effects, do not re-



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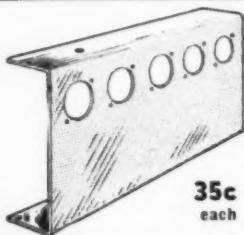


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The performance of a superheterodyne receiver is in a large measure dependent upon the design of its r.f. and i.f. stages. If the r.f. stages do not provide the necessary preselection and off-channel selectivity, at least some of the many types of spurious interfering responses that we have studied in the preceding few lessons will occur and hopelessly spoil the reception.

(To be continued)

The Television Channel

(Continued from page 46)

shown on the figure (vertical sweep). Consequently, each horizontal line begins slightly below the previous one, the beam gradually making horizontal traces down the screen under the pull of the much slower moving vertical sweep. We also can notice from Fig. 3 that the vertical seems to have more pull during the horizontal trace than during the retrace. This is accountable because the horizontal trace is slower than the retrace.

Interlaced Scanning

The scanning of the horizontal lines is not performed in sequence (1, 2, 3, etc.) but instead the odd-numbered lines are scanned first (1, 3, 5, 7, etc.) and then the beam returns and scans the even-numbered lines (2, 4, 6, 8, etc.). This method is called interlaced scanning and is shown in Fig. 6. Scanning begins at line number 1 at the top left of the screen, or scanning raster, and proceeds to the right; at this point, the beam retraces to the left and begins scanning the third line. The scanning cycle continues until the beam reaches the lower right-hand corner of the raster. Here the vertical retrace returns the beam to the top center of the scanning raster and the scanning of the even-numbered lines begins. When the last line is scanned, ending at the bottom center of the scanning raster, the beam is returned to the top left and initiates the start of a new frame. Each frame or one complete picture consists of 525 lines and to simulate motion 30 frames or complete pictures are scanned each second. However, because of the interlaced sys-

tem there are 60 vertical sweep cycles or fields per second as first the odd-numbered lines and then the even-numbered lines are scanned. Since each frame or picture is constructed of both odd-numbered and even-numbered lines each frame consists of two fields.

Although each frame consists of 525 horizontal lines only approximately 485 of these lines actually carry picture or video signal; the remainder of the horizontal lines are lost during the vertical retrace intervals (there are two vertical retrace intervals for each frame—one between fields the other between frames). The vertical retrace interval lasts for approximately 1250 microseconds twice each frame, and consumes approximately 40 horizontal lines. Thus, the beam is not returned directly from bottom to top, as shown in Fig. 6, but returns over a path similar to that shown in Fig. 2—there being quite a number of horizontal sweeps during the vertical retrace.

It is evident a considerable amount of time is consumed in retracing the beam, and for these intervals no picture information is transmitted. Furthermore, it is necessary to blank out or cut off the electron beam during these intervals to prevent visible retrace lines from streaking across the picture on the screen. In fact the only time the electron gun emits a strong beam and the only time useful picture information is transmitted is during the traces from left to right of the 485 active lines. During the retrace intervals, both horizontal and vertical, the electron gun cuts off the beam and no picture information is conveyed from transmitter to receiver.

Construction of Television Signal

Three types of information are transmitted on the picture carrier: (1) picture or video signal, a progressive series of electrical impulses which represent the relative light values of the object televised; (2) sync, a series of rectangular pulses which keep the cathode-ray beams at transmitter and receiver in synchronism; and (3) blanking, a series of rectangular pulses, which blank or blackout the fluorescent screen during all retrace intervals.

(1) The video signal is formed when

Table 1. Technical data on the first three television channels.

Chan- nel	Low- Freq. End of Chan- nel	Guard Band	Flat Portion Low- Freq. Sideband	Picture Carrier Fre- quency	Flat Portion High- Freq. Sideband	Guard Band	Sound Carrier Fre- quency	High- Freq.- End of Chan- nel
1	50 MC	50 to 50.5	50.5-51.25	51.25	51.25-55.25	55.25-55.75	55.75	56
2	60	60 to 60.5	60.5-61.25	61.25	61.25-65.25	65.25-65.75	65.75	66
3	66	66 to 66.5	66.5-67.25	67.25	67.25-71.25	71.25-71.75	71.75	72

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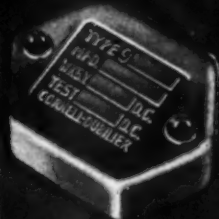
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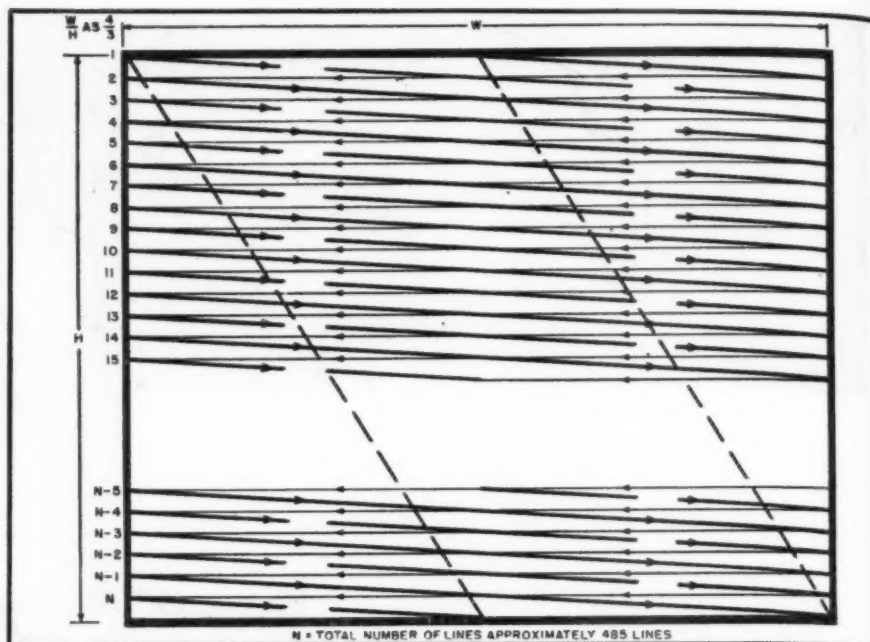


Fig. 6. Procedure of scanning the horizontal lines. The odd-numbered lines, that is, 1, 3, 5, etc., are scanned first and then the beam returns and scans the even-numbered lines, that is, 2, 4, 6, etc. This method is termed interlaced scanning.

the electron beam of the pickup tube moves from left to right across the mosaic, releasing electrical charges in accordance with the intensity of the light focused on the various points scanned. One complete frame or picture is transmitted in $1/30$ th of a second and one complete line is transmitted in 53 microseconds. Now let us assume a dark black spot on the mosaic represents peak signal amplitude and an intense bright spot, minimum signal amplitude. Thus, a gradual change in light intensity from white to black and back again to white as the beam scans one horizontal line, can be assumed to represent one cycle. Since one horizontal scan from left to right occurs in 53 microseconds the base frequency of this one cycle is $1/53 \times 10^{-6}$ or 18,870 cycles per second. What is meant is that a frequency response of 18,870 cycles would be required to pass this very gradual change in light value, at the high velocity with which the beam scans. However, a very much greater response is necessary to make a more abrupt change from light to dark or dark to light. It is possible to have a change from white to black and back to white occur in .025 inches in the case of a thin black vertical line on a five-inch screen. For the five-inch tube the beam travels the horizontal trace in 53 microseconds and, therefore, travels one inch in 10.6 microseconds, and the number of microseconds required to travel .025 inches is, consequently, $.025 \times 10.6$ or .265 microseconds. Thus one cycle which occurs in .265 microseconds is equivalent to a base frequency of $1/.265 \times 10^{-6}$ or 3.77 megacycles per second. It is apparent from the above figure how necessary it is to use wide-band amplifiers and broad channels, to convey a picture with clarity and definition from transmitter to receiver.

The video signal and its position in the composite signal is shown in Fig. 4 and again in Fig. 5. In conclusion the video signal is transmitted point-after-point and line-by-line and is only interrupted for the horizontal and vertical blanking (retrace) intervals.

(2) The horizontal sync pulses, of which there are 525 each frame, keep the horizontal motion of the receiving tube scanning beam in synchronism (or "in sync") with the same motion of the pickup tube beam. Therefore, at any one instant, the two beams are striking their respective scanning rasters at the same relative position. These "sync pulses," thus, hold the picture stationary horizontally (prevent tearing out). A typical sync pulse, as shown in Fig. 4A, has a duration of approximately 5.08 microseconds, and initiates the horizontal retrace at the receiver by regulating the generation of the horizontal sawtooth sweep. For a short interval before the transmission of the sync pulse a blanking pulse is transmitted, Fig. 4B, which immediately blacks out the screen. This blanking signal continues for an interval after the sync pulse, permitting sufficient time for the beam to return to the left side of the screen before the screen is unblanked—the total blanking interval has a duration of 10.16 microseconds.

The actual television signal which appears on the control grid of the picture tube, as shown in Fig. 4C, has a negative polarity—that is, the more signal amplitude applied the further negative the grid is driven and the darker the fluorescent screen becomes. Consequently, when the picture signal is at minimum value the screen is brilliantly illuminated and when it reaches a maximum value there is a dark spot on the screen. After the completion of one horizontal line the grid is driven

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to cutoff by the blanking signal (point a) and the screen is blacked-out. A short time later the horizontal sync pulse is transmitted—the sync pulse swings the grid further negative (called the blacker than black region) still holding the screen blacked-out. The blanking signal continues for a short interval after the sync pulse, still holding the screen blacked-out and allowing the beam to retrace. At point b, the blanking signal is removed, the screen is unblanked, and a new horizontal line begins. Drawing (c) shows two horizontal lines and corresponding horizontal blanking intervals.

(3) The vertical sync pulse intervals, of which there are two each frame (interlaced scanning system), keep the vertical motion of the receiving picture tube scanning beam in sync with the same motion of the pickup tube beam. These vertical sync pulses hold the picture stationary vertically (prevents turning over). A typical vertical sync pulse, as shown in Fig. 7A, has a duration of 27.3 microseconds—actually, Fig. 7C, the vertical sync pulse interval consists of six 27.3 microsecond pulses. The brief interruption of the vertical pulses prevents the horizontal from losing synchronism during the vertical blanking intervals. Here again the vertical blanking drives the control grid of the picture tube to cutoff, blanking out the screen. During the vertical interval, and before and after the vertical sync pulse interval a series of short duration equalizing pulses are transmitted which equalize the vertical retrace intervals between frames and between fields (interlaced scanning system).

Television Facts and Figures

6 megacycle channel
525 lines—485 active lines and 40 inactive lines
interlaced scanning — 30 frames per second or 60 fields per second
15,750 lines per 30 frames
one frame—33,334 microseconds
one field—16,667 microseconds
one horizontal sweep cycle—63.5 microseconds
horizontal retrace or horizontal blanking interval—10.16 microseconds
horizontal trace—53.34 microseconds
horizontal sync pulse—5.08 microseconds

vertical blanking interval—1250 microseconds
vertical sync pulse interval—190.5 microseconds
vertical sync pulse—27.3 microseconds
equalizing pulse—2.54 microseconds
4 to 3 aspect ratio

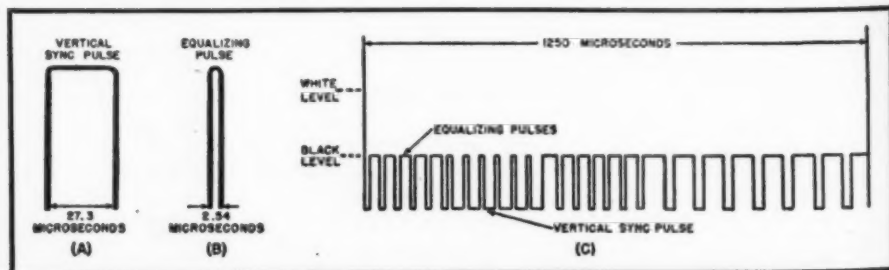
Summation

The contents of this article has covered in considerable detail the facts and figures on the standard television signal. It is difficult to understand and remember all the detailed information; consequently, a large portion of the most pertinent material is presented in chart form and to assist in retaining the signal construction detail. A step-by-step analysis of the standard signal is presented in connection with Fig. 5. As the various subjects are discussed individually in future installments the actual detail will become firmly established and no longer a process of memory. Until such time this installment should be held as a reference to which future installments will occasionally refer.

Refer to the Federal Communications Commission standard television signal (Fig. 5) and follow the signal sequence from the start of one frame to the start of the next.

1. Start of picture signal at top left hand corner of raster.
2. Picture or video signal for one line.
3. Horizontal blanking pulse at completion of first line. Blanks out screen to make retrace invisible.
4. Horizontal sync pulse which initiates the beam retrace—controls horizontal sweep circuits.
5. Horizontal blanking continues, to allow sufficient time for the beam to retrace.
6. Second line of video signal begins—actually this is No. 3 scanning line because of interlaced scanning system.
7. All the odd-numbered scanning lines are covered—consecutive odd-numbered lines interrupted by the horizontal blanking intervals.
8. Odd-numbered line scanning completed at bottom right hand corner of scanning raster. Only a few of the horizontal lines are shown on the drawings.
9. Vertical blanking pulse at completion of first field. Blanks out screen to make retrace invisible.

Fig. 7. (A) The vertical synchronizing pulse which holds the picture stationary, preventing turning over. (B) Transmitted pulse which equalizes the vertical retrace intervals between frames and between fields. (C) A succession of vertical synchronizing and equalizing pulses as they occur.





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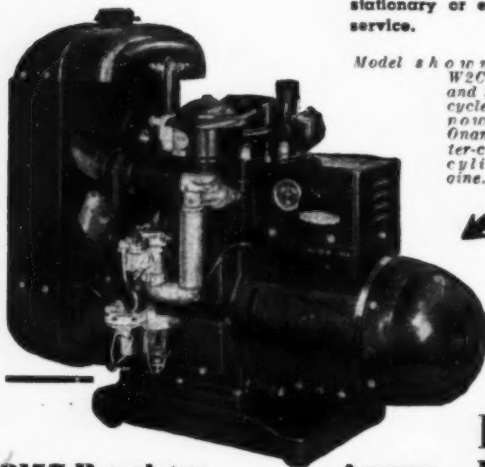
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10. A series of six equalizing pulses.
11. Vertical sync pulse interval which initiates the beam retrace—controls vertical sweep circuits.
12. Series of six more equalizing pulses and continuation of blanking to allow sufficient time for beam retrace.
13. Horizontal pulses continue throughout vertical blanking interval to prevent loss of horizontal control during the vertical retrace.
14. Retrace returns beam from lower right-hand corner to top center of scanning raster.
15. Start of even-numbered scanning (second field) at top center of scanning raster.
16. First horizontal blanking interval of second field.
17. Even-numbered lines are scanned until picture information for the frame is completed at lower center of scanning raster.
18. Vertical retrace between frames begins.
19. Beam has returned from bottom center to top right of scanning raster, completing one frame.
20. Start of first scanning line of next frame.

-30-

Wacs at Work (Continued from page 35)

sages throughout the teletypewriter-operated wire, cable, and radio networks without the necessity of manual retransmission. Wacs become proficient in the operation of all the apparatus used in the relay system.

Security of military communications is of first importance. The Wacs must be alert at all times to prevent valuable information from falling into the hands of the enemy. They must recognize messages which require censorship, and must see that the messages are censored.

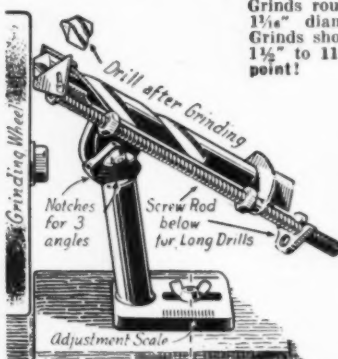
Work done by the Wacs has assumed additional importance with the integration of the Army Communications Service's domestic wire and overseas radio networks into a flexible, uniform world-wide system.

Although many of them are new to their assignments, the Signal Center Wacs are doing an outstanding communications job. Brigadier General Frank E. Stoner, Chief, Army Communications Service, Office of the Chief Signal Officer, has this to say:

"Members of the Women's Army Corps are performing vital tasks in the War Department Signal Center, hub of the United States' world-wide communications system, where security, accuracy, and speed are of paramount importance. We have found the Wacs conscientious, efficient, and dependable in handling the messages of war. They have proved that they are thoroughly capable of filling many positions which formerly required trained men who thus have been released for service in the Theaters of Operations."

-30-

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The rig he left behind is due for a big change when GI Joe comes home. War experience has been an "eye opener" for him. From chassis to sky wire many pre-war Ham outfits will undergo a major alteration and amazing technical advances will be put into practice. Stimulated by training and experience gained in the armed services thousands of new enthusiasts will swell the ranks of amateur radio.

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CQ'ing, SS or DX; UNITED will be ready to serve the Amateur with war-perfected Transmitting Tubes.

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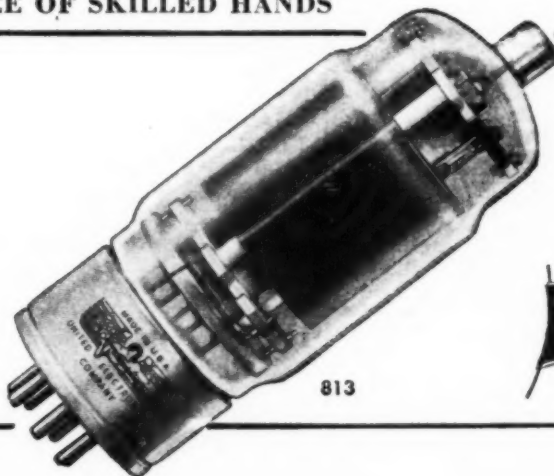
ELECTRONICS COMPANY

NEWARK, 2



NEW JERSEY

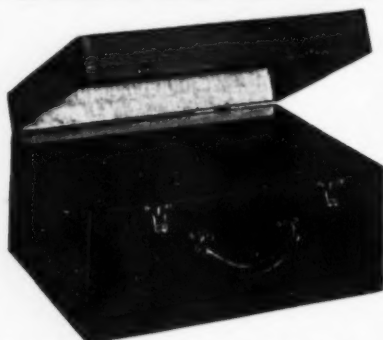
Transmitting Tubes EXCLUSIVELY Since 1934



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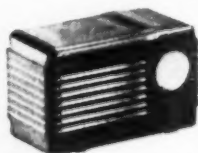
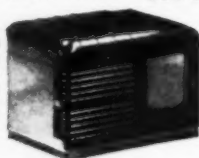
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Portable Phonograph case, of sturdy durable plywood, in handsome brown leatherette finish. Inside dimensions 16 1/4" long, 14" wide, 9 1/2" high. Has blank motor board. As illustrated \$6.95 above, specially priced at.....

Replacement cabinet in dark walnut finish plastic. Inside dimensions 10L x 6 1/2H x 6D. Price.....

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Dark walnut finish plastic cabinet to accommodate practically any Tiny Tim radio. Size 7 1/2L x 4 1/2H x 4D. Price.....

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Cabinets available in ivory color and Swedish Modern. Write for prices.

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4, 5, or 6 Tube—6.3V at 2 amp. 50 mill Power Transformer.....

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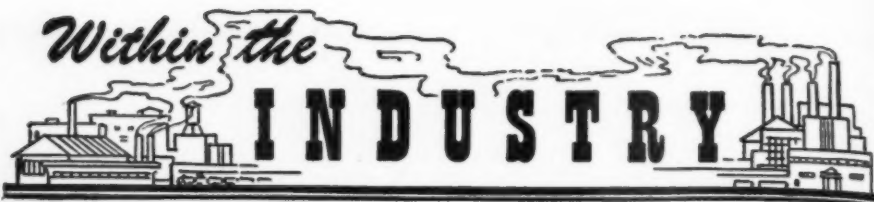
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NORMAN L. CANNON, president of Cannon Electrical Supply Company of Charleston, South Carolina, is the new Stromberg-Carlson distributor for that area according to the announcement made by C. J. Hunt, manager of radio sales for the company. This appointment is one of several made recently. At the same time, Mr. Hunt announced the return of Mr. E. S. Germain, pre-war sales manager of the Pacific Coast division, who has been on a leave of absence from this post with the company's government subcontract sales division.



The Adair Appliance Company of Memphis has been appointed exclusive area distributor of the company's postwar radio, FM, and television lines.

NATIONAL UNION CORPORATION, manufacturers of cathode-ray and electronic tubes has appointed Ejnar O. Sandstrom as controller of the corporation.

Mr. Sandstrom joined the company organization as an auditor in 1930. In addition to his duties as controller, Mr. Sandstrom will continue to serve as secretary to the company, a post which he has held since 1941.

ROBERT N. BAGGS is the new manager of the Merchandising Division of International Resistance Company according to the announcement made by Harry A. Ehle, IRC's vice-president and General Sales-manager. Mr. Baggs comes to IRC from RCA and brings 14 years' experience in the radio field with him to his new post. He is well known in the jobbing field and has a long experience in the merchandising field.



GALVIN MANUFACTURING CORPORATION, through its president, Paul V. Galvin, has announced the appointment of two new vice-presidents: Elmer H. Wavering, who will be in charge of the new Automotive Division and Walter H. Stellner, vice-president in charge of the new Home Products Division.

Mr. Wavering joined the Motorola organization as an engineer in 1930 and pioneered the design and engineering development of the first commercial car radio receiver during that

year. Later, Mr. Wavering became Sales Manager of the Car Radio Division, a position which he relinquished to become head of the Quartz Crystal Division.

Mr. Stellner joined the company in 1937 as Advertising Manager for the Home Radio Division. A year later he was promoted to the post of Sales Manager of this division. In 1942 he became head of the Washington Office of the Galvin Company.

R. S. CHAPMAN, of the firm of Chapman and Wilhelm, has predicted a

vast increase in the use of electronic equipment in the southern states after the war. His prediction was made recently when his company was appointed exclusive distributor for the Stromberg-Carlson postwar radio, FM, and television sets, for North and South Carolina. The area served by the firm, whose headquarters are in Charlotte, includes Durham, Greensboro, Winston-Salem, Asheville, and nearby areas. The higher standard of living made possible by wartime wages will provide an excellent postwar market in this area, according to Mr. Chapman.



HARRISON RADIO CORPORATION of New York has announced the appointment of Irving Phillips Wolfe to the post of Advertising and Assistant Sales Manager, through its president William E. Harrison.

Mr. Wolfe has been active in the advertising and sales promotion fields for over 15 years. He is a former Signal Corps and Air Corps instructor and a veteran of World War II. He is an old-time "ham" having been licensed as 2APJ since the early part of 1920.

Harrison Radio Corporation is a distributor and wholesaler of radio and electronic equipment to industrial firms, laboratories, amateurs, and radio servicemen.

WALTER E. PEEK has been named to the post of sales manager of the Electronic Laboratories, Inc. of Indianapolis, according to the announcement made recently by Mr. Norman L. Kevers, president of the company. Mr. Peek has been a member of the engineering staff of the company for the past



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.001 mfd 600v	12¢	.006 mfd	12¢
.002 mfd 600v	12¢	.01 mfd	12¢
.003 mfd 600v	12¢	.02 mfd	12¢
.004 mfd 600v	12¢	.05 mfd	13¢
.005 mfd 600v	12¢	.1 mfd	18¢

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.01 mfd	.08	.70	6.00
.02 mfd	.08	.70	6.00
.05 mfd	.10	.80	7.00
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BX	Crystal	7'	\$9.95	\$5.85
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BD	Dynamic	7'	14.50	8.53
33D	Dynamic	20'	23.50	13.82



PM SPEAKERS

5" Round	1.25
6" Round 3.6 oz.	2.10
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Each	135-160-180-220-250-290 OHM	4.30
ICA Universal 22-330 ohm		73¢
560 ohm for 3-way Portable		73¢

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20% deposit required on all C. O. D. orders. Orders of \$25.00 or more accompanied by payment in full, will be shipped prepaid. DON'T FORGET L-265 or AA-3 certificate.

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four years, serving both as a design and sales engineer, specializing in the vibrator field. In his new capacity, Mr. Peek will be in charge of sales for all of the products manufactured by Electronic Laboratories, Inc.

ROYAL J. HIGGINS has been appointed representative for The Turner Company of Cedar Rapids, Iowa. He will assist purchasers of the Turner line of microphones in the Greater Chicago area. Mr. Higgins is well known in the radio industry as he has been an active "ham" since 1923 and maintains his own station, W9A10. He was formerly employed by Sears Roebuck and Company and Hallicrafters. His offices in Chicago are located at 600 South Michigan Avenue.



EMERSON RADIO AND PHONOGRAPH CORPORATION has announced the appointment of two new distributors for the company's line of radio and television sets.

The Sunset Electric Company of Spokane, Washington, will act as distributor for the Spokane area. Mr. R. M. Spiger is the manager of this branch of the company and J. H. Johnson is the radio salesman.

The Capitol Distributing Company of Providence, Rhode Island, is the second distributor to be granted the Emerson franchise. This newly organized wholesaling firm is headed by Morrie and Roy Rosenfeld who have been connected with the Emerson organization for many years. Active management of the Emerson line will be under the direction of Mr. Roy Rosenfeld.

E. GUY FLAIG has been elected to the post of president of the radio division of the Cincinnati Electrical Association. Mr. Flaig has held various positions in the appliance field, including sales manager for RCA and branch and regional manager of the Crosley Corporation. At the present time, he is the manager of the appliance division of the Bimel Company of Cincinnati, distributors of Admiral radios and home appliances.



RADIO CORPORATION OF AMERICA has announced the appointment of Chester C. Aiken to the staff of the Electronic Apparatus Section of the RCA Victor Division in Camden, New Jersey.

Mr. Aiken has been associated with the field engineering training and personnel division of RCA since 1928. In his new post Mr. Aiken assumes commercial responsibilities for electronic

equipment now under experimental development for quality control and inspection of liquids.

Mr. Aiken entered the RCA organization in 1928 as the head of a staff charged with training field engineers in the service division of RCA Telephone, Inc. In 1936 he organized the executive training program to recruit outstanding college graduates and supervised their training and initial experience. In 1943 he was appointed to RCA's national Personnel Administration staff, in charge of recruiting technical and specialized personnel.

THE HALLICTRAFTERS COMPANY of Chicago has announced the appointment of Charles Knoblauch to the post of superintendent of the firm's Clearing Plant.

Mr. Knoblauch, who was formerly assistant superintendent of Hallicrafters' 26th Street Plant, has been with the company more than six years. His experience includes over seventeen years in the radio production field.

DAVID M. SALISBURY is the new vice-president and general manager of the Westinghouse Electric Supply Company, according to the announcement made by B. W. Clark, president of the organization. In his new position, Mr. Salisbury will head the company's operations. The supply company is the wholesale outlet for the appliances manufactured by the parent company, Westinghouse Electric and Mfg. Co.



FEDERAL TELEPHONE AND RADIO CORPORATION has announced the appointment of Frank O. Zimmerman of Oak Park, Illinois as assistant manager of the Chicago Sales branch of the company.

Mr. Zimmerman formerly was employed by the Westinghouse Electric Elevator Company at Chicago and Indianapolis. He is a graduate of the Illinois Institute of Technology in electrical engineering.

BURLINGAME ASSOCIATES has organized a new Instrument Repair section under the direction of William E. Adams.

Because many test instruments badly needed for war production and essential civilian use are out of commission due to lack of repair facilities by the manufacturer or the shortage of small parts, the company feels that the new service will be of value to many persons.

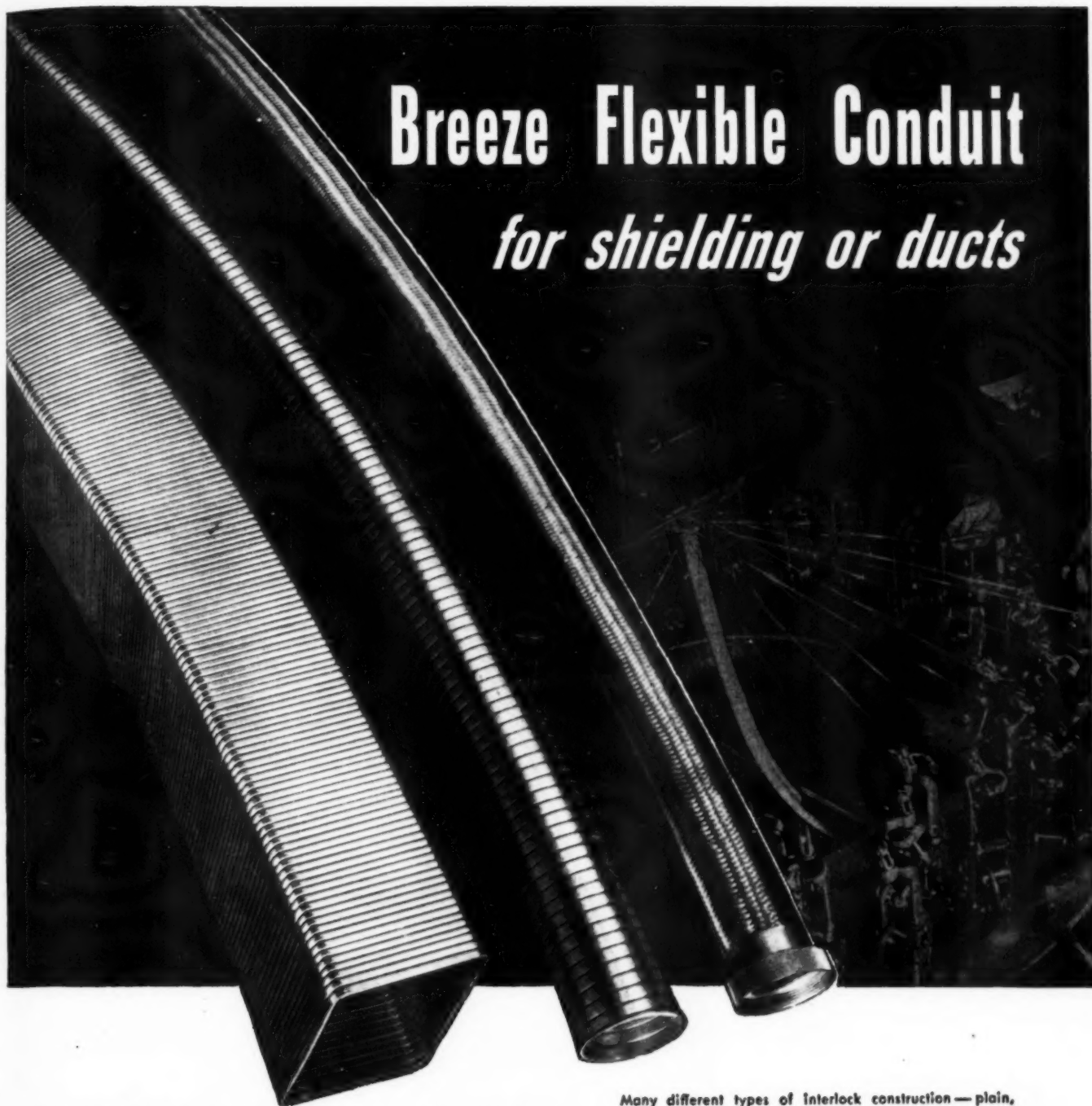
The company has requested that persons having instruments to be repaired write to the company first giving the make of the instrument and other pertinent data before shipping the instrument in for repairs.

The company is located at 11 Park Place, New York, New York.

-30-

Breeze Flexible Conduit

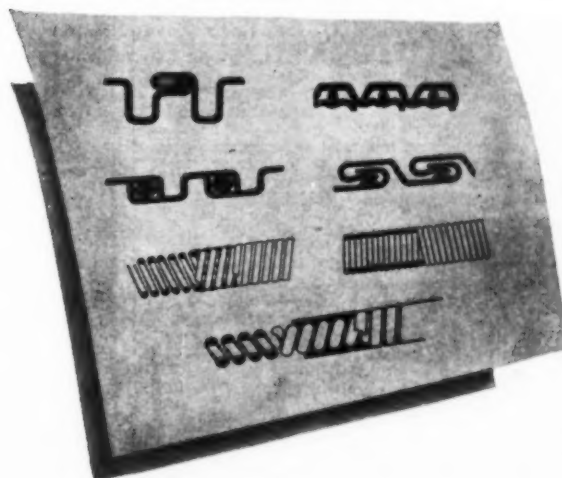
for shielding or ducts



Breeze Flexible Tubing, manufactured in many diameters from a wide variety of metals, is used as ventilation and exhaust ducting in industrial, aircraft, marine and automotive applications. The same basic tubing, with the addition of a braided metal covering, becomes light-weight shielding conduit, used extensively for shielding ignition systems and any electrical circuit to insure dependable radio communication.

Manufactured from a continuous strip of metal, Breeze Flexible Tubing and Conduit can be furnished cut to length, with necessary end-fittings for any conduit installation.

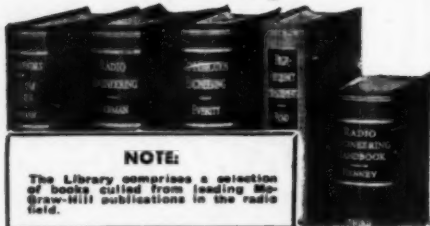
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Feature this
new tool in
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WRITE FOR
DETAILS!

Electrical Gunsight (Continued from page 34)

amount of leeway in the adaptation of this sight to various turrets.

Of the various factors involved, range, as has been said, is derived from the sight head's reticle and is set into the computer unit by the foot control assembly. Indicated air speed and altitude are set in manually by means of controls located on the computer unit. They do not have to be put in automatically since they do not vary appreciably during combat. Wing span of the target also is set in manually.

Azimuth gun elevation is supplied by an attenuator driven by means of flexible shafts connected to the turret gearing.

The angular velocity of the target is indicated by specially designed d.c. generators connected to the turret and gun elevation drive. These generators are similar to electrical tachometers, but instead of the usual permanent magnet fields used in such devices, they have wound fields and use laminations with extremely small hysteresis loss loops to maintain the linearity of output within 1%. This is necessary because the linear relationship computation involves multiplication of angular velocity in either direction, as indicated by the shaft speed of the generator by the time of flight, indicated by the strength of the current in the field of the generators.

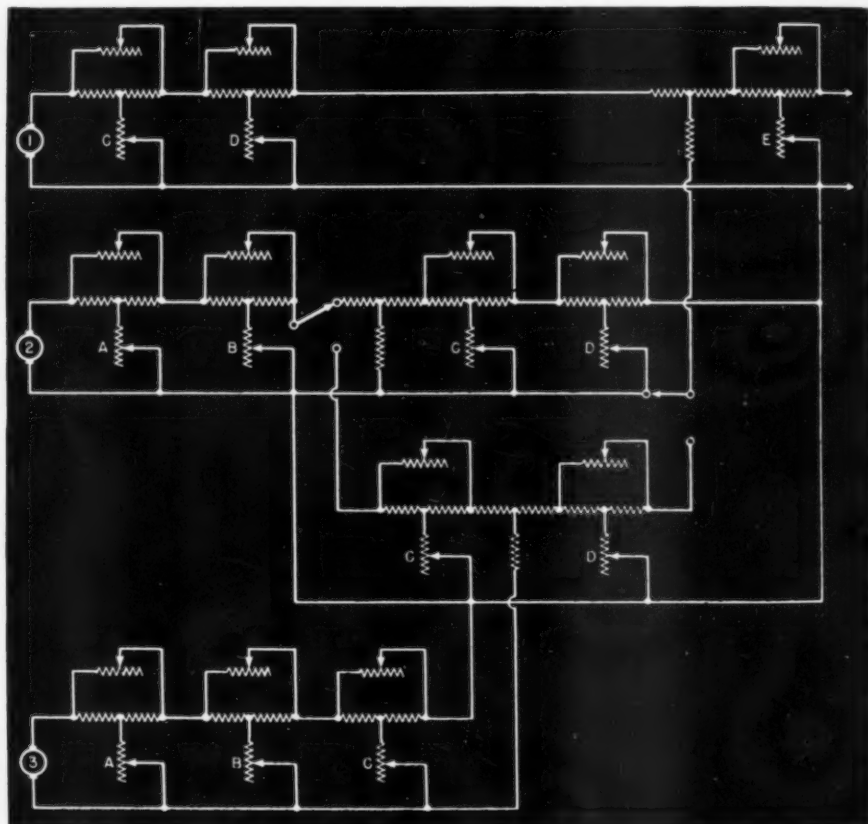
The time of flight current is ob-

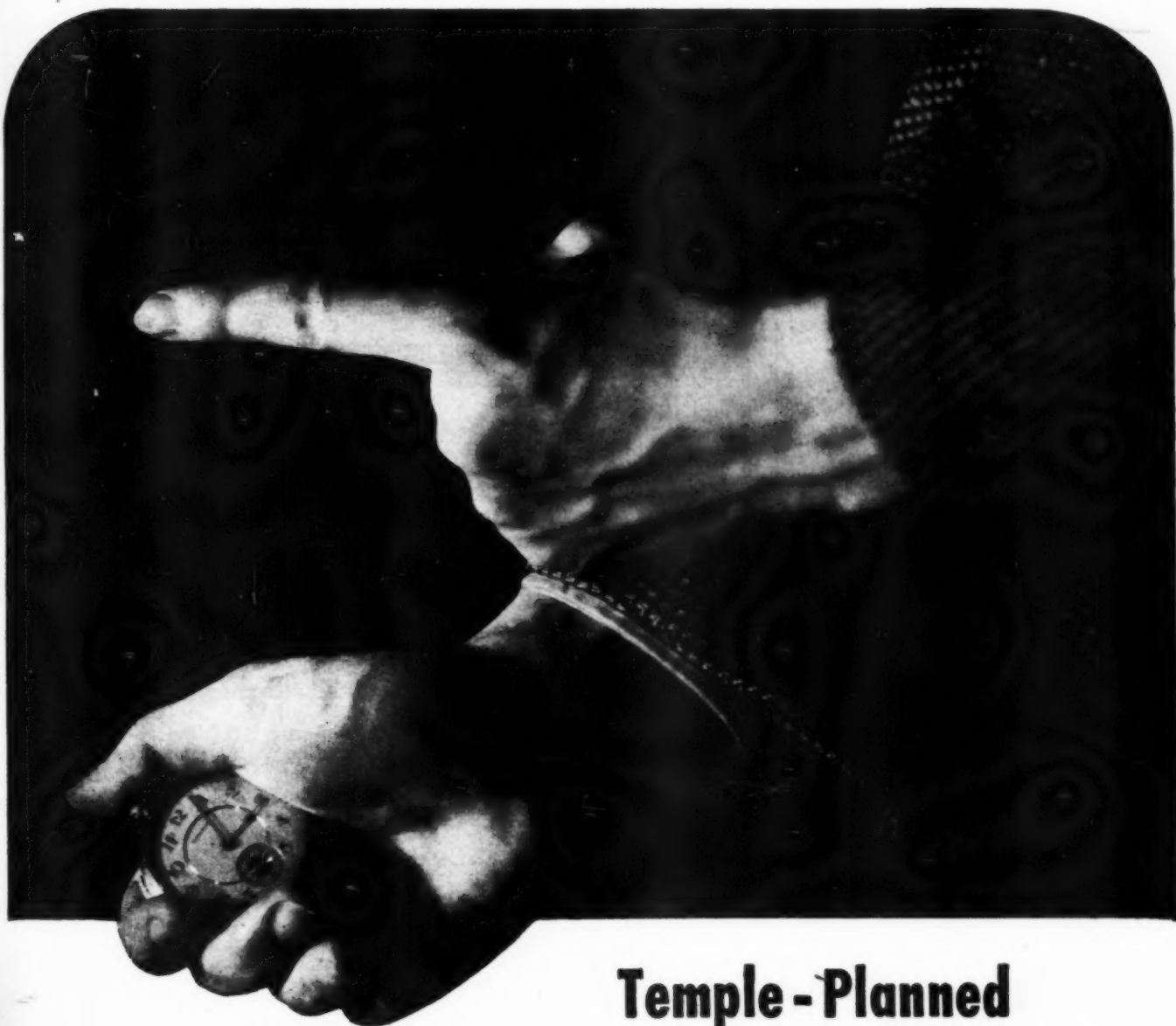
tained from an electrical attenuator network especially developed for this purpose. The attenuators themselves are basically the same as those which have been used for years in the radio industry, but they have been adapted to meet much greater accuracy requirements than previous applications have demanded. The problem of obtaining this accuracy and the special tapers required for the various attenuators was worked out in conjunction with *Clarostat*, a concern of long experience in this field. Attenuators—or T-pads, as they are known—are used in the computing network in order to maintain constant circuit impedance while the attenuation is being altered to correspond to the various factors entering into the computation.

Figs. 6 and 7 show the method of approach to the problem of designing an electrical computing network. The three sets of curves in Fig. 6 are the result of flight tests and computations both theoretical and practical. Fig. 7 represents an electrical computing network which will produce a voltage varying in accordance with these curves.

The curves show the variation of time of flight with four factors A, B, C, and D. Two conditions of C are shown, with D remaining fixed, and two conditions of D, C remaining fixed. In each group five conditions of B are illustrated. It will be seen that under the condition B₁, time of flight is affected by C and D and not by A. In Fig. 7 generator 1 supplies a voltage proportional to the time of flight corresponding to B₁ under condition

Fig. 7. General representation of the electrical computing network, which, when properly designed, will produce a voltage varying in accordance with the curves of Fig. 6.





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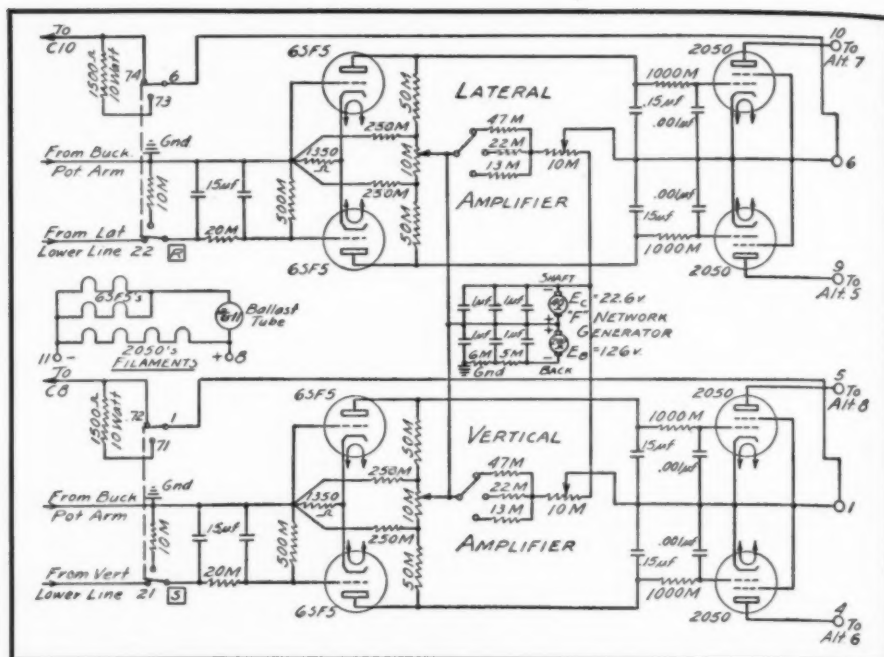
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In a similar manner it was found that the factor E affected all circuits equally. Consequently, the first auxiliary circuit is connected to the main circuit prior to the attenuator for factor E, whose current or voltage is proportional to the time of flight under all conditions of all five factors illustrated. If necessary, still further refinement could have been added by the inclusion of further auxiliary circuits.

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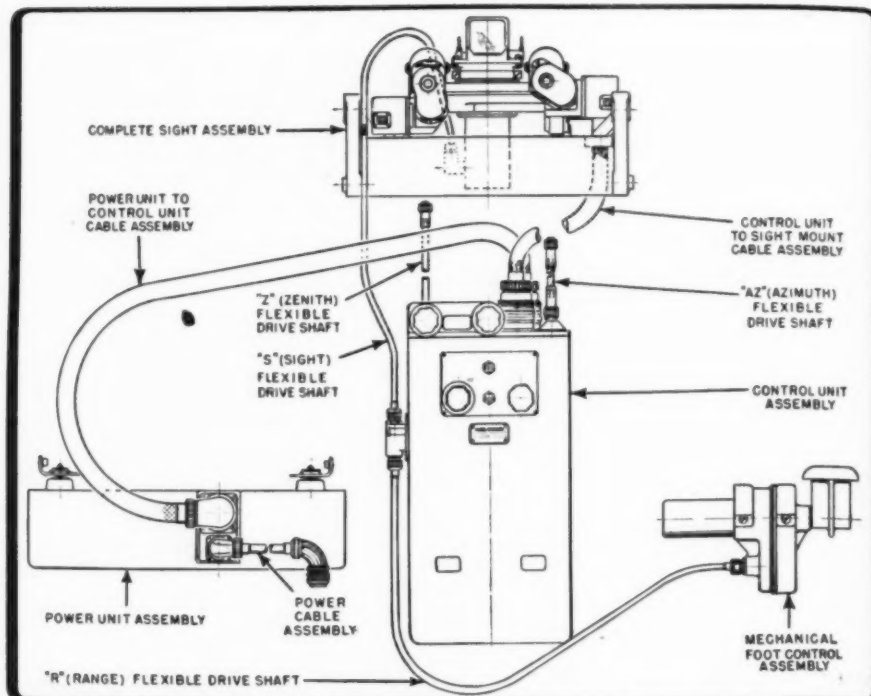


Fig. 9. Diagram of the arrangement of component parts of this electrical gunsight.

But the values obtained here for time of flight are within 0.01 of a second, which would correspond to an insignificant error of less than 1 yard at 1,000 yards for a relative speed of 200 miles an hour.

(EDITORS NOTE: Figs. 6 and 7 were included and discussed in this article to give the reader a general idea as to how an electrical network of attenuators could be designed to operate a mechanical device which automatically compensates for various variable factors, such as would be encountered in this automatic gunsight. The curves of Fig. 6 and diagram of Fig. 7 do not include or mention the actual factors involved or the values of the electrical components that finally were arrived at. More detailed information has been omitted purposely for security reasons.)

Lateral and vertical ballistic deflections are computed with circuits very similar to the one just described. The voltage from the vertical ballistic deflection circuit is added to that from the vertical relative velocity generator and the result then delivered to the computer unit. The same process takes place with the lateral ballistic voltage except that the lateral velocity generator voltage to which it is added is modified by a gun elevation attenuator. This is necessary because the azimuth relative velocity generator is driven by the rotation of the turret in the horizontal plane while the sight is offset at a variable angle to this plane.

The sight offset creates a problem which has been solved, in the K-8, by the addition, mentioned further back, of an auxiliary generator on the same shaft as the lateral offsetting motor.

Space and weight limitations in a gun turret make it more practicable to offset the sight itself rather than the guns. One complication here is that any offset of the sight tends to move it off the target and the gunner then has to rotate his turret to bring it back. This rotation causes relative

velocity which in turn brings false velocity into the system. Also the compensating rotation causes a still greater offset of the sight, resulting in an unstable system.

In the mechanical gunsight this was overcome by the introduction into the system of a fixed amount of damping, in the form of a time lag. The disadvantage here is that the fixed amount gives a satisfactory correction for only one range and one set of conditions of altitude, air speed, azimuth and gun elevation position. At short range it is much too sluggish to be of benefit and at long range it is so insufficient that the gunner has difficulty staying on the target.

The K-8's auxiliary generator gives the sight a uniform performance at all ranges. Its velocity is proportional to the rate at which the sight is offset and it receives the same time of flight current as is supplied to the fields of the velocity generators. Its output (velocity of offset) is subtracted from that of the relative velocity generator (turret velocity) and the result is true target velocity.

Servo System

The K-8's Servo System, a direct result of the great development in the art of electronics within the past few years, is what converts the voltages into the final answer in the form of mechanical action. Its principal parts are the d.c. amplifier and the alternator contained in the power supply unit. The amplifier takes the voltage from the computer and, acting as a valve or switch, passes this on through the alternator which drives the sight motors.

Fig. 8 shows a circuit of the amplifiers, two of which are used in the complete unit, one for lateral and the other for vertical deflection. It was

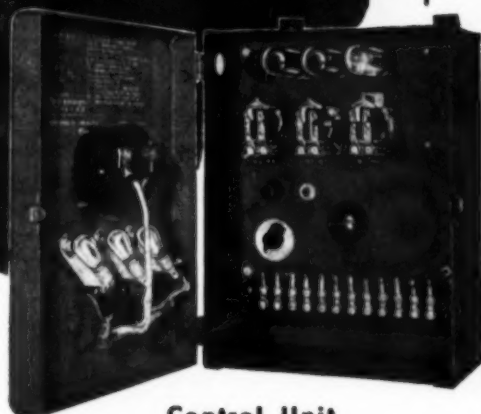
wherever a tube is used . . .



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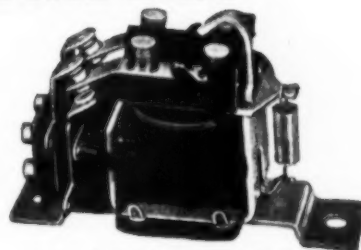
Control Unit

THERE'S A JOB FOR *Relays* BY GUARDIAN

The "Combustion Control Supervisor," made by Warner Electronic Devices of Chicago, is a photo-cell system that responds to any predetermined degree of smoke density. To avoid "false alarms" resulting from momentary puffs of smoke, it is equipped with a time delay feature.

Warner's specified that the three relays used in this system must be sensitive but not delicate; that they require no adjustment; and that they meet Underwriter's requirements.

Guardian engineers developed the Series 155 D.C. relay as the answer to these specifications. This is a compact, sturdy, easily mounted unit with constant spring tension on the contacts. It is widely used on remote selection devices and other low voltage applications. Copper slug time delays up to .05 seconds on attract and 0.15 seconds on release are available. Coils for operation on any voltage up to 230 volts D.C. For further information write for Series 155 bulletin.




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designed especially to combine great accuracy and yet be able to withstand the vibration and gun shock encountered in an aircraft turret. It has a sensitivity of 20 millivolts and performs throughout a temperature range of from 65 degrees below zero to 160 degrees above, and a humidity range of 0 to 95%. Its sensitivity is maintained at maximum by the provision of balance and bias adjustments to take care of any variation in the tubes (when, for instance, the voltage in the plane varies radically from the standard voltages). The voltage range specified is of 26 to 32 volts, and the sensitivity will remain within about 10 to 40 millivolts, which would correspond to only a 2-yard error at 1,000 yards, well within the accuracy of the gun itself.

Each offset motor (split-field series) is powered through a pair of 2050 thyratrons whose plates are connected respectively to two phase outputs of the alternator, time phased 180° apart. The sight is offset in one direction or another, depending on which of the motor's fields is energized by the firing of the associated thyatron. This, in turn, is determined by the polarity of the d.c. computed voltage on the grids of the 6SF5 voltage amplifier tubes which drive the grids of the 2050 thyratrons.

The motor's degree of rotation is controlled by the "follow-up" system. This includes two bucking potentiometers, one for each motor, supplying an opposing voltage at the input grids of the amplifier. Each of these is mechanically driven, simultaneously with the sight offset and is powered from a permanent magnet generator driven by the same drive motor as the generators supplying the computing network. Thus, network voltage and potentiometer voltage vary proportionately due to any speed changes in the drive motor and cancel out this variable. When the potentiometer is rotated by the sight motor, a bucking voltage finally is established that is equal and opposite to the computer voltage, reducing the net input signal reduced below its threshold sensitivity. The thyratrons are di-ionized and the motor stops. Variations in the speed of the motor driving the generators, as pointed out above, do not affect the computation in any way, and mechanical backlash is held to an absolute minimum by the fact that the potentiometers are driven on the same shaft which offsets the sight.

This instrument has extended the effective range of .50 cal. machine guns from 400 to 1,000 yards. A pursuit ship must now fly through six or eight hundred yards of deadly gunfire in order to press home an attack.

Although it is at present primarily a weapon of war, it has numerous peacetime possibilities. It has been the testing-ground for a number of developments—especially in the greater control of electrical and mechanical action—and the future applications of the principles and innovations it con-

tains are daily increasing in scope.

It has, for instance, helped to demonstrate that it is possible to build an electrical computing network that will follow an exact mathematical formula. This principle can be adapted to any of the numerous instances in which several variables are involved that are difficult or impossible to compute by mechanical means.

Other developments came about in conjunction with it, such as the curve-plotter and a new device for winding of precision attenuators and potentiometers. The future of these, as well as the computer itself, is seen by engineers as an active one in the postwar world.

Two Fairchild engineers, Erwin H. Hale and Irving W. Doyle, are inventors of the K-8 sight. Doyle conceived the instrument, and Hale spent the ensuing years working it out.

-30-

Electronically Yours
 (Continued from page 37)

neers: Maintenance and repair of electrical equipment, installation of equipment.

2. Operating engineers: Operation of generating and substations or other electrical equipment.

3. Laboratory engineers and assistants: Working under direction of engineers, they perform routine and experimental work.

4. Design engineers: This work covers design of specific apparatus for a specific purpose by making use of development and design information available.

5. Development engineer: Works with the research engineer and others to solve problems so that a specific job may be done. This work usually results in development information and a model which forms the basis of the product design.

6. Research engineer: Applies fundamental knowledge and principles to develop new techniques, solve new problems and point the way to new products, processes, etc. This advanced information is called upon by the development and design engineers.

Basic requirements for electrical engineers include a fundamental knowledge of mathematics, physics, chemistry, mechanics and materials. For a specific job in a specific field, a detailed knowledge of apparatus techniques and methods employed also is necessary. To progress in that field, there is no substitute for practical experience in addition to the required education. It is essential to have a college education or its equivalent to succeed in the electrical engineering profession, the experts agree.

The equivalent may be obtained by home study, extension courses at some university or college, or night schools.

Some general advice by the manufacturers to the soldier who wants to become an electrical engineer:

1. Carefully appraise your past education and experience and make up



War shortages crop up in strange materials. Mica, for instance. Once seen principally in the windows of stoves, and in small boys' pockets, it is now used extensively as electrical insulation. In some war products, it is virtually indispensable: capacitors for radio, spark-plugs for airplane engines, insulators in electronic tubes.

With demand mounting, manufacturers were desperate. A four-man

technical mission flew to London to help ration the world's supply between the United States and Great Britain. The shortage was serious.

The War Production Board, convinced that much mica was classified too low when judged by appearance alone, asked Bell Telephone Laboratories to develop a new method of electrical tests. The Laboratories were able to do this quickly and successfully

because of their basic knowledge and experience in this field.

The new tests were made available to manufacturers in this country and abroad—the supply of usable mica was increased 60% — and a difficult situation relieved.

Skill to do this and other war jobs is at hand in Bell Laboratories because, year after year, the Laboratories have been at work for the Bell System.

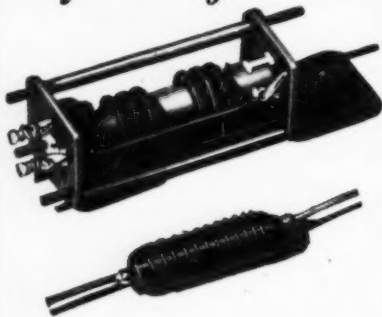
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your mind that you are capable of studying and working for the objective you desire.

2. Select the goal you expect to achieve in, say five years, and plan systematically to reach it.

3. Determine the path you will follow to reach the particular job in the particular field of electrical engineering:

A. Home study while working.

B. Extension college course while working.

C. College courses.

4. Do your best in each course or job, and remember that the extra effort will be remembered and rewarded by promotion.

—50—

International Short-Wave

(Continued from page 87)

p.m. daily; announced they were transmitting on 11.88, 7.3, 11.95, 15.23, and at 7:15 on 6.98. Back on the air at 8 p.m. on 7.3, 9.48, and 11.95 (announced). Moscow comes on the air and leaves with the statement, "Death to the German Invader." Berlin in the 16- and 25-meter bands heard with news in English, 9:30 a.m., with almost unbelievable power, beamed to Central, South, and North America. On 6.22, Berlin comes in quite strong in the evening, beamed to North America, with news every hour on the hour. (Hester, Illinois).

HCJB, Quito, Ecuador, 9.958, heard with very good signal, 6:30 a.m.-11:30 p.m. XEWW, Mexico City, 9.50, heard with good signal, daytime and evenings, mostly music. (Underwood, Rhode Island.)

Near 11.000, Station Victory 229 heard from 12:03 to 12:11 p.m. recently talking to Victory 263; Victory 229 told Victory 263 to let up on the guy rope on the antenna so he could hear him better. (Can anyone identify?) (Harris, Mass.)

CE1185, Santiago, Chile, heard at 1:35 a.m.

DJR, Berlin, 15.340, heard signing off at 12 noon.

ZFY, Georgetown, British Guiana, heard 6:45-8:45 a.m., 10:45 a.m.-12:45 p.m., and 3:15-8:15 p.m., relays BBC news at 6:45 (S-7). Signs off with Ted Lewis singing "Is Everybody Happy?" and then, "God Save the King." OFE, Lahti, Finland, 11.780, has English news at 9:15 p.m.; announces as "Radio Finlander" (S-6). OZF, Copenhagen, Denmark, 9.520, has English news at 8:30 p.m.; announces as "Radio Copenhagen." Nazi propaganda (S-4). SBT, Stockholm, Sweden, 15.155, heard with English news at 11 a.m. (S-7); address, "Radiotrons." HAT4, Budapest, Hungary, English program, 9-10 p.m., with English news at 9:30 p.m. Breman and Braman, Germany, on 15.150, heard with English news at 11:15 a.m., in parallel with Breman and Leipzig, 15.670. Leipzig and Essen, 15.800, has English news at 11:30 a.m.

The Japanese Quarter Hour with news of the Far East, is heard over DZD, 10.540, and DZB, 9.610, Berlin, around 10 p.m. (Cotter, Mass.)

AFHQ, Italy, 17.30, has been heard broadcasting press reports in English during mornings. HP5A, Panama City, 11.70, heard with R-8 signal, evenings. ZQI, Kingston, Jamaica, 4.70, heard around 7 p.m. (Shadid, Illinois.)

PJY, Curacao, 15.140, heard calling WRS, 11:15 a.m., woman announcer. KIO, Honolulu, 11.680, heard working KKQ, California, strong signal, 8:15 p.m. Moscow on 15.240 heard with very strong signal, news in English, 11:00 a.m. Soldatensender, Athens, Greece, 9.930, woman announcer speaking German, no English, heard at 5:30 p.m. Prahava, 9.870, speaking Czech, some English praise of United States and President Roosevelt, heard at 5:35 p.m. XGOY, Chungking, China, 9.646, heard at 12 noon, good, clear signal, announced as "The Voice of China." (Barry, N. J.)

WWV, U. S. Bureau of Standards, a good guide for checkup on calibration of receivers, is scheduled as follows: 2.5 mc., 7 p.m.-9 a.m.; 5.0 mc., continuous day and night; 10.0 mc., continuous day and night; and 15.00 mc., 7 a.m.-7 p.m. Time checks are given on the various frequencies each quarter hour, generally. (Horn, N. Y.)

London's transmitter on 2.880, listed to open at 9 p.m., is now on at 8 p.m., announced on transmission of November 30. (Yates, N. Y.)

"Debunk, Voice of All Free America," listed as on 7.195, 8:30-8:50 p.m., is now heard on 7.210, Wed., Thurs., Fri., 8:38-8:48 p.m. (De Arras, Virginia.)

Jerusalem, Palestine, on 9.670, has English news at 1:45 p.m. HVJ, Vatican City, 17.445, has English news at 11:00 a.m., Tuesdays. Berlin, DJL, 15.110, DZB, 10.042, and DXR, 11.760, has English news at 11:30 a.m. VLC7, Shepparton, Australia, has English news on 11.840, at 1:15 a.m. (Harris, Mass.)

"Sinpac," believed to be in Honolulu, heard on 7.2 mcs., about 5 a.m., transmitting "Spotlight Band" spots for Blue Network. (Woolley, Colorado.)

Moscow on 15.53 is heard on the 6:48-7:25 p.m. transmission to the United States. (Brewer, Oklahoma.)

HE04, Bern, Switzerland, 10.338, puts in a good signal, 3:45-4:15 p.m. (Weissman, New York.)

TAP, Ankara, Turkey, 9.465, heard 4:25-4:45 p.m. daily; Monday and Thursday, information about Turkey; Sundays, "Postbag" program for SWL's. DXP, Berlin, 6.03, and DXJ, 7.24, heard to North America, 5:50 p.m.-1 a.m., with news on the hour. DJD, Berlin, 11.770, heard to Africa, 11:15 a.m.-4:45 p.m., with English news at 2:15 and 4:30 p.m. VLG3, Melbourne, 11.71, and VLG4, 11.84, heard 1:10-1:45 a.m., with English news at 1:10 a.m. VLG3, 11.710, and VLC6, 9.615, heard 11:00-11:45 a.m., with English news at 11:00 a.m.

The Swiss are now using 6.165 mcs.,

RADIO NEWS



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4. Conservative design and operation permits wide range of loading and modulation at high fidelity.

Supporting data on all these features will be furnished gladly, along with detailed facts on other Westinghouse advantages, such as: *Low Operating Cost, Simplicity of Control, Continuity of Operation, Ease of Maintenance.*

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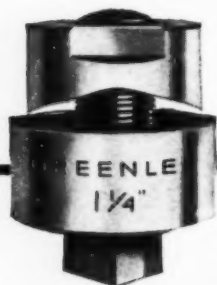
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February, 1945

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FOR SOUTHWEST READERS

From Tulsa, Oklahoma, Don Brewster sends us these tips for listeners in the Southwest (CWT):

The BBC's North American Service is now heard best on GSU, 7.26 mc., during the entire transmission, 4:15 p.m.-11:45 p.m., and during the latter part of the transmission over Leopoldville on 9.783 mc., 8:15-9 p.m., and 9:15-11:45 p.m.

XEW, Mexico City, is on the air broadcasting Mexican programs from their local station, XEW, during the daylight hours. They operate on approximately 9.50 mc. Reception is very good.

CBFX, Montreal, Quebec, is heard here in English on 9.63 mc. during early mornings from 7-8 a.m. Reception is excellent. Relays CBF, Montreal.

HCJB, Quito, Ecuador, is now heard from 7 to 8 a.m. and 3-5:30 p.m. This station is off the air on Mondays at these hours. Programs are of a religious nature. On Tuesdays through Fridays, they present radio lessons of Spanish (in English). The station operates best on 12.445 mc., and reception varies, but generally is good.

Radio Brazzaville, 11.97 mc., has been coming in with poor reception quality lately on its 6:25 p.m. news broadcast.

PRL8, Rio de Janeiro, Brazil, hasn't been heard here for some weeks. This station, on 11.720 mc. formerly was one of my best "stand-bys," when I didn't want to hunt around for other stations. I presume they still are short-waving their North American program in English from 9 to 9:40 p.m.

(EDITORS NOTE: PRL8 is heard 10-11 p.m. EWT).

VLC6, Shepparton, Australia, still comes in with excellent signal strength on its 7-10 a.m. broadcast, but is violently QRM'd here by a Spanish-speaking station, making the program almost unintelligible at times. The frequency is 9.615 mcs.

NEW ENGLAND REPORT

From our faithful friend, Gilbert L. Harris, of North Adams, Massachusetts, we have the following report this month:

11.635—Hungarian Nations Radio, heard Sunday, from 1:15 to 1:28 p.m.; good.

9.835—Hungarian Nations Radio, heard Sunday, from 3:15 to 3:30 p.m.

15.340—DJR, Berlin, heard with news in English at 10 a.m.; heard at 11:14 a.m. with odd music (probably African beam).

12.115—ZNR, Aden, Arabia, heard Sunday, from 11:50 a.m. to 12:01 p.m., testing with recordings. At 12:01 p.m. gave news in Arabic.

15.430—ZOY, Accra, Gold Coast, heard from 11:40 to signoff at 11:47 a.m. English announcement given just prior to signoff.

11.760—DXR, Berlin, heard at 9:30 a.m. with news in English.

9.535—JZI, Tokyo, heard at 9:35 a.m. with talk in English.

17.445—HVJ, Vatican City, heard Saturday, at 9:44 a.m. with bells ringing. Heard at 9:45 a.m. calling South Africa.

6.760—YNDS, Managua, Nicaragua, heard Saturday, at 11:06 p.m., with music.

18.080—GVO, London, heard signing off at 11:15 a.m.

21.470—GSH, London, heard Sunday, signing off at 11:30 a.m.

6.212, 7.420, 9.800, 9.930—Radio Atlantik, checked signing on at 1:30 p.m.

8.188—CNR, Rabat, Morocco, heard Sunday, at 1:49 p.m.

7.869—SUX, Cairo, Egypt, heard Sunday, at 3:24 p.m.

7.300—New Delhi, heard at 3:30 p.m. with news in English. Said "good night" at 3:48 p.m. signoff.

11.640—Press Wireless Station heard at 10:23 a.m. calling Paris, France; still on the air at 10:47 a.m.

9.590—Berlin, heard Sunday, at 11:45 a.m. with news in English at dictation speed. At 3 p.m. heard calling Ireland as Holland and Berlin. Then had news in English.

10.005—"Voice of Free Arabs," heard Sunday, 1:15-1:30, 2:15-2:30, and 3:15-3:27 p.m.

9.990—Dakar, heard Sunday, 2:20-3:31 p.m. Music with speaking in French.

9.705—Radio Martinique, heard Sunday, signing on at 6:30 p.m.

9.32—Buenos Aires, Argentina, heard Sunday, at 8:20 p.m., with music; still on at 10:30 p.m.

6.097—German Catholic Station, heard Sunday, 4:53-5:13 p.m., 5:33-6:13 p.m., and 6:53-7:13 p.m. Church music; talking in German.

15.170—TGWA, Guatemala City, heard at 10:45 a.m.

8.550—Radio Tevere (German-controlled Italian station), heard Sunday, signing off at 8 p.m.; 40 db. above S-9.

4.105—HCJB, Quito, Ecuador, heard Sunday, at 10:13 p.m., with music.

5.620—Trujillo, Peru, heard Sunday, 10:20 p.m., with music.

6.870—Managua, Nicaragua, heard Sunday, at 11:24 p.m., with music.

6.270—Station heard at 6:15 p.m., Sunday, very weak; believed to be "Die Heimat Ruft Die Front."

ANKARA'S "POSTBAG"

Of much current interest is the series of "Postbag" broadcasts from TAP, Ankara, Turkey, 9.465 mc., on Sunday afternoons from approximately 4:25 to 4:40 p.m. These programs are directed to SWL's the world over.

Gilbert L. Harris, Massachusetts, tipped me on this one and I have been hearing it R-9 plus each Sunday afternoon lately. TAP officials are anxious to have reports from anywhere in the world, according to announcement. Recently it was announced on "Postbag" that Turkey would shortly have three new transmitters on the air. Frequencies of these stations were not given. If anyone picks them up, please

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let me know. In the meantime we have written for full information on this proposed expansion of short-wave service.

COSTA RICA STATION LIST

We have just received the following list of short-wave broadcasting stations in Costa Rica from the *Direccion General de Telegrafos y Radios Nacionales*, giving call letters, frequencies, power, station name (identification), owner, and location:

TI-GPH, 5.875 mc., 1,000 w., "Alma Tica," Gonzalo Pinto H., San Jose.

TI-RH, 6.150 mc., 250 w., "Radio el Mundo," Rafael Hine Ch., San Jose.

TI-LS, 6.165 mc., 2,000 w., "Para Ti," Luis Saenz Mata, San Jose.

TI-RCC, 6.180 mc., 300 w., "Accion Catolica," Prbo. Carlos Borge, San Jose.

TI-EP, 6.700 mc., 1,000 w., "La Voz del Tropico," Eduardo Pinto H., San Jose.

TI-PG, 9.615 mc., 2,000 w., "La Voz de la Victor," Claudia Martinez N., San Jose.

TI-NRH, 9.692 mc., 750 w., "La Voz de Costa Rica," Amando Cespedes Maria.

The best-known stations in Costa Rica, of course, are those operated by Senor Amando Cespedes Maria, TI-NRH, on 9.692 mc., and the broadcast band station, T14-NRH, on 710 kilocycles. A verification from T4-NRH was much prized in the "good old days" of early radio broadcasting, you will recall.

In the broadcast band, Costa Rica now has in operation 24 stations from 575 to 1,200 kilocycles, inclusive, with powers ranging from 400 to 8,000 watts. (If anyone would like a complete list of these Costa Rica broadcast band stations, please write me.)

WATCH FOR DUTCH STATION

You should be on the lookout for broadcasts from The Netherlands short-wave station as that country is liberated from the Nazi yoke. An interesting story has come to us about how the new Dutch long-wave radio station, *Nerrijzend Nederland* (Resurgent Netherlands) was built secretly, piece by piece, "under the very eyes of the Germans" in different parts of occupied Holland.

The story was recently related by Frank Gillard, BBC correspondent, who reported that a group of Dutch patriots early last year had begun to build the transmitter, which broadcast from liberated Holland for the first time on October 3, 1944, in order "to have a radio station ready to go on the air as soon as the Allies reached Dutch territory."

"Through 18 months of occupation, under the very eyes of the Germans the work went on," he said.

"Three men were given the job of constructing a transmitter which would be powerful enough to cover the whole of Holland and be adequate for the job. They drew up their plans. Everything had to be done with great secrecy. The transmitter was to be

built in sections at scattered points, and then when the great day came the sections could be put together and free Holland could go on the air."

The Netherlands Government in London was informed of the plan by secret messages, Gillard said, and at the end of September, when a substantial part of Holland had been liberated, the different sections of the transmitter were assembled, an aerial was strung "between two chimneys," and *Nerrijzend Nederland* began a regular program service which can now be heard throughout Holland.

According to the best information we can obtain, the Germans still control the powerful short-wave voice of Huizen, but watch for the voice of a free Holland in the popular short-wave bands this spring!

REPORTS FROM READERS

(EWT, unless otherwise indicated herein.)

TEXAS—Ralph E. Dahm, San Antonio, Texas, using a Philco 116-B, says London comes in "fair," Berlin, "poor;" Tokyo, "good;" Moscow, "good;" Brazzaville and Leopoldville, "good;" Australia, "good;" and Djar-karta, "good."

WEST VIRGINIA—Charlie Gonder, a student at West Virginia University, Morgantown, West Virginia, reports:

The European Service of the BBC on approximately 7.45 mcs. is heard well from 5:45 to 6 p.m., with identification in drumbeats. The North American Service comes in well on all frequencies, evenings.

HP5K, 6.005, Panama Broadcasting Company, Colon, Panama, is heard with news in English at 11 p.m.

9.445—Brazzaville, French Equatorial Africa, pounds in from 6:30 to 7:45 p.m., with news in French for Canada at 7 p.m., and news in English for the United States at 7:25 p.m.

9.55—Radio Shonan, Singapore, heard in Japanese recently at 10:30 a.m.

11.72—Winnipeg, Manitoba, Canada, is heard well during the daytime and early evenings. Has news in English at 1:15 p.m.

11.737—COCY, Havana, pounds in here during the evenings. Signoff is usually at midnight.

11.897—Radio Tokyo is heard with a signal of great power these days, 6:15-8:15 p.m., with news in English at 6:20 and 7:20 p.m.

CALIFORNIA—Lt. William T. De Van, ASF Regional Hospital, Fort Ord, California, writes that he has been receiving Leopoldville, Havana, Tokyo, Voice of the Pacific Fleet, Rio de Janeiro, Australia, and Berlin, but finds the announcers "loathe to give station call letters."

FLORIDA—From Tampa, Florida, Bill Britton reports the following stations:

11.93, 9.825, 9.69, 11.68, London, weak to excellent, early evenings, and sometimes to 11 p.m.

9.615—VLC6, Australia, 8-8:45 a.m., good sometimes, but splashed badly by South Americans.

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11.77—DJD, Berlin, heard 4:15-midnight, fair.

10.543—Berlin, heard 5:55 p.m.-midnight, weak. (Believed to be Latin American Service.)

9.865—Madrid, 6-7:15 p.m., good.

10.338—Bern, Switzerland, 3:45-4:15 p.m., was good, but now rather weak.

9.539—Bern, Switzerland, 9:30-11 p.m., good.

11.725—Radio Tokyo, 9 a.m.-noon, good.

ACKNOWLEDGMENT

Thanks for all reports received this month. We are sorry we cannot print all of them due to space limitations, but please keep them coming as they are always helpful. Address: Kenneth R. Boord, % RADIO NEWS, 540 No. Michigan Ave., Chicago 11, Illinois.

-30-

QTC

(Continued from page 60)

positions both aloft and aground in the postwar aviation boom. Tax rates for some outfits are doubled up for the same properties because each state, as well as the Federal government, can tax them under present regulations. A recent proposed federal law will give the federal government exclusive control over all air traffic, which is as it should be; airways traffic is too national and international in scope to be governed by each state and control for traffic of this type should be under the federal government in the same manner that radio communications are governed . . . there would be a nice mess if we had each state making radio laws.

FEDERAL Telephone and Radio Corporation is getting a new television transmitter for Columbia Broadcasting System which will transmit both sight and sound on a single carrier. The new outfit will be located atop the Chrysler Tower in New York City and will broadcast the programs from studios of WCBW at Grand Central Terminal. Most of you in television will appreciate what this means in simplified design, reduced cost due to necessity of only one transmitter instead of two, and reduction in total number of tubes necessary. Additional stations, with the new type equipment brought out recently, will be installed in other key points by CBS before long, it is believed.

To go along with WNBT, the NBC television station in New York, NBC has filed for permits to construct stations in Cleveland, Chicago, Denver, San Francisco, and Los Angeles. New FM stations also will be placed in operation at points where the network maintains studios.

SOME of the marine coastal stations which have been closed for some time are expected to reopen shortly; business is picking up. Things

are still busy in various ports along the east coast with shipping still good . . . and U. S. Maritime still looking for men. The radio operator situation seems to be as usual—not enough men to go around for the three-men-to-a-ship regulations which have been in effect nearly a year now. Although Allied and Neutral nations lost 5,758 ships from the start of the war to the end of 1943, and the U. S. Merchant Fleet lost 767 ships, the construction of new ships by the Allied nations has far overcome this loss. U. S. construction alone has nearly replaced those lost. Very few ships have been lost since last year, the serious time being back in 1942.

Men of the Navy and Coast Guard who have been disqualified for some physical disability have been asked to enter the merchant marine by the USES to relieve the present shortages in the merchant fleet. Men with 18 months deck or engine experience can take exams for third mate or third assistant engineer.

ACA's Harry Morgan has appeared before WLB, dickering for a National Master Agreement to cover all ships and companies in place of making an individual agreement with each outfit and also trying to straighten out the wage situation. The boys on the ships have a base pay of about three quarters or two thirds what a radio operator gets ashore and the airways pay nearly twice what a marine man gets, so maybe that accounts for some of the boys going into aviation.

HAVE a recent letter from D. D. Bulkley requesting some dope on stations that send out press addressed to c.q. and also asking for some of the other stations sending regular press schedules that he may use for code practice. Can any of you assist with the above? We have already forwarded what information we have on hand but believe that some of you can furnish much more complete information. Thanks. 73.

-30-

Spot News

(Continued from page 18)

multiplexing system. Here facsimile could be multiplexed on transmitting maps, storm warnings, barometric readings, wind velocity and direction, ceilings, and other data which is reduced to permanent records. Marine services would find the system useful, too, he explained. They could use it for maps, charts, diagrams, etc. Mr. Payne also stressed the educational field, stating that facsimile provides a blackboard for every home and classroom.

Testimony of A. W. Norton and D. K. DeNeuf of Press Wireless revealed that a large increase in public service facsimile is expected. The im-

portance of the service, particularly in transmitting foreign language code and characters such as Chinese, Persian, and Turkish, was stressed. These experts also pointed out that facsimile can deliver intelligence in terms of ordinary English text at rates of more than 1000 words a minute. Commenting on this speed factor, Mr. Hogan said that no other method of communications can transfer ideas from one point of our world to another at any such speed.

Reporting for the Government, C. M. Braum, chief of the nonstandard broadcast application section in the broadcast division of the FCC, said that experimental facsimile broadcasting began in 1928. And from that date to 1939, the FCC had allocated frequencies between 1500 and 2950 kilocycles for these tests. In April, 1939, the frequency schedule was changed to include 25,025 to 25,250 kc.; 43,540 to 43,940 kc.; 116,110 to 116,470 kc., and any frequency above 300,000 kilocycles, except the band of 400,000 to 401,000 kc. In 1940, two of these bands, 43 and 116 megacycles, were reassigned to other services. There are now three experimental facsimile broadcast stations operating in a ten-channel 25-megacycle band from 25,025 to 25,250 megacycles. These are W9XWT, the Courier-Journal and Louisville Times Company; WBNS, Columbus, Ohio; and WOKO, Albany, N. Y. Mr. Hogan has a special license to transmit in the 43 to 50 megacycle band on FM with 1000-watts of power. The other stations' power are 1000 and 500 watts.

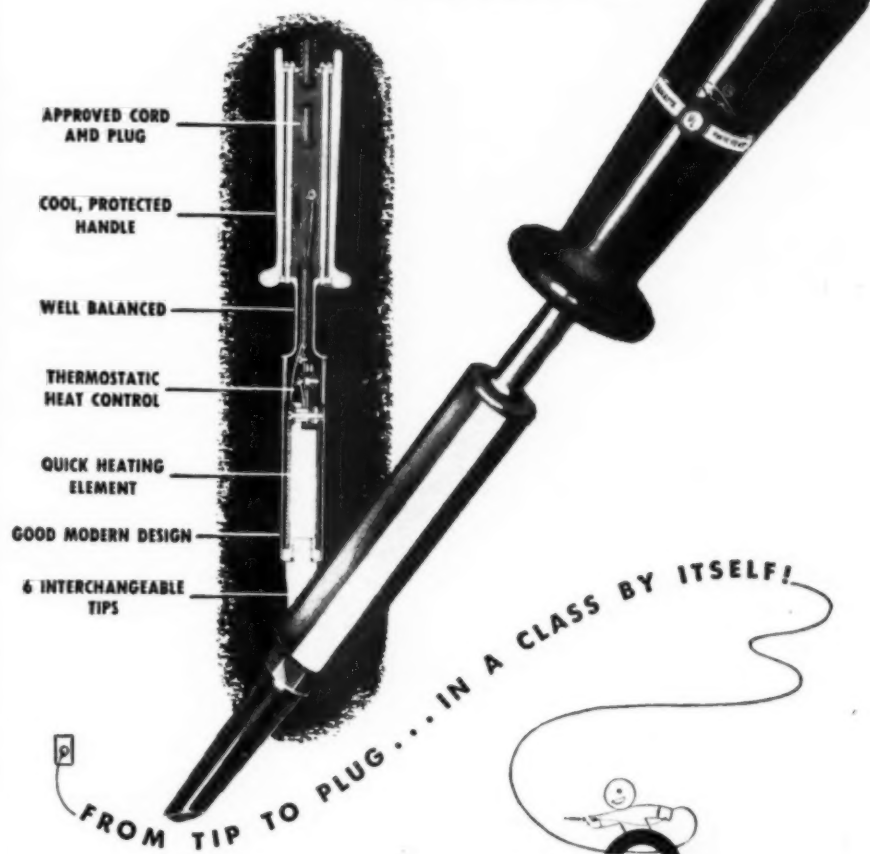
The many stations who had experimented with facsimile are expected to renew their interest and request new licenses.

One railroad has already tried facsimile from a station to a moving train and reported excellent results. The railroad . . . Chicago, Rock Island and Pacific. Messages were sent from the station on Blue Island to a 12-car freight train en route to Kansas City. The recording instrument was located in the caboose. The key message transmitted lauded the progress of radio, and indicated that facsimile is further evidence of American leadership in the art of communications.

A WALKIE-TALKIE SERVED TO PREVENT extensive loss of life and property during a recent fire in New York City. A fireman in a burning building notified those below through the walkie-talkie that highly inflammable materials stored in lofts nearby would be ignited if additional water and auxiliary pumping equipment were not put into action immediately. Not only was the water power supplied, but an additional alarm was sounded bringing the requested auxiliary equipment. The flames were brought under full control, and kept away from the inflammable material. During the year, fire department officials found the walkie-talkie to be

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THE NEW YEAR SAW MANY station shifts in the networks. The Blue network gained quite a few new members, which included 5000-watt KRNT of Des Moines; 5000-watt WPDQ, Jacksonville, Florida; 5000-watt WLAW, Lawrence, Mass.; and 10,000-watt WFTL of Miami, Florida. These new affiliates provide the Blue network with a total of 193 stations. The CBS network also has grown. There are now 152 stations in its system. Recent additions include: KOTA, Rapid City, South Dakota; KGKY, Scottsbluff, Nebraska; KTYW, Yakima, Washington; and WJEF, Grand Rapids, Michigan.

For a time, it appeared as if a new network would enter the broadcasting scene: the Cowles system. However, Gardner Cowles, Jr., president of the Cowles Broadcasting Company, declared at a sales meeting that they were not interested in starting any new network. They were purchasing stations in strategic locations, he admitted, but only to provide substantial local coverage. Links will be provided if the advertiser desires simultaneous coverage, pointed out Mr. Cowles. Describing their future plans, Mr. Cowles said that they expect to operate stations in Boston, New York, Washington, Minneapolis, Yankton, S. D., and Des Moines. FM will be featured in most instances. Former FCC Commissioner T. A. M. Craven is executive vice president, in charge of engineering for the Cowles interests.

TELEVISION

A BARRAGE OF COMPLEX QUESTIONS fired at television experts who appeared at a round-table session during the recent Television Broadcasters Association conference in New York City, provided many intriguing and informative replies. Questions asked covered the use of 16-mm. film, color, antennas, studios, program hours, coaxial cable and telephone wires for transmission, lineage, ghosts, and projection. Participating on the answering panel were: O. B. Hanson, NBC; J. E. Keister, GE; Dr. Allen B. Du Mont; Dr. C. B. Joliffe, RCA; F. J. Bingley, Philco; A. H. Brolly, Balaban and Katz; Klaus Landsberg, Television Productions (Paramount Pictures); C. W. Mason, Earle C. Anthony, Inc.; and Dr. Alfred N. Goldsmith, who acted as moderator.

Answering the 16-mm. question, Dr. Du Mont said that there is a need for improved equipment to provide recording of sight and sound. The film is very useful, he said, and every effort should be made to increase its efficiency. The industry needs a satisfactory 16-mm. station projector, too, he said. Other experts agreed with Dr. Du Mont on the value of 16-mm. film for television, adding that such

film would be ideal for the small television station owner, who could buy packaged shows and dispense with the expensive coaxial cables or relay links. Such a procedure would eliminate the timeliness virtue of the showing, but for certain periods of the day, this practice would not be too injurious, declared some of the specialists.

The delicate question of color was answered by O. B. Hanson, who said that color transmission and reception will not be practical for at least eight to ten years. He pointed out that all problems on the present black and white transmission on 6-megacycle bands should be solved first. Coaxial cables also will have to be improved to allow for wide-band transmission which color requires. Production problems are also acute in color work. Mr. Bingley said that color will not be available for a long, long time.

An interesting question on lineage inquiring into the history of increased multiple lines, particularly 525 lines, prompted a reply by Dr. Du Mont. He said that the Du Mont labs had experimented with high-definition pictures as far back as 1931, when they transmitted 735-line scenes. No improvements were noted, for as far as the lineage was increased, the peak of transmission and reception efficiency appeared to diminish. Receiver complexities also prompted many problems, such as involved sweep circuits. Ghosts also increased in appearance as the lineage was increased, Dr. Du Mont indicated. Dr. Joliffe added that they had studied increased line transmission and found that 735- to 1000-line transmission is a compromise between economy and practical transmission. More lines do not solve all the problems, he said.

Studio size questions were answered by O. B. Hanson and Dr. Du Mont. Mr. Hanson said that the studio should be very large, perhaps 25 feet in height, 40 feet wide, and 70 to 90 feet long. Such a studio would permit flexibility of action, better lighting, more room for substantial sets and better acoustic control. Dr. Du Mont preferred several separate studios to permit rehearsals, particularly for the benefit of prospective sponsors.

The use of telephone lines for television-signal transmission was discussed by F. J. Bingley and O. B. Hanson. Mr. Bingley did not look too favorably on the method. He said that many narrow-band systems for wide-band transmission have been conceived, but none proved practical. Mr. Hanson reported that transmission over telephone wires is practical, however, over limited distances. NBC has used telephone wire links over 1 to 4 miles quite effectively. Longer lengths of circuits would require too many repeaters, which would make the system quite costly and impractical, he said.

Projection received an interesting analysis by the panel members, too. Dr. Joliffe reported that the 525-line pictures are adequate for projection.

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"X" in thousands of homes of every type.

So plan your merchandising about this theme, and remember that Stromberg-Carlson is:

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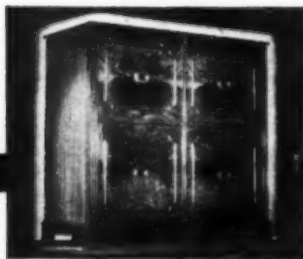
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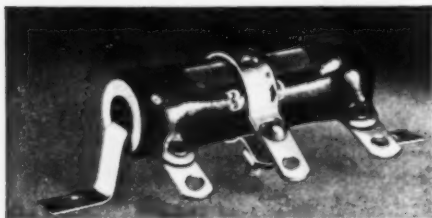
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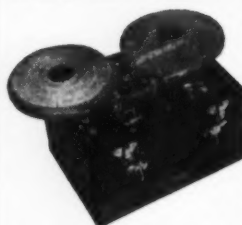
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He pointed out that in 1940, a 440-line picture was enlarged to 12 by 15 feet at the New Yorker theater, with satisfactory results. The present systems will provide an exceptionally bright picture on an 18 x 24 inch translucent screen, he pointed out. A modification of the Schmidt optical system used in 1940 has been adopted for the new system. The image will be bright enough to view in a moderately lighted room.

Answering a question on the properties of the very-high frequencies for television, J. E. Keister pointed out, since very-high frequencies are very directional, an expensive directive antenna array would be necessary to not only receive signals from a variety of directions, but to avoid ghosts. If the antenna were directed at the station, ghosts probably could be minimized, he said. But this would require some form of antenna switching. Klaus Landsberg reported that impedance matching is critical at the very-high frequencies. The lead-in wire would require special treatment in its installation, a treatment that might be costly and difficult in large apartment buildings.

NEW OFFICERS WERE ELECTED

at the close of the TBA conference. J. R. Poppele, chief engineer of WOR, was named president, succeeding Dr. Allen B. Du Mont, who becomes a member of the board. Robert L. Gibson, assistant to the vice president, in charge of advertising and publicity at General Electric was elected vice president. O. B. Hanson, chief engineer of NBC, was named assistant secretary-treasurer. Will Baltin was re-elected secretary-treasurer. Serving on the board are J. R. Poppele, Curtis W. Mason, and F. J. Bingley.

Achievement awards were given to Lloyd Espenschied, Bell Telephone Laboratories; P. T. Farnsworth (accepted by Ray Cummings of Farnsworth); Dr. Peter Goldmark, CBS; Dr. Vladimir K. Zworykin, RCA; Dr. Allen B. Du Mont; Brigadier General David Sarnoff; David B. Smith, Philco; Dr. A. N. Goldsmith; and Dr. W. R. G. Baker, General Electric. Stations WABD, WNBT, WRGB, WPTZ, WCBW, and W6XYZ were also award winners.

Personals . . .

Dr. Ernst Fredrik Werner Alexanderson, consulting engineer at General Electric and inventor of the famed Alexanderson alternator, has won the Edison medal for 1944. The presentation was made in a joint session of the IRE and AIEE in January. . . . **Theodore C. Streibert** has become president of WOR, succeeding **Alfred J. McCosker**, who became chairman of the board. **Jack I. Straus**, president of R. H. Macy, resigned his post as chairman of the board. . . . **Murray Crosby**, inventor of the FM Crosby Circuit, has become a consulting engineer for Press Wireless. He was formerly

a research engineer for the communications divisions of RCA Laboratories at Riverhead, Long Island. . . . **Brigadier General Frank E. Stoner** has become a Major General, and **Colonel David Sarnoff** is now a Brigadier General. General Stoner is chief of the Army Communications Service. General Sarnoff has been serving the Army in a special consulting capacity. He received the Legion of Merit for his services in reopening of communications in Paris. . . . **Leon Golder**, formerly of Rolta, has joined General Instruments as manager of a speaker division, which will be known as the General Electronic Apparatus Corporation. . . . **D. Martin** has become chief engineer of Wilcox Gay Corporation. . . . **Arnold Peterson** is now an applications engineer at United Electronics. . . . **D. H. Miller**, president of Speer Carbon, died recently. . . . **Raymond Soward** has rejoined Supreme Instruments Corporation. He is now chief engineer. **Robert H. Streeter** also is now with Supreme as a design engineer. . . . **Louis G. Pacent, Jr.**, son of Louis G. Pacent of the Pacent Engineering Corporation, has been named head of the industrial engineering department of Emerson Radio.

—30—

Let's Talk Shop (Continued from page 51)

radio sets. This arrangement can be made, but it does involve additional bookkeeping and is frowned upon in most cases. Most dealers will want to supply their own tubes to the serviceman for the repair of their own customers' sets. This should be considered as part of the sales and commission on their sale and is due the serviceman.

There should be a flat charge for installation of new radio sets done for the dealer. If further installation has been made for which the customer is charged, then the usual discount arrangement between the dealer and the serviceman applies.

Auto Installation

Another large part of your wholesale business should be the installation of auto receivers for auto dealers as well as retail radio dealers. There are two ways in which to do this—in the dealer's place of business which in all cases is to be frowned upon since you have to use portable equipment and installations take longer and are not as profitable. The preferred way to handle this is to do the work in your own place of business. If you are going to have any amount of volume of auto installations, you must make arrangements suitable for this work. You should also have a trained man who does nothing but auto installation and repair. You will find that the average serviceman that you hire will waste more time if he is

inexperienced with auto servicing than on any other job you can give him.

You will also find that generally the manufacturer of automobiles has specified in his price manual to the auto dealer, the amount of money which should be allowed for auto radio installation. You will be able to do the job for this amount of money, provided as noted above, you have an efficient, well-trained installation crew. In other cases, you will find automobile dealers with no cost knowledge about the installation of auto radios, and you should then arrange to make price agreements with him based upon the actual time and materials needed for complete installation.

The above remarks outline in some detail the major considerations of a wholesale operation. Generally speaking, the greatest danger is occasioned by a drop in volume of the number of repair jobs which are available at any time throughout the year. Under operating conditions before the war, as most of you know, a drop in the volume of repairs could be expected during the summer months. By using auto radio installations and repairs, it was found that the volume of business could be maintained. However, this is not enough and you should consider using all means of sales promotion at your command throughout the year in order to maintain volume.

Since most servicemen do not have sufficiently large capital structure to permit carrying a large number of employees on the payroll in times of slack business, this represents a very real danger to the operation. Store traffic is not important in the wholesale business operation since obviously most of your work will be done over the phone and by contact with the individual dealer. Therefore, it is not necessary to maintain a large imposing salesroom at a consequently large expense in this type of operation. Space does not permit the elaboration of more complete details. If any of our readers have any further questions, we would be glad to help answer them.

J. M.

Multi-Band Transmitter

(Continued from page 50)

ing output on high crystal harmonics, this can be avoided without sacrificing desirable simplicity by buying a couple of extra, high-frequency crystals—a cleaner, cheaper, surer course than loading oneself down with a long string of frequency-doubling stages making for complexity and bother—not to mention greater strain on the pocket-nerve.

A companion receiver exists, 8" by 5" by 3½", superheterodyne, single-signal, 1750 through 30,000 kc. It is hoped that it may be described and illustrated in a future article—that the data here presented may prove of interest to currently aching-to-be-active amateurs.

-50-



IT TAKES

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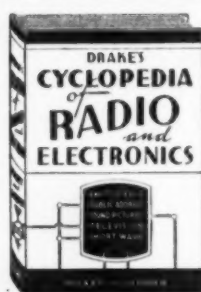
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Tone Control Circuits

(Continued from page 43)

o'clock, to accept pointer-knob set screws. A convenient ground for the bass cutoff control is a shakeproof lug of the type usually furnished to fit over volume-control shanks. To this lug can also be grounded the shields of the input and output lines.

Testing

Install the equalizer between record player and amplifier, set its controls all the way right, and turn on the system. If no unusual hum appears as the amplifier warms up, rub the needle point of the pickup with your finger to test for a signal; if no sound comes from the speaker when the needle is agitated, look for a ground between the audio line and its shield—inside the equalizer, at connectors—or at a connection to the wrong (left-hand) side of the bass cutoff resistance. This last may be checked by rotating the control counterclockwise, and again testing at the pickup. If the signal now carries through to the speaker, change the bass cutoff ground to the control's other end terminal.

If noticeable or excessive hum appears when the tubes warm up, a break may exist in shield or line, or hum is being picked up by an unshielded portion of the line. Often if the phono motor frame is not grounded to the shield of the pickup line, hum from a.c. wiring in the motor is induced along unshielded line underneath the shell of the pickup arm, and may become stronger when the pickup is handled, especially when an ungrounded pickup and its cartridge shell are connected to the audio line by mistake. Hum through which signals still may be heard occurs most often at an exposed section of line outside the amplifier chassis, and an unprotected inch or two in a high-gain system can produce enough induced hum to be noticeable through music being reproduced at the same time. Tracing and eliminating hum calls for considerable patience and for ingenuity in producing a continuous shield.

A very loud hum, through which no signal from the pickup is transmitted, requires testing of all audio lines and connections for a break. Since voltage in the pickup circuit is very low, any weak connection easily may have too high a gap-resistance to conduct such "no-voltage" currents.

Testing Operation of Controls

Turn the equalizer controls all the way to the left and start a record on the player. Turn the bass cutoff right until sound appears, and as you continue with this control, adjust volume on the amplifier to a fairly high level. As the bass control reaches its maximum position, turn up the volume until the bass begins to distort or boom, then try cutting out bass to a satisfactory listening level by returning the cutoff slowly toward the left. The

effect should be distinctly audible, and if no change occurs during this adjustment, or the control traverses its entire range without effect on the over-all volume, a break exists within the control or at its ground connection. Blind spots along the resistance will produce sudden increases of volume when the cutoff is set to include the higher frequencies, and a control having such spots should be replaced.

Leaving the bass cutoff turned to the right, advance the series load of the filter in the same direction. High notes should weaken considerably until they become relatively inaudible against the bass when the series load is at its maximum of 5 megohms. Now advance the condenser by-pass to the right. Each change should produce a greater proportion of highs. If a step value decreases the highs during this advance, the fixed condensers were arranged in improper sequence at the selector taps, or one of them has an open connection. A shorted condenser will result in excessive volume when placed in the by-pass; it should be checked for external shorting and discarded if it still by-passes the entire load.

Operation of the Equalizer

Individual amplifiers vary greatly in the amount of distortion present in each tone range. Likewise, in a given amplifier, these characteristics vary with change in volume level. Hence, experimentation in using the equalizer with your own amplifier is the quickest way to attain satisfactory control of results. The equalizer permits a wide range of possible control, to which is added the scope of tone controls already present on your amplifier.

Fig. 1 illustrates a general rule that highs and lows should balance one another, whether closely confined about the middle frequencies for high volume or expanded in wide range for lower volumes. Low volume requires a greater amount of highs and lows in proportion to mid-frequencies, and high volumes are most effective if highs and lows are reduced to a narrow range setting, not only to minimize overload distortions within the amplifier in these ranges, but to reduce room-echo and resonance, which are very unpleasant in higher frequencies at loud volumes.

These principles may be tested easily. For a given recording, set the by-pass to a point where brilliance and scratch noises are not too prominent, then adjust the low-frequency level with the bass cutoff. If the recording is deficient in highs, its balance improves by moving the cutoff up into the lower mid-frequencies. If it is weak in lows, add power in this range by reducing by-pass values, and by opening the bass cutoff to maximum bass, increasing amplifier volume and then applying enough bass cutoff to prevent distortion.

Record scratch for most low-pressure pickups sounds sharpest at the 100 μ fd. by-pass value. Greater val-

ues submerge it in increasing predominance of the medium frequencies and lesser ones cut out the hiss as well as portions of the high range. Note that use of the bass cutoff to balance whatever proportion of highs is chosen reduces hiss to a minor element in a correctly balanced tone picture, which may be expanded or contracted to include any desired amount of the sound spectrum.

The series load may at times be somewhat reduced to shift emphasis of tone slightly downward for by-pass values up to 100 μ fd. Recordings are seldom deficient in the lower mid-range frequencies, but overbrilliant highs resulting from certain types of recordings made in nonresonant studios often benefit if played with emphasis shifted away from them in this manner. With the by-pass set at 250 or 500 μ fd., more of the highs travel via the condenser, hence the reduction of series loading has less effect on higher by-pass values.

Warped or uneven records sometimes produce rumble in the low frequencies, which may be reduced with the bass cutoff; records pressed from worn or duplicate master molds may have very rough and constricted grooves. Resultant noise may be lessened by cutting out the by-pass entirely and also most of the bass range. This method of reproduction from a narrow middle band reduces the unpleasantness of the chatter and gritty sounds of such discs, but there is no effective remedy for a gravelly record of this type.

About Pickups

Manufacturers of crystal pickups supply equalization data which show values of parallel and series resistance loads and of high-frequency by-pass condensers, as well as the frequency-response curves accompanying these circuit values for a particular pickup. The writer is much indebted to the information thus available, for the equalizer circuit in the form described here is the result of experiments based on data supplied with pickups of a number of manufacturers.

Each model has circuit values which give equally distributed response throughout the sound spectrum range, in the straight line which characterizes high-fidelity response. The equalizer is designed to include these values, as given for widely-used types of pickups, and the additional values needed to compensate for the acoustical needs of high and low volume levels shown in Fig. 1.

Wide-Range, High-Fidelity Operation


A sound-system which reproduces all frequencies with equal intensity from 30 to 7,000 cycles per second in wave-forms closely resembling the original input signals is said to be a wide-range, high-fidelity system. In reproducing disc recordings of music, such a system will include turntable rumble and surface irregularities as low-frequency noise, and its high-frequency range will include needle-hiss and mechanical resonances of the pickup. At low volumes, these noises may not be objectionable, but they will become noticeable at average volumes, and at very high volumes their effects will be very unpleasant, unless their ranges are reduced by further adjustment of the equalizer circuit, which was already a part of the system to secure linear, or high-fidelity, response from the pickup.

Thus, the main advantage of a high-fidelity system lies in its medium-volume operation where all of a recording is adequately and clearly reproduced at a level least fatiguing to listeners, and their neighbors. This adequate volume is lower for a high-fidelity system than for a reproduction unit whose restricted range and "mellowness" (overemphasis on low frequencies) cannot present clearly detailed highs without distorted booming in the low range, a range already clipped of its true bass frequencies to avoid the audio power requirements of these frequencies for even moderate volume levels.

"Phonographs" and combinations of this sort are what lead devotees of recorded music to the purchase of higher-powered separate amplifier systems, to escape inadequate, inefficiently-used conventional audio systems. To the subsequent unhappy discovery that higher-powered phonograph systems need a very efficient and flexible control unit, the equalizer circuit, together with description of its theory and operation, is offered as a solution by the author with assurance that the unit meets that need as it was encountered in a number of, practical installation problems.

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Transit Utilities (Continued from page 45)

radio (both present and expected in the immediate postwar period) make a general reallocation inevitable.

In transit, for instance, 20 companies already have gone on record as desiring to install new stations as soon as the necessary equipment is made available. Many others can be expected to follow suit. The investment is not great. In the case of Capital Transit it amounts to only \$20,000—for a company whose worth is around \$40,000,000. But the 10 frequencies presently available for such use do present a potential obstacle. Capital Transit on 31,460 kilocycles gets interference at times from the Brooklyn & Queens Transit Corporation, the first transit utility to use two-way radio. And because the frequencies are limited, the FCC requires that they be used only in emergencies.

At the allocations hearings the transit companies proposed that 20 channels in the 30-40 megacycle band be set aside for their use for emergencies. There is no doubt that the 10 frequencies now allocated them will be inadequate if a large number of the hundreds of companies in the country want to adopt radio. The argument advanced in favor of 20 channels, however, seems open to question. Of the 250 separate transit companies in New York City, it is pointed out, 20 are large enough to be considered likely applicants for radio frequencies. The problem of interference could be solved only by 20 different frequencies. Admittedly sharing of a frequency by two different companies may mean that one is deprived of radio service if the other is handling a serious emergency. There is the interesting possibility, however, that in New York, or any large city having several transit companies, an organization might be formed which would be assigned several frequencies and which would contract to handle emergency communications, and, conceivably, the emergencies themselves, under contract for all the transit companies in a municipality. (Similarly Aeronautical Radio Inc. handles radio communications for many of our commercial airlines.) While the 10 emergency frequencies probably will be increased, the 20 channels (10 extra) requested for this purpose may not be granted.

Unquestionably, radio has proved successful in avoiding and correcting transit emergencies. It is helpful in an almost infinite number of possible situations. Perhaps a fire is reported over the police radio. At the transit company's dispatchers' office the location of the fire is noted and checked against the trolley routes. If the fire is in the vicinity of the tracks, a mobile unit is ordered to the scene. Quite often on arrival the supervisor will find that it has been necessary to place a fire hose directly across the trolley tracks. Where the cars are powered

through an overhead wire, it is a matter of seconds to restore service. Grooved metal hose jumpers protect the fire hose and the streetcar rolls right over them. If the power is derived from a contact rail on the ground, the problem is more complex. The supervisor radios his dispatcher that a hose bridge will be needed. This cumbersome device holds the hose aloft so that trolley traffic may proceed normally underneath it. The dispatcher, of course, reroutes traffic until the bridge is delivered and set up, and normal service can be resumed.

With two-way radio equipment all these arrangements can be completed in an amazingly short time. But for most transit companies all the work must be directed by telephone. The delay may amount to two hours. Supervisors who cruise their districts report to the dispatcher every 30 minutes as a matter of routine. Capital Transit, for years has had 20 telephones at strategic points throughout Washington. If the fire did not happen to be located near a phone, the supervisor might be delayed getting to one. Perhaps the emergency truck and crew usually stationed at the main office have just been sent out on a call.

In extreme emergencies, such as floods or severe storms, telephone lines may be crowded or even cut off completely. Availability of radio in such cases may mean lives saved. In cities which are subject to flood conditions, transit company supervisors are stationed at the low points on the system during flood danger to report on the rise or fall of the water. When conditions change rapidly and instant communication is not possible, cars or buses may be trapped by the rising water.

Another case in which instant supervision is needed is damage to the wire structure with resultant danger to persons or autos from the 600-volt trolley wire.

A report of an incident in Cleveland is typical. "On March 19, 1944, at 7.45 a.m., an automobile hit and broke a steel pole which helped support trolley wire at East 75th St. and Quincy Ave. The pole fell, blocking the track and causing trolley wire to sag badly. Zone 3 supervisor was notified by radio and cleared the tracks and held the wire up to let the cars move until the line truck arrived. Total delay was only eight minutes."

One potentially useful bit of equipment which requires no additional frequencies is the walkie-talkie unit. With it, emergency crews in a situation covering an area of several blocks could stay in constant contact with each other and with the supervisor. A fairly common difficulty in which they certainly would be used is when a whole section of track becomes temporarily useless due to power failure. Two crews working from either end of the track and testing as they go along can clear up the trouble much faster if one immediately can notify

the other to come and help make repairs as soon as the source of the trouble is discovered.

A recent traffic control device, a "headway recorder," is particularly effective when combined with use of two-way radio. Electrical contacts at selected check points are activated by the passage of the trolley. The current is carried on a telephone wire to the recorder where a pen automatically uses a mark each time the contact is closed. A moving tape less than ten inches wide may contain twenty columns for as many different check points. Capital Transit's headway recorder, installed in July, has two tapes with 20 columns on each. On some routes the lines come close together—perhaps there is only a minute-and-a-half headway between cars—on others the spacing of the lines indicates a regular 15-minute headway. If the dispatcher notes a four-minute headway when it should be only two, he radios one of the mobile units to make an investigation. The reports he may get back range from "overloading" (with longer delays at stops and more frequent discharge stops) or "funeral" to "collision" or "defective car." Companies using headway recorders find that the dispatcher almost invariably is able to spot trouble on a line before it is reported.

An incident at the Brooklyn & Queens Transit corporation shows how well this can work with the two-way radio. The dispatcher on duty at the machine called to the radio dispatcher that one location had a break of six minutes on a line with a three-minute headway. An inspector sent to check up found a truck overturned on the track. He radioed for an emergency wagon, but cancelled the call a minute later. He had gotten a passing truck to pull the overturned vehicle off the track. The line was blocked only eight minutes from the time the delay was spotted at the dispatchers' office.

While these machines work only on cars using tracks, experiments point to the possibility of radio-activated headway recorders for buses. Such use of radio, however, does not come under the "emergency" use for which frequencies are now granted to transit companies. They are requesting, however, 20 additional channels for this and related traffic control and supervisory use. Another experiment whose future will depend on the outcome of the FCC allocation hearings is a radio-controlled track switch device. It is said to be simpler and more foolproof than the present electrically-operated control; it involves an electronic-tube circuit controlled by a switch on the instrument panel, entirely independent of the main power circuit. The twelve extra channels requested for this use probably will not be granted.

Greater use of radio certainly will mean better service to the public, and better service will mean better business for the transit companies. During 1943 they provided passengers in

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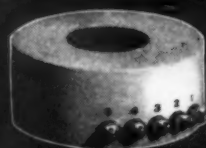
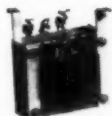
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the U.S. with 22 billion rides—a war-born increase they would like to maintain. Capital Transit's engineers have worked out half a dozen different methods of improving service which depend on increased use of their frequency. At present they send and receive about a hundred radio messages a day. The messages average half a minute each. Thus, the frequency is used less than an hour a day. Perhaps another hundred incidents a day are handled by telephone as they are not considered "emergencies" in the sense intended by the FCC. But, by such limitation of use, the FCC is enabled to assign the same frequency, despite limited interference, to several other companies and still leave a margin of safety sufficient to handle really serious and widespread emergencies in any area.

The additional channels requested by the transit utilities now are being used by other services for which other frequencies must be allocated if the transit companies are to be given all or part of what they ask. Some rearrangement probably will be made; perhaps even the definition of emergency may be broadened. But it seems certain that at the present time each company's use of its frequency will be limited.

-30-

STANDARDIZED GRAPHICAL SYMBOLS

THE American Standards Association has recently published a bulletin, No. Z32.5-1944, entitled "Graphical Symbols for Television, Telegraph, and Radio Use." This bulletin presents the graphical symbols and abbreviations for use in schematic diagrams, that are considered to be standards.

In conforming with the policy of RADIO NEWS, we will adopt these standards as soon as possible, as they are presented.

Fig. 1. shows the old and new methods of symbolizing fixed and trimmer condensers. In regards to the fixed condenser, a curved line will be used. This curved element, where it is necessary to identify the capacitor electrode, shall represent the outside electrode in fixed paper dielectric and ceramic dielectric capacitors. It also shall indicate the negative electrode in electrolytic capacitors.

Variable trimmer capacitors will be indicated, as shown in Fig. 1, with the letter "T" directly alongside. Where



Fig. 1.

variable capacitors are to be indicated, the same symbol will be used with the letter "T" omitted. The curved line will indicate the moving element in variable capacitors.

All other symbols, which have been adopted as standards, conform in general with those appearing in the past in this publication. . . . Editor.

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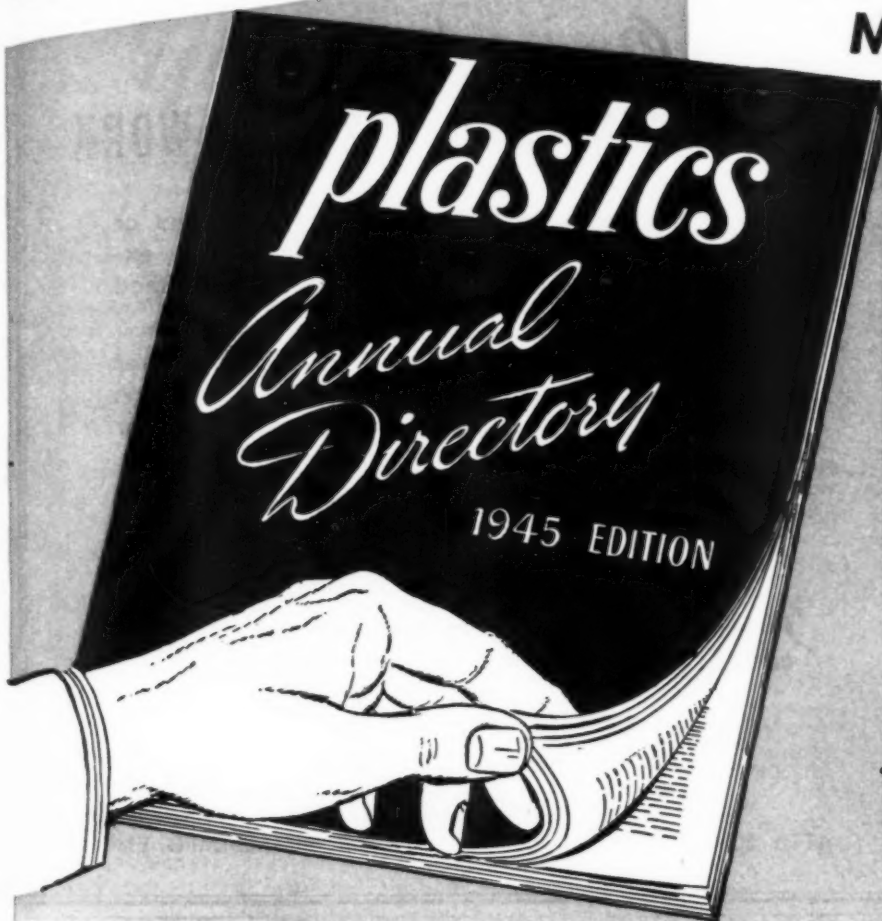
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U.H.F. Course (Continued from page 59)

however, the magnetic field will col-
lapse and force the electrons to flow
around the circuit into the other plate
of the condenser. The condenser now
is charged up, but in the other direc-
tion. The process is ready now for
repetition. While in the above exam-
ple the energy was introduced into the
circuit via the condenser, another coil
inductively coupled to the first one
would have been quite as satisfactory.
The same is true of the cavity resona-
tor, with the electron beam doing the
activating. This latter means might
be called capacity coupling although it
might be rather hard to say this with-
out some reservations.

The second matter to consider per-
tains to the points where a possible
loss of energy could take place. If the
cavity resonator were enclosed entire-
ly and the dielectric was air (as it
nearly always is) then the only pos-
sible place that energy could be lost
would be in the confining walls. In
the preceding explanations, the walls
always have been postulated to be con-
structed of materials that had no re-
sistance or, what is the same thing, in-
finite conductivity. This was done to
simplify the discussions so that more
important ideas could be understood.
Now, however, it is time to remember
that actually there are no materials
that possess the above properties and
anything that could be used for the
walls of the cavity resonator would
have some resistance, no matter how
slight. The waves in a resonator, in
their continual back and forth motion,
strike the various walls and cause cur-
rents to flow. Current flowing through
a resistance will lose energy in a man-
ner dependent on the amount of flow
and the resistance. I^2R covers this
completely. This, then, would be taken
from the energy contained in the fields
in the resonator and would represent a
loss. The latter would represent to a
cavity resonator what the resistance
in the coil and connecting wires would
mean to a low-frequency resonant cir-
cuit.

While the walls are perhaps the
place where the greatest amount of
energy is lost, it is by no means the
only place. Cavity resonators never
are enclosed completely and so some
energy could escape through these
openings. By proper design, this lat-
ter loss is generally kept very small.
A third method whereby energy would
be lost could be brought about by elec-
trons arriving at the resonator grids
in time to absorb energy instead of
giving some. This latter point can be
very important, especially with poor
design, for the entire oscillating pro-
cess depends on the fact that the grids
obtain more energy from the electrons
than they give up. This third type of
loss is taken care of by combining it
with the total received energy and
using their difference.

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Returning to the discussion of the Q of a cavity resonator, the preceding paragraphs indicate that the ratio:

Volume of Resonator

Surface Area of Resonator

should be proportional to the Q of the resonator. The ratio is based on the fact that the energy is contained in the volume of the resonator while the loss in energy occurs in the walls and these are expressed by the surface area. With this ratio a higher Q will be obtained if the volume to surface ratio is large and in practice this objective is striven for when these small units are designed.

The reader will notice that fundamentally the definition of Q and all it stands for (selectivity and efficiency of a circuit) still remains the same, although expressed slightly differently. The need for a change was brought on by the variation in design and construction of this newer tuning unit. That it can be altered and still possess the same meaning shows at once the relationship between the old and the new and speaks well for a system of units that is so flexible.

In the operation of cavity resonators with high-frequency oscillators, the resonator structure is generally made an integral part of the tube itself and as such is subject to changes in volume because of the heat that is generated in the tube, both at the collector plate (see article on Klystron) and at the filament. A change in volume automatically will alter the resonant frequency of the resonator. In practice, this undesirable effect is minimized by constructing the resonator with materials that will counteract the change in frequency (a decrease).

With the conclusion of the discussion on the Q of a cavity resonator, this article is brought to a close. Only the basic theory has been covered and applied essentially to a simple rectangular resonator. Needless to state, almost innumerable forms of resonators may be used, all essentially the same except for the field distributions. To date, the mathematical theory has been applied to only a few of these complex shapes.

(To be continued in April issue)

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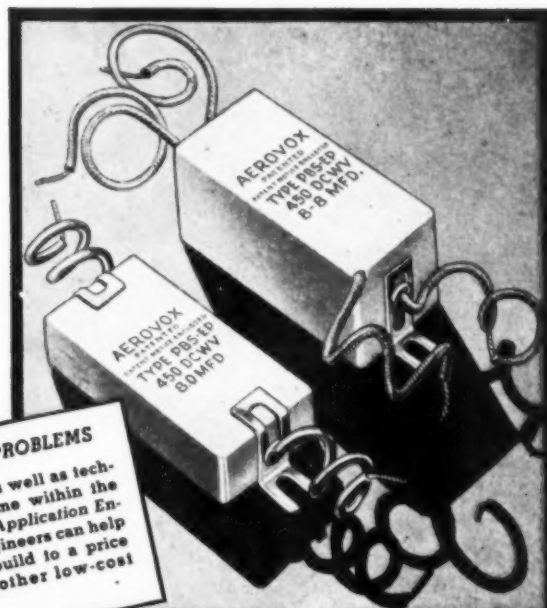
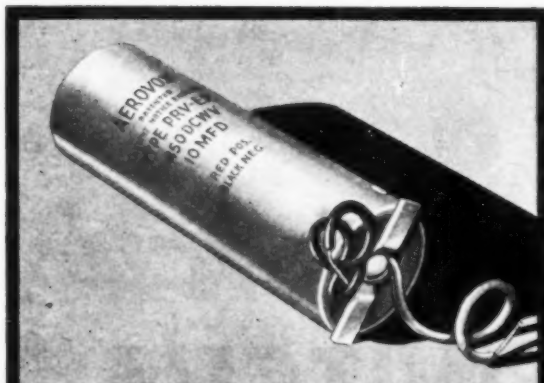
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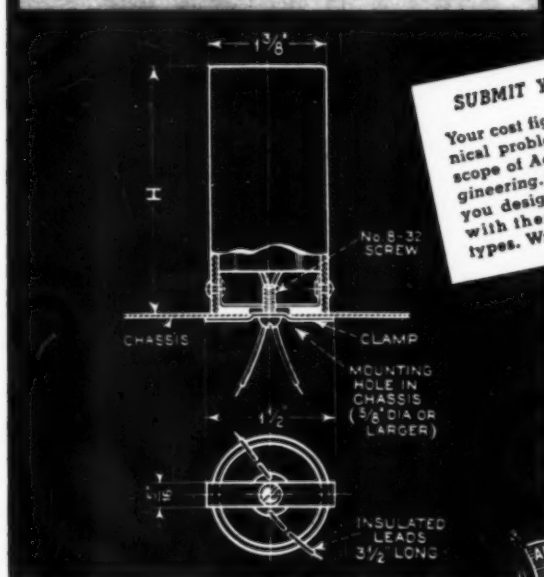
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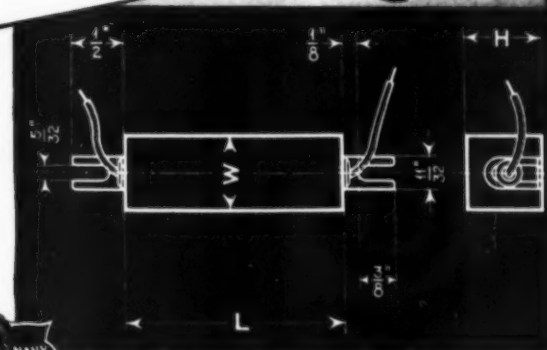
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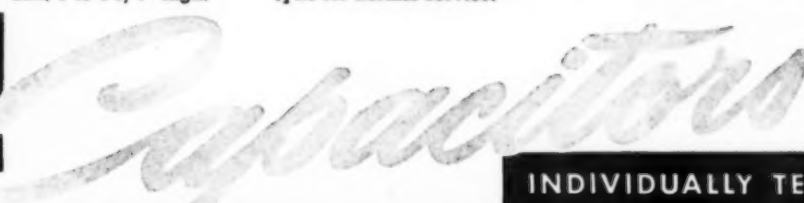
CLAMP-MOUNTING ELECTROLYTICS

● **PRICE** with inbuilt Aerovox Quality—that's the prime objective of the ingenious Type PRV one-hole-mounting paper-cased electrolytic. • Wax sealed. Impregnated cardboard-tube container. Suitable for commercial and other applications where extreme operating conditions are not encountered and metal-can types are not essential. • Note ingenious clamp and center-screw mounting means. This type can take the place of various other vertical-mounting electrolytics such as twist-prong, spade-lug, screw-base, etc. • Normally with etched foil. Also available in plain foil. High-purity aluminum elements throughout. Positive and negative lead for each section. 450 and 600 v. D.C.W. 4 to 40 mfd.; 8-8 to 20-20 mfd. 1-3/8" dia.; 3 to 4-3/4" high.



CARDBOARD-CASE ELECTROLYTICS

● **PRICE** with inbuilt Aerovox Quality—that's the prime objective of this popular Type PBS rectangular cardboard-case dry electrolytic. • Sections housed in sturdy cardboard containers. Patented Aerovox Adjustimount or swivel metal flange permits mounting flatwise or on narrow side according to space limitations. Also, PBS units may be stacked and held together by overlapping metal flange and soldering securely. • Normally with etched foil. Plain foil also available. High-purity aluminum elements throughout. Made in single and multiple sections. Separate sections with positive and negative leads for each section. • 450 and 600 v. D.C.W. 4 to 16 mfd.; 8-8, 8-16 and 8-8-8 mfd. Dimensions: L, 2-7/16 to 3-3/16"; W, 3/4 to 1-1/2"; H, 1/2 to 1-7/16". A good general-purpose electrolytic for normal service.



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TABLE I—SINGLE BRAID TYPES

Designation	Impedance, Ohms	Capacitance, p.f./ft.	Attenuation, db/100 ft.	Weight, lb./100 ft.
ST-1	50	1.8	0.1	0.1
ST-2	50	1.8	0.1	0.1
ST-3	50	1.8	0.1	0.1
ST-4	50	1.8	0.1	0.1
ST-5	50	1.8	0.1	0.1
ST-6	50	1.8	0.1	0.1
ST-7	50	1.8	0.1	0.1
ST-8	50	1.8	0.1	0.1
ST-9	50	1.8	0.1	0.1
ST-10	50	1.8	0.1	0.1

TABLE II—DOUBLE BRAID TYPES

Designation	Impedance, Ohms	Capacitance, p.f./ft.	Attenuation, db/100 ft.	Weight, lb./100 ft.
DT-1	50	1.8	0.1	0.1
DT-2	50	1.8	0.1	0.1
DT-3	50	1.8	0.1	0.1
DT-4	50	1.8	0.1	0.1
DT-5	50	1.8	0.1	0.1
DT-6	50	1.8	0.1	0.1
DT-7	50	1.8	0.1	0.1
DT-8	50	1.8	0.1	0.1
DT-9	50	1.8	0.1	0.1
DT-10	50	1.8	0.1	0.1

TABLE III—ARMORED TYPES

Designation	Impedance, Ohms	Capacitance, p.f./ft.	Attenuation, db/100 ft.	Weight, lb./100 ft.
AT-1	50	1.8	0.1	0.1
AT-2	50	1.8	0.1	0.1
AT-3	50	1.8	0.1	0.1
AT-4	50	1.8	0.1	0.1
AT-5	50	1.8	0.1	0.1
AT-6	50	1.8	0.1	0.1
AT-7	50	1.8	0.1	0.1
AT-8	50	1.8	0.1	0.1
AT-9	50	1.8	0.1	0.1
AT-10	50	1.8	0.1	0.1

TABLE IV—AIR SPACED LOW CAPACITANCE TYPES

Designation	Impedance, Ohms	Capacitance, p.f./ft.	Attenuation, db/100 ft.	Weight, lb./100 ft.
LT-1	50	0.5	0.1	0.1
LT-2	50	0.5	0.1	0.1
LT-3	50	0.5	0.1	0.1
LT-4	50	0.5	0.1	0.1
LT-5	50	0.5	0.1	0.1
LT-6	50	0.5	0.1	0.1
LT-7	50	0.5	0.1	0.1
LT-8	50	0.5	0.1	0.1
LT-9	50	0.5	0.1	0.1
LT-10	50	0.5	0.1	0.1

TABLE V—DUAL CONDUCTOR (TWINAX) TYPES

Designation	Impedance, Ohms	Capacitance, p.f./ft.	Attenuation, db/100 ft.	Weight, lb./100 ft.
DT-1	50	1.8	0.1	0.1
DT-2	50	1.8	0.1	0.1
DT-3	50	1.8	0.1	0.1
DT-4	50	1.8	0.1	0.1
DT-5	50	1.8	0.1	0.1
DT-6	50	1.8	0.1	0.1
DT-7	50	1.8	0.1	0.1
DT-8	50	1.8	0.1	0.1
DT-9	50	1.8	0.1	0.1
DT-10	50	1.8	0.1	0.1

ANTENNAE LEAD IN WIRE

Designation	Impedance, Ohms	Capacitance, p.f./ft.	Attenuation, db/100 ft.	Weight, lb./100 ft.
LT-1	50	0.5	0.1	0.1
LT-2	50	0.5	0.1	0.1
LT-3	50	0.5	0.1	0.1
LT-4	50	0.5	0.1	0.1
LT-5	50	0.5	0.1	0.1
LT-6	50	0.5	0.1	0.1
LT-7	50	0.5	0.1	0.1
LT-8	50	0.5	0.1	0.1
LT-9	50	0.5	0.1	0.1
LT-10	50	0.5	0.1	0.1

TABLE VI—DUAL COAXIAL TYPES

Designation	Impedance, Ohms	Capacitance, p.f./ft.	Attenuation, db/100 ft.	Weight, lb./100 ft.
DT-1	50	1.8	0.1	0.1
DT-2	50	1.8	0.1	0.1
DT-3	50	1.8	0.1	0.1
DT-4	50	1.8	0.1	0.1
DT-5	50	1.8	0.1	0.1
DT-6	50	1.8	0.1	0.1
DT-7	50	1.8	0.1	0.1
DT-8	50	1.8	0.1	0.1
DT-9	50	1.8	0.1	0.1
DT-10	50	1.8	0.1	0.1

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